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DEMONSTRATION OF SPLIT-FLOW VENTILATION AND RECIRCULATION AS FLOW-REDUCTION METHODS IN AN AIR FORCE PAINT SPRAY BOOTH

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This report has been reviewed and is approved for publication.

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#### Form Approved REPORT DOCUMENTATION PAGE OMB No. 0704-0188 Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Artington, VA 22202-4302, and to the Office of Management and Budget. Paperwork Reduction Project (0704-0188), Washington, DC 20503. 1. AGENCY USE ONLY (Leave blank) 2. REPORT DATE 3. REPORT TYPE AND DATES COVERED 940727 Final, 910215 to 921009 4. TITLE AND SUBTITLE 5. FUNDING NUMBERS Demonstration of Split-flow Ventilation and Recirculation as Contract 68-D2-0063 Flow-reduction Methods in an Air Force Paint Spray Booth Work Assignment 0/002 Program element 63723F 6. AUTHOR(S) Project 2103 S. Hughes and J. Ayer; R. Sutay, CIH (Section VI) Task 70 Work unit accession 97 8. PERFORMING ORGANIZATION 7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) REPORT NUMBER Acurex Environmental Corporation 555 Clyde Avenue FR-93-115 P.O. Box 7044 Mountain View, CA 94039 9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES) 10. SPONSORING/MONITORING AGENCY REPORT NUMBER U.S. EPA Armstrong Laboratory AEERL Environics Directorate AL/EQ-TR-1993-0002 MD-61 AL/EQS-OL Research Triangle Park, NC 27711 139 Barnes Drive, Suite 2 EPA/600/R-94/214b Tyndall AFB, FL 32403-5323 11. SUPPLEMENTARY NOTES 1. Responsible individual: Joseph D. Wander, (904) 283-6240 2. Office symbol: AL/EQS-OL 3. Availability of report is specified on inside front cover. 12a. DISTRIBUTION/AVAILABILITY STATEMENT 12b. DISTRIBUTION CODE Approved for public release; distribution is unlimited. 13. ABSTRACT (Maximum 200 words) During a series of painting operations in a horizontal-flow paint spray booth at Travis AFB, CA, baseline concentrations of four classes of toxic airborne pollutants were measured at 24 locations across a plane immediately forward of the exhaust filters, in the exhaust duct, and inside and outside

During a series of painting operations in a horizontal-flow paint spray booth at Travis AFB, CA, baseline concentrations of four classes of toxic airborne pollutants were measured at 24 locations across a plane immediately forward of the exhaust filters, in the exhaust duct, and inside and outside the respirator in the painter's breathing zone (BZ). The resulting data were analyzed and used to design a modified ventilation system that (1) separates a portion of the exhaust exiting the lower portion of the booth, which contains a concentration of toxic pollutants greater than the average at the exhaust plane (split-flow); and (2) provides an option to return the flow from the upper portion of the exhaust to the intake plenum for mixing with fresh air and recirculation through the booth (recirculation). After critical review by cognizant Air Force offices, and an experimental demonstration showing that a flame ionization detector monitoring the air entering the booth is able to detect excursions above the equivalent exposure limit for the solvents in the paint, the exhaust duct was reconfigured for split-flow and recirculating ventilation. A volunteer painter was briefed on the increased risk of exposure during recirculation, and on the purposes and possible benefits of this study. He then signed an informed consent form before participating in the recirculation tests. A series of tests generally equivalent to the baseline series was conducted during split-flow and

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#### SECURITY CLASSIFICATION OF THIS PAGE

recirculating ventilation, and three tests were performed during only split-flow ventilation. Data from the two sets of tests show that pollutants concentrate toward the bottom of the booth during ordinary painting operations; that local processes associated with circulation near the paint spray gun contribute far more to the net exposure to the painter than do toxic pollutants in the recirculated air stream; and that, under well-ventilated conditions, including split-flow and recirculation of a large fraction of the exhaust air, equivalent exposures to airborne toxic pollutants (calculated as the sum of 8-hour, timeweighted concentrations of toxicants divided by their respective Permissible Exposure Limits) should not exceed 0.25 in the intake air. An economic analysis of costs to implement thermal or catalytic incineration, with and without flow reduction by split-flow and recirculating technologies, projects substantial savings, such that the payback periods for inclusion of flow-reduction technology during installation of the control device are about 1 year. The recirculation of air in the paint spray booth did not result in an increase in air contaminants that would exceed the capability of proper respiratory protection. The magnitude of the incremental increase in exposure derives primarily from particulates in the recirculated air. This is defined by the particulate removal efficiency of the particulate controls, which can be compromised by improper maintenance. However, with proper design, installation, and maintenance, the increment to risk is normally less than the round-off errors in the calculation of net jobrelated risk. Because the cost benefit is obtained at an increase of risk of exposure to painters, the acceptability of this cost-benefit tradeoff will have to be resolved by industrial hygiene functions at both policy and local levels before this advance can be implemented at Air Force installations.

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## SUMMARY

## A. OBJECTIVE

The objective of this program was to demonstrate that split-flow and recirculating ventilation, individually and in combination, are safe and cost-effective methods of reducing paint spray booth exhaust flow rates to lower the costs both of conditioning intake air and of controlling volatile organic compound (VOC) emissions in exhaust air.

## B. BACKGROUND

This study was part of an extended program of investigations into the cost and efficacy of innovative approaches for bringing U.S. Air Force industrial operations into compliance with current and anticipated air pollution environmental standards. Adequate ventilation of paint spray booths requires the movement of large quantities of air, which are slightly contaminated during passage through the booth. Air exhausted from this process requires decontamination, which, although technically achievable at operating flow rates, can be prohibitively expensive. Because emission-control costs depend on the volume of exhaust air being treated, considerable savings can be realized through the application of an acceptable flow-reduction method.

A first principle of industrial hygiene is to employ engineering controls to their limit before invoking personal protection. In dealing with exposures to airborne toxics, the mainstay engineering device is enhancement of ventilation. However, increased ventilation creates enormous volumes of slightly contaminated air, which must be treated before discharge and, in many situations, the cost of such treatment is excessive. In such circumstances, a judgment must be made about the relative cost in increased exposure compared to the economic benefit in decreased operating cost. The goal of this study was to provide experimental data to support the development of a general Air Force position and objective criteria for local decisions about the acceptability of using flow-reduction methods in paint spray booths, based on local health-risk/cost-benefit considerations.

## C. SCOPE

This study comprised two sets of experimental measurements in Booth 2, Building 845, Travis Air Force Base (AFB), California, plus the results of an ancillary effort conducted at Research Triangle Institute (RTI) to verify experimentally that the flame ionization detector (FID) used in the ventilation control loop is within its linear response range at the equivalent exposure limit for the mixture of solvents present in the mixed topcoat. The first set of experimental measurements was a baseline characterization of the distribution of toxic pollutants at the exhaust face and in the exhaust duct of Booth 2. These data, the RTI results, and the test plan for the second set of tests were reviewed by HQ AFLC/SGBE before approval was given to proceed with the recirculation tests. The test plan and engineering drawings were reviewed by the Fire Department, Safety Office, and Civil Engineering Office at Travis AFB and approved before implementation. For the second set of tests, the ductwork in Booth 2 was reconfigured to separate exhaust streams from the top and bottom of the booth (split-flow) and to return the upper exhaust stream to the intake plenum for recirculation through the booth. The volunteer painter was briefed and signed an informed consent form before participating in the study. During separate painting sessions, several sets of concentration measurements were made of VOCs, particulates, heavy metals, and isocyanates. Equivalent exposures  $(E_m)$  were calculated from these data, and projections of  $E_m$  were made for a range of recirculation ratios, together

with an economic analysis of the corresponding costs to install flow reduction technology and apply VOC emission control devices.

## D. METHODOLOGY

Per standard Travis AFB policy, painters in Booth 2 wear a protective jump suit, a separate hood, and an airline respirator. To determine exposure concentrations, sampling was performed simultaneously inside and outside the respirator, at 24 locations at the exhaust face. in the exhaust ducts, and, during the second set of tests, at three locations at the face of each of the two intake filters. To determine environmental contributions to the load of pollutants. background air samples were collected at the back of the booth prior to the release of any paintderived materials. Standard sampling methods used were National Institute of Occupational Safety and Health (NIOSH) Method 1300 (integrated measurement of individual organic species), Bay Area Air Quality Management District (BAAQMD) Method ST-7 and U.S. Environmental Protection Agency (EPA) Method 25A (continuous measurement of total organic concentration). Occupational Safety and Health Administration (OSHA) Method 42 (filter faces and ducts) and NIOSH Method 5521 (painter and ducts) (isocyanates), EPA Method 5 and NIOSH Method 500 (particulate), and EPA Draft Multiple Metals and NIOSH Method 7300 (metals). Paint usage was determined by weighing the gun after each filling and at the end of each painting session. The percent volatile content of the paint was determined gravimetrically, as percent weight loss to Airflows were measured with an anemometer (American Conference of Governmental Industrial Hygienists [ACGIH]) in the booth and with a pitot tube (EPA 2) in the exhaust ducts. Painting start and stop times were recorded manually by an observer, stationed at the rear of the booth, who also noted the dimensions and locations of workpieces painted, coatings applied, and other details. Projections of equivalent exposures at different recirculation ratios were calculated by a Lotus 1-2-3 program written at U.S. EPA-Air and Energy Engineering Research Laboratory (AEERL).

#### E. TEST DESCRIPTION

In both test series, representative workpieces were prepared and coated according to normal operating procedures. During each such painting run, measurements were made of one of the four pollutant classes using the methods specified in Section D. A typical painting session lasted 30 to 90 minutes, and included postpainting cleaning of the paint spray gun with methyl ethyl ketone (MEK) and tidying up of the area. In general, two sets of tests were accomplished during an 8-hour shift, corresponding to a typical workday. A complete series of blood chemistry parameters was determined for the painter at the conclusion of the testing.

## F. RESULTS

Concentrations of airborne toxic pollutants are recorded in the tables of the report. Strontium chromate occurs as the major contaminant during primer coating and was the largest contributing factor to the  $\boldsymbol{E_m}$ . Organic exposures were minor during all painting exercises, except that high isocyanate exposure occurred outside, but not inside, the painter's respirator during topcoat application inside a comfort pallet (caused by airflow restrictions in the closed space, and unrelated to the mode of ventilation in the booth). The newly constructed recirculation duct was a source of several metals. These metals were included in  $\boldsymbol{E_m}$  calculations, but the concentrations are expected to decrease after the newly constructed surfaces are blown clean. Contributions to  $\boldsymbol{E_m}$  from recirculation are significantly less than the Air Force criterion of 0.25 imposed by HQ AFLC/SGBE for these tests, and much less, in

general, than the contribution from the painting process. The painter showed no evidence of overexposure during the posttest medical evaluation.

## G. CONCLUSIONS

Data support the prediction that workplace exposure levels during recirculation of paint spray booth exhausts, especially combined with split-flow extraction of the pollutant-enriched lower portion of the exhaust stream, can be maintained less than an arbitrarily selected criterion (here,  $E_m = 0.25$ ). Flow splitting as a technology is only marginally effective; however, in combination with recirculation, it acts to lower the concentrations in the recirculated stream at a given rate of recirculation. Computational projection of  $E_m$  to larger recirculation rates, and interpolation of results of an earlier economic analysis of scale-related costs to decontaminate exhaust air, indicate that available cost savings allow projected payback periods on the order of 1 year for thermal or catalytic incineration.

## H. RECOMMENDATIONS

Improvements should be examined to augment or replace present-generation filter and water particulate control systems. Concurrently, or when the improved technologies satisfy local standards, a combination of flow reduction and VOC control should be implemented in an area of intense regulatory pressure as the definitive prototype. A standardized set of criteria should be established to quide site selection, design, installation, and maintenance.

## **PREFACE**

This final report was prepared by Acurex Environmental Corporation, 555 Clyde Avenue, Mountain View, CA 94043, under Contract No. 68-D2-0063, for the U.S. Environmental Protection Agency (EPA), Air and Energy Engineering Research Laboratory (AEERL), and the Armstrong Laboratory Environics Directorate (AL/EQ), 139 Barnes Drive, Tyndall Air Force Base (AFB) FL 32403-5323. The industrial hygiene evaluation was performed by Clayton Environmental Consultants. 1252 Quarry Lake, Pleasanton, CA 94566.

This report describes measurements of background concentrations of airborne toxic pollutants in Booth 2, Building 845, Travis AFB, CA; design and construction of modifications to the booth ventilation system; measurements of airborne toxic pollutants in the modified booth during split-flow and concurrent split-flow and recirculating ventilation; and a projective analysis of equivalent personnel exposures and net costs to operate flow reduction and emission control systems at varying recirculation ratios. The work was performed between February 1991 and September 1992. The Air Force project officer was Dr. Joseph D. Wander. EPA project managers were Charles H. Darvin and Jamie K. Whitfield.

Indispensable cooperation and support were provided by a number of Air Force functions. Ted Liston (60 EMS/MAEFP) provided facilities in Building 845 and practical advice; Terry Kirkbride (60 EMS/MAEFP) and Mark Sandy (60 ABG/EM) managed coordination with cognizant Travis functions and solicited volunteer painters; Sgt. Bill Fleming and Bill Harrison painted during the baseline and split-flow tests, respectively; Richard Smith painted during the recirculating ventilation tests; TSgt. Haugen (DGMC/SGPM) saw to the posttest evaluation of Mr. Smith and secured his release of the test results; Det 6 AL/SAO, Brooks AFB TX, performed metals and isocyanate analyses; Major John Seibert, Det 6 AL/EHI and the designee of Col. Bruce Poitrast, AL/OE-CA, was an active contributor to discussions of baseline data and the test plan for the recirculation tests; Col. Phil Brown, HQ AFLC/SGBE, accepted responsibility for authorizing the performance of the recirculation tests, after several iterative discussions of these baseline results plus data and conclusions from experimental verification of the capability of flame ionization detector (FID) technology to reliably detect equivalent exposure limit of a complex (specified) mixture of paint solvents. Major Steve Bakalyar, AL/OEMI, offered constructive suggestions and contributed to the final version of this document.

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#### APPENDIX D

## **BOOTH MODIFICATION DESIGN AND CONSTRUCTION PACKAGE**

The booth modifications are illustrated in the accompanying schematics and described briefly below.

## A. DUCT MODIFICATIONS

Downstream of the existing exhaust blower (exhaust fan 1) a 48-inch-diameter sheetmetal tee was installed in the existing duct. Two motor-operated, 48-inch-diameter air dampers were installed on the exhaust ports of the tee (dampers 1 and 2). Damper 2 was installed on the downstream side of the tee and between the tee and the continuation of the existing 48-inch-diameter duct. It controls the flow of exhausted gases to the atmosphere outside the building. Damper 1 was installed on the branch side of the tee and controls the flow of exhausted gases to the inlet duct for recirculation. A new 48-inch-diameter sheetmetal duct was installed between damper 1 and the existing fresh air supply duct.

Control of the two damper air motors is regulated by Analysis Safety Valve (ASV)-1 (ASCO Model 834911), a four-way dual solenoid valve, which allows plant air to flow to or vent from the air motors according to the feedback control system (discussed below). In the event of power loss, the solenoid valve fails to the fail-safe mode, *i.e.*, the single-pass position, which closes damper 1 and opens damper 2, thus diverting all exhaust gases to the atmosphere outside the building.

In addition to modifications to the existing ducts, a new 30-inch-diameter axial blower and duct was installed to vent the lower chamber of the plenum.

## B. FEEDBACK CONTROL SYSTEM

A failsafe damper interlock control system was designed to respond to an instantaneous emission peak exceeding the STEL action level and to a 60-second emission level at or above the TLV.

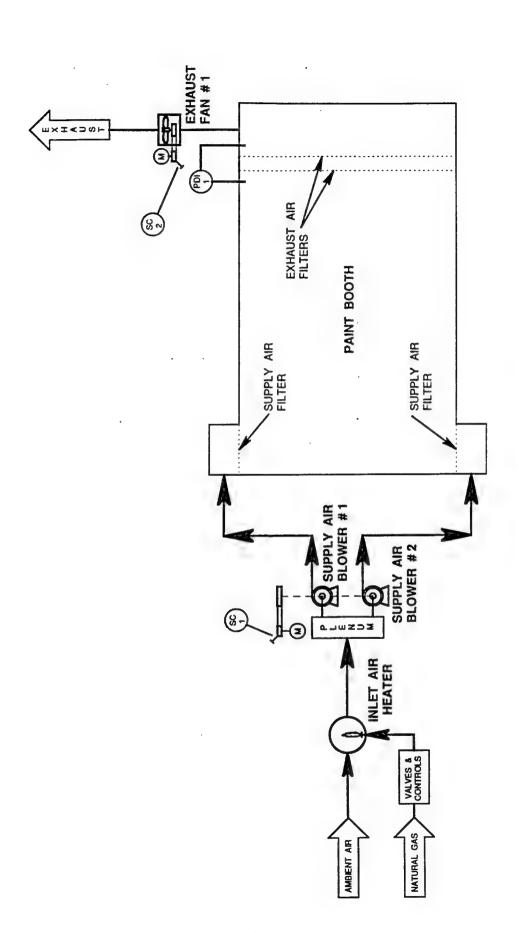
The interlock system (see drawings 8380E100 and 8380E101) was equipped with the following features:

- Total unburned hydrocarbon (TUHC) analyzer (Ratfisch Instruments type RS 55CA heated total hydrocarbon analyzer FID) (ASE-1/AST-1).
- Failsafe controls (ASA-1/ASV-1):
  - An instantaneous interlock to begin single-pass operation when STEL concentration action level is exceeded.
  - An adjustable timer (set at 5 minutes) to ensure single-pass operation for a predetermined time after STEL or TLV interlock activation, prior to converting back into the recirculation configuration.

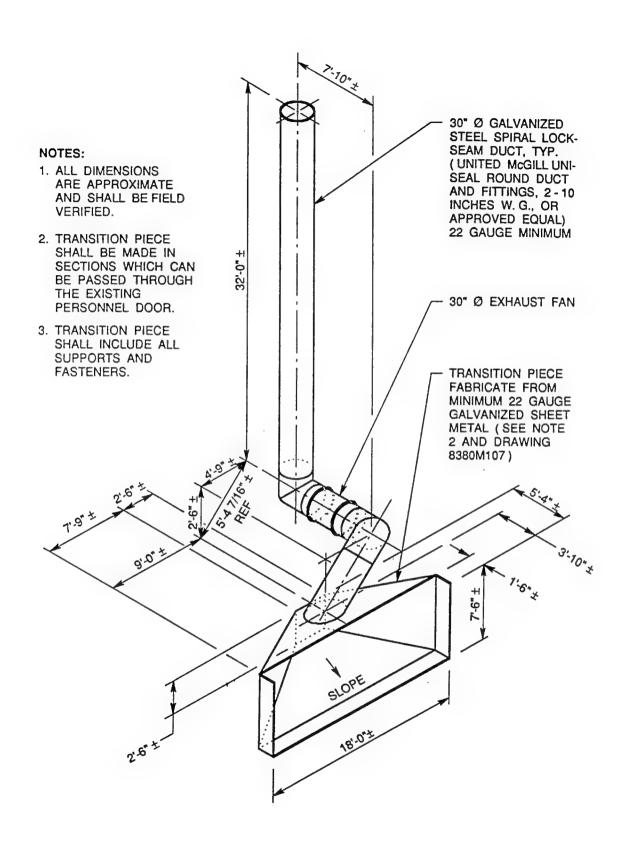
- An adjustable timer (set at 60 seconds) to delay operation of the TLV concentration interlock for 1 minute while continuing monitoring operations. If, after 1 minute, the concentration is still above TLV, the system initiates the singlepass mode.
- An indicator light to indicate that the 60-second TLV concentration timer is "on."
- An interlock to convert the system to single-pass mode if the hydrocarbon analyzer power is turned off or its flame goes out.
- A solenoid valve wired and plumbed to return to the single-pass operation mode whenever there is a power loss.

## C. PERMIT VARIANCES

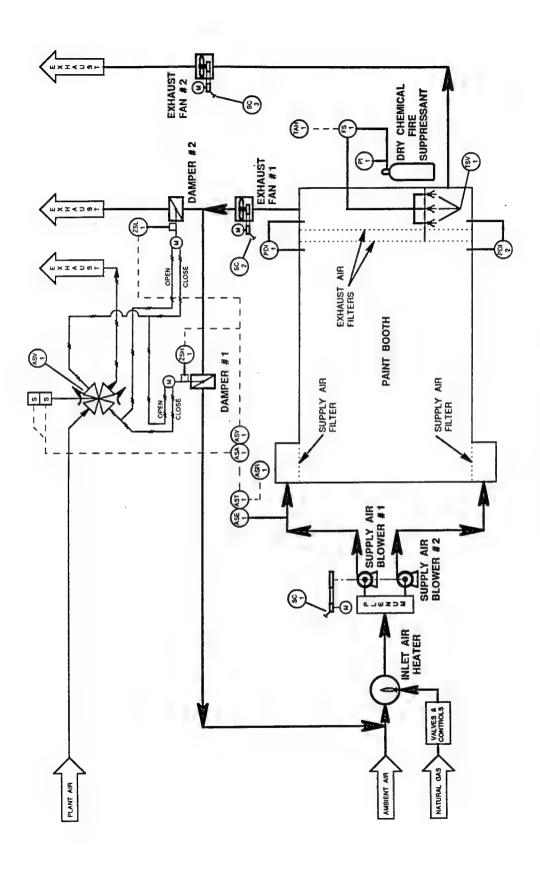
At the start of this study, the paint booth was operational and permitted for use in the single-pass mode. In conversations with the Bay Area Air Quality Management District (BAAQMD), it was determined that a new permit to operate the booth after modification was unnecessary; a notification letter to BAAQMD in advance of the modification sufficed.



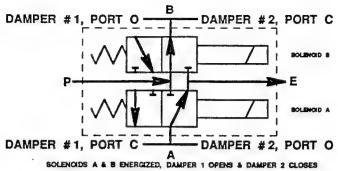
Process and Instrumentation Diagram Travis AFB Building 845 Paintbooth No. 2 Prior to Modification



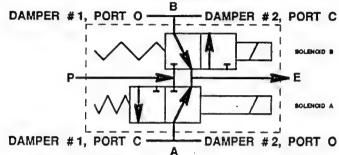
Lower Exhaust Plenum Chamber Transition Piece and Exhaust Duct Isometric for Travis AFB Building 845 Paintbooth No. 2



Process and Instrumentation Diagram
Travis AFB Building 845
Paintbooth No. 2 After to Modification

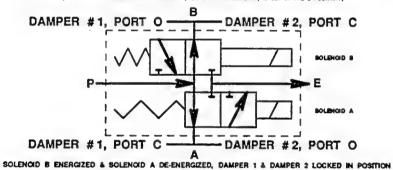


ENERGIZING BOLEHOIDS A 8 B MOVES BOTH DAMPERS INTO POSITION FOR NORMAL RECIRCULATION OPERATION (THE BWITCH INSIDE THE CONTROL BOX (SEE DRAWING \$2006100) IS SET IN THE AB POSITION.)

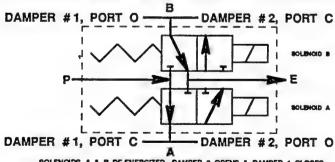


SOLENOID A ENERGIZED & SOLENOID B DE-ENERGIZED, DAMPER 1 & DAMPER 2 IN FLOATING POSITION

ENERGIZING SOLENGED A & DE-ENERGIZING SOLENGED B ALLOWS MANUAL MOVEMENT OF THE DAMPER BLADES
(THE SWITCH INSIDE THE CONTROL BOX (SEE DRAWING \$180E(D)) IS SET IN THE B POSITION)



ENERGZING SCLENOID B & DE-ENERGIZING SCLENOID A LOCKS THE DAMPER SLADES AT WHATEVER POSITION THEY ARE N (THE SWITCH INSIDE THE CONTROL BOX (SEE DRAWING 8380E(00) IS SET IN THE AS POSITION)

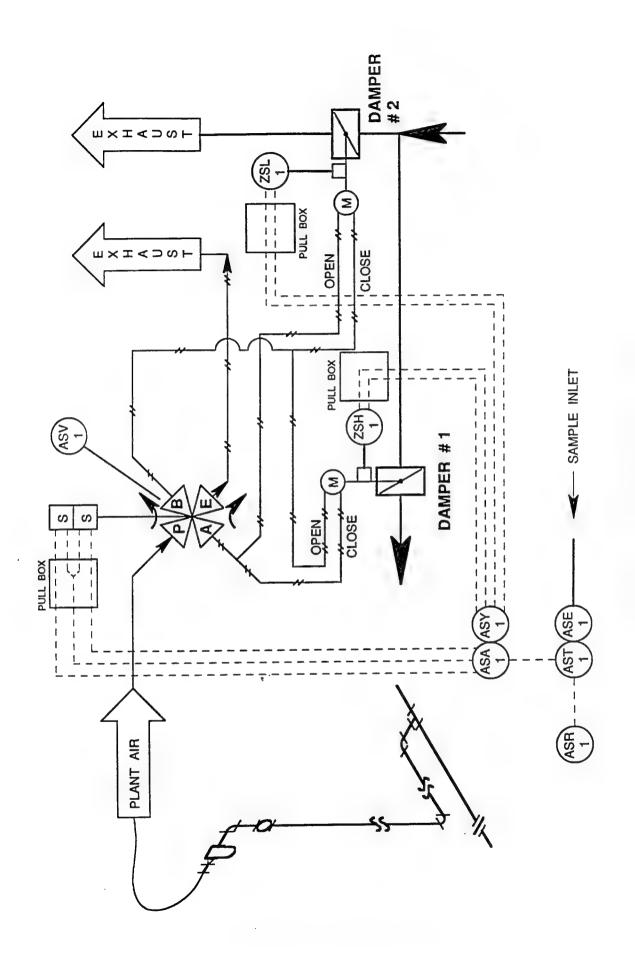


SOLENOIDS A & B DE-ENERGIZED, DAMPER 2 OPENS & DAMPER 1 CLOSES

DE-ENERGIZING SOLENOIDS A 8 8 MOVES BOTH DAMPERS INTO POSITION TO CLOSE THE RECIRCULATION LOOP AND DUMP ALL VAPORS TO THE ATMOSPHERE (THE SWITCH INSIDE THE CONTROL BOX (SEE DRAWING ISDAE100) IS SET IN THE AS POSITION)

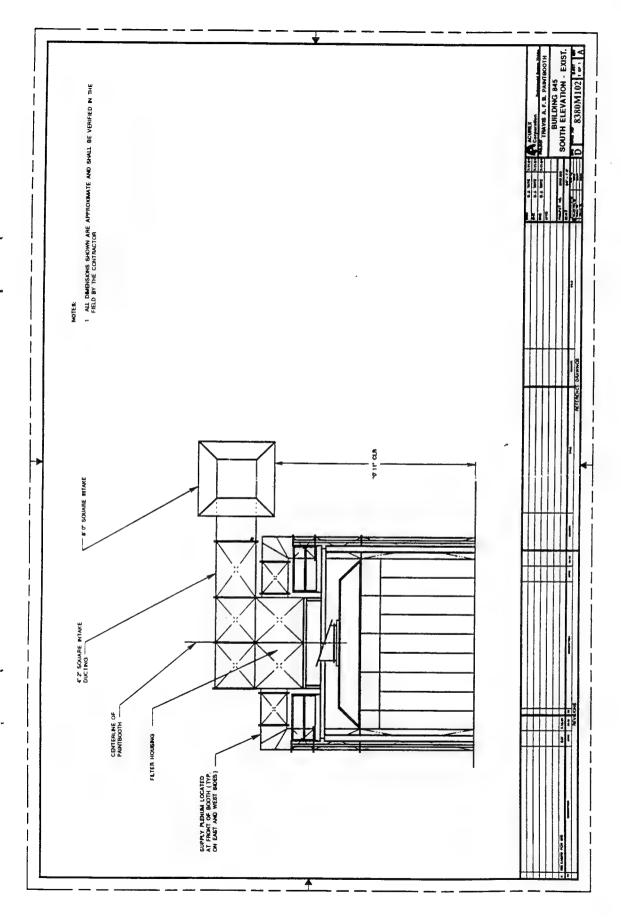
## ASCO 834911

Position Diagrams of Damper Control 4-Way Solenoid Valve ASV-1 Describing Various Energized and De-energized Positions and the Effect on Dampers No. 1 and No. 2

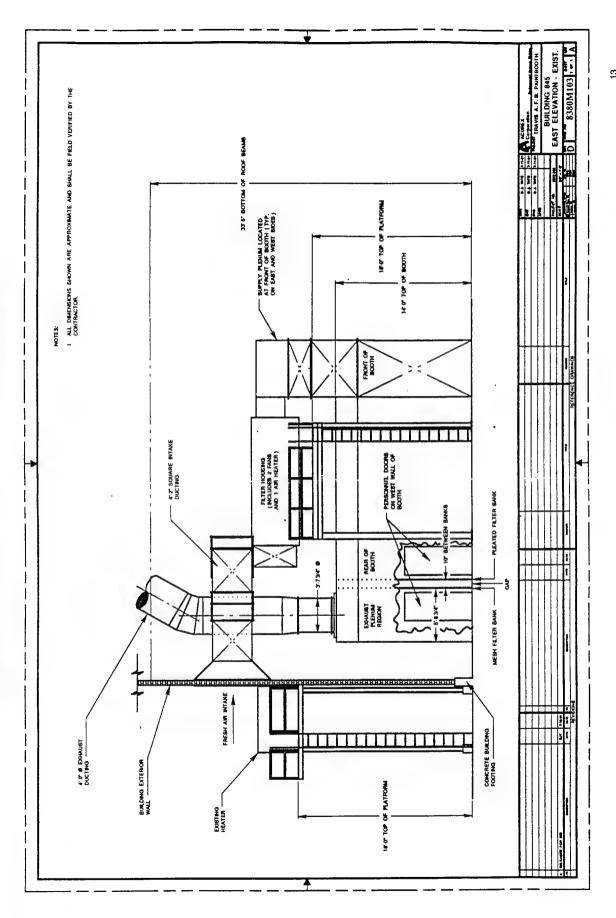


Damper Control Instrumentation Diagram

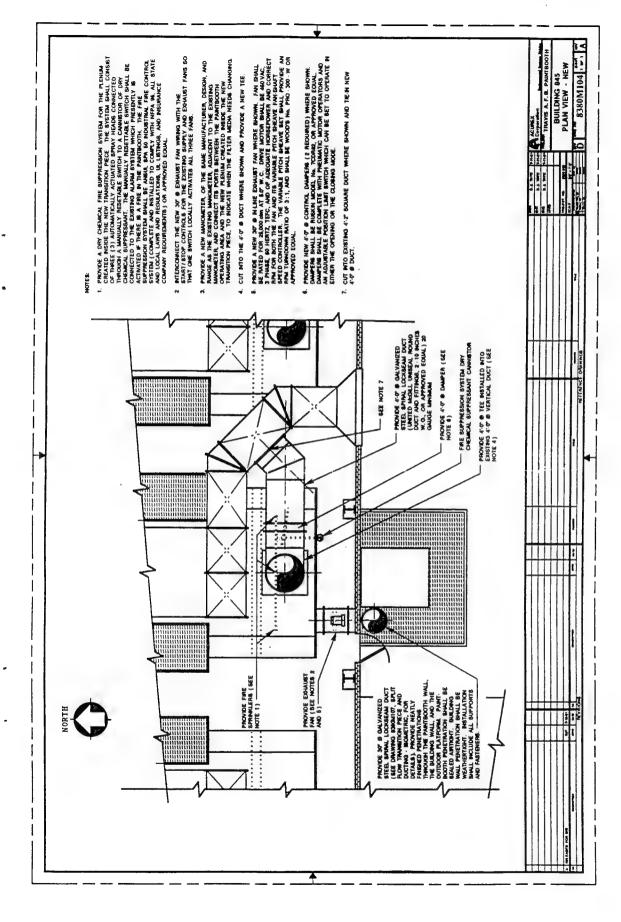
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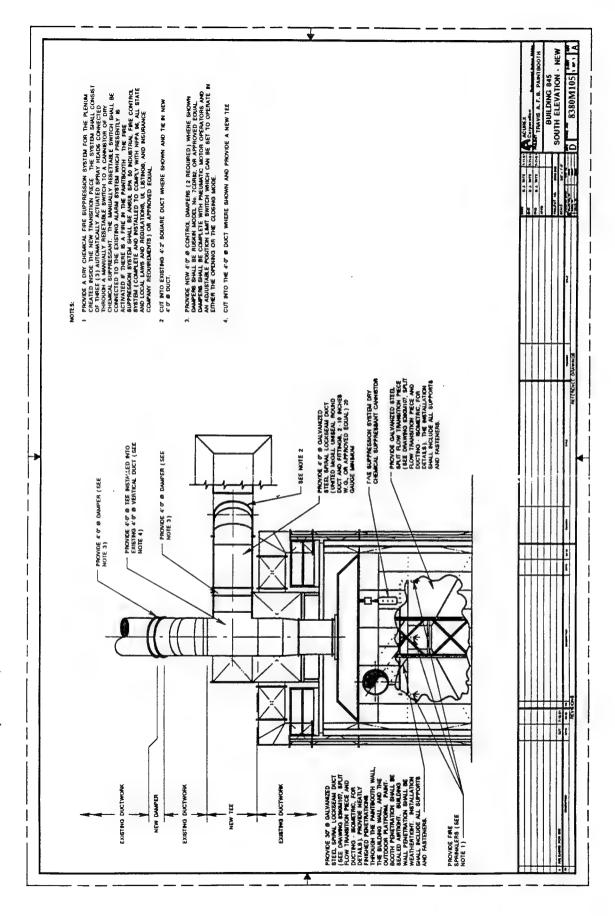


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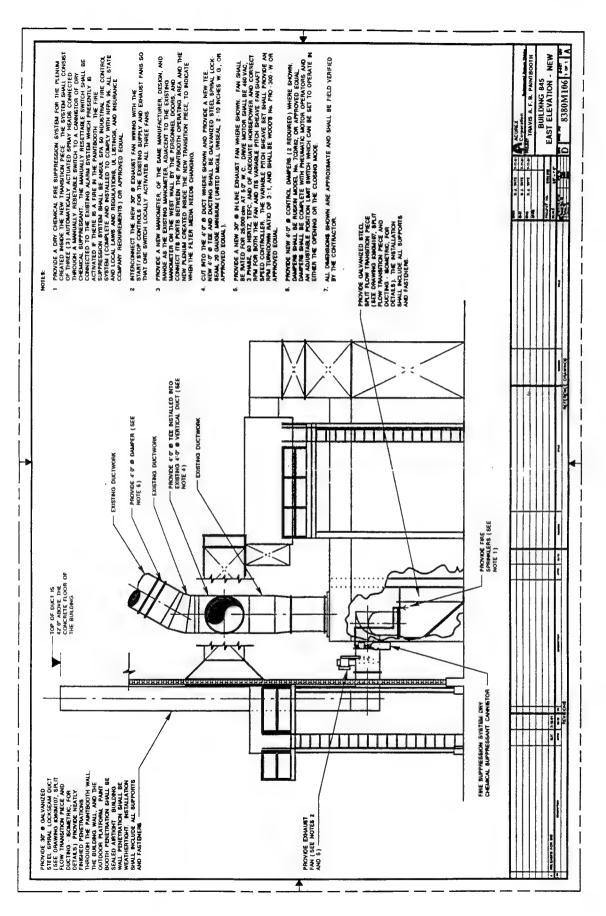


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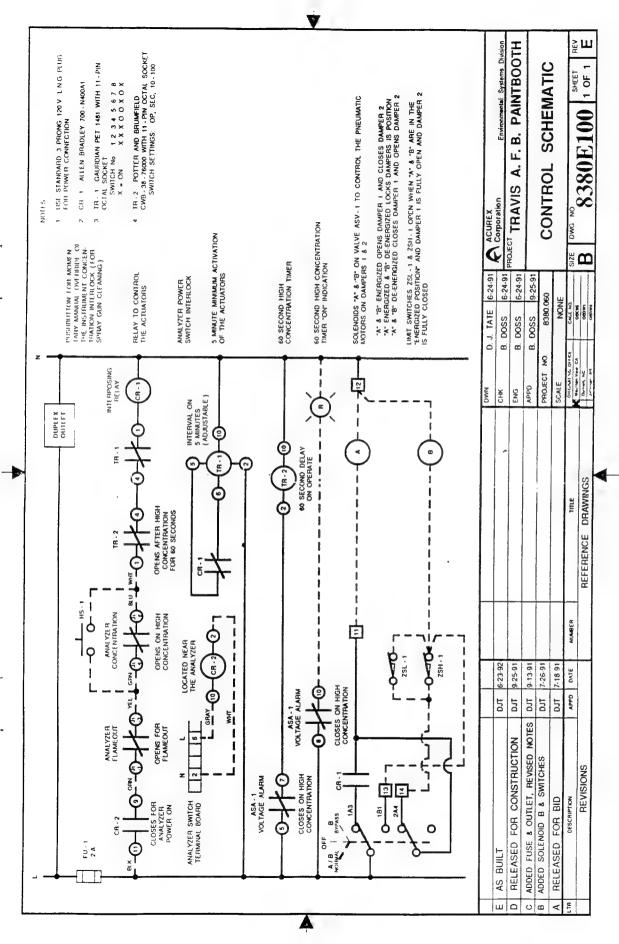


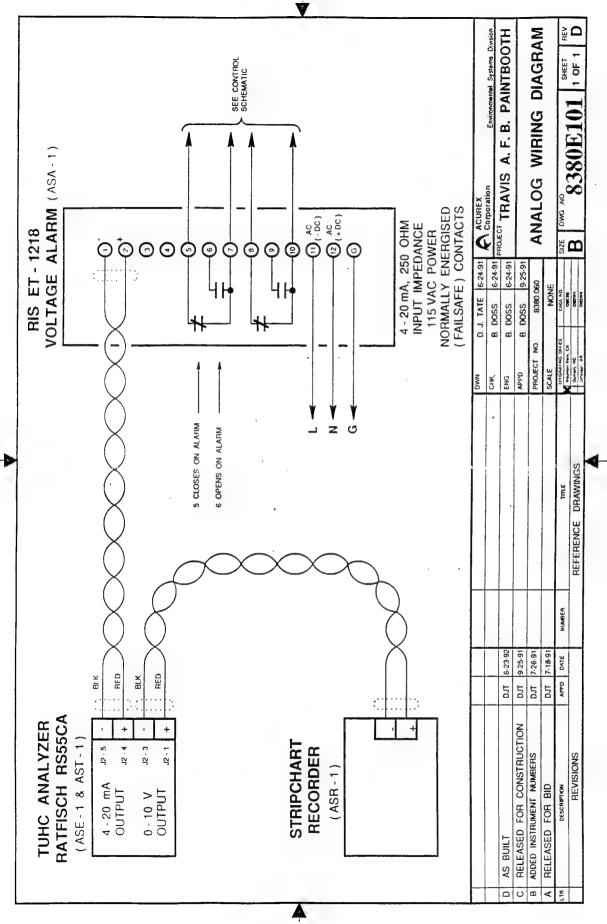


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# APPENDIX E ORGANIC DESORPTION STUDY



Mid-Pacific Environmental Laboratory, Inc. 625B Clyde Avenue Mountain View, CA 94043 (415) 964-0844 FAX (415) 961-7113

June 4, 1991

Ms. Jackie Ayer Acurex Engineers 555 Clyde Avenue Mountain View, CA 94043

Ms. Ayer:

Here are the NIOSH 1300 information I promised you. Our final report to you has all been corrected for desorption efficiency. The desorption efficiency study was performed at three levels approximately 100ug, 700ug, and 1400ug per tube. The MDL study was performed using the same amount as level I of the desorption efficiency study. The correction factor used in calculating your NIOSH 1300 is slighly different from this set I am sending to you. The only difference is that I had normalized all recovery greater than 100 percent to 100%. This set I am sending you has was not been normalized for recovery greater than 100 percent. There is only about 0.1 to 0.6 percent difference between the numbers. If you want your reports revise using the new correction factor please let me know.

Sorry this took so long. I hope this did not cause you any inconvenience with your project.

Sincerely,

2/0/93

Daniel Mew, U GC Section Manager

Mid-Pacific Environmental Laboratory Inc.

National Express Laboratory

recycled paper

MID-PACIFIC ENVIRONMENTAL LABORATORY Instrument ID: 3400-2 (DB624 60m column)

Date: 4/25/91

# Desorption Efficiency Study - Level 1

Page 2

	Extract conc.	A1	A2	A3	A4	Average %Rec.
MEK ETHYLACETATE 2-BUTANOL N-BUTANOL METHOXYACETONE ETHOXYETHANOL MIBK1 TOLUENE BUTYLACETATE ETHYLBENZENE M & P XYLENE PMGE ACETATE O-XYLENE 2-EOE ACETATE	37.00 35.00 38.00 33.00 19.00 28.00 31.00 34.00 34.00 34.00 38.00 35.00	104.82 103.64 101.60 93.65 49.37 21.35 104.61 103.57 105.15 105.76 98.47 105.00 101.18	104.57 103.55 99.80 92.62 49.11 21.59 103.58 102.63 104.17 104.81 134.76 104.47 101.46 106.23 69.15	104.99 103.29 101.38 93.33 48.08 23.88 103.50 102.51 104.05 104.31 119.45 103.52 101.42 100.73 71.00	104.18 101.56 99.92 93.04 49.52 22.33 102.03 101.11 103.08 103.47 129.22 102.90 100.65 105.04 66.08	104.64 103.01 100.67 93.16 49.02 22.29 103.43 102.46 104.11 104.59 120.48 103.97 101.18 104.74 68.22
2-MOE ETHER	38.00	66.66	09.13			

# Desorption Efficiency Study - Level 2

	Extract conc.	B1	B2	B3	B4 %	Average Rec.
MEK ETHYLACETATE 2-BUTANOL N-BUTANOL METHOXYACETONE ETHOXYETHANOL MIBK1 TOLUENE BUTYLACETATE ETHYLBENZENE M & P XYLENE PMGE ACETATE O-XYLENE 2-EOE ACETATE 2-MOE ETHER	185.00 175.00 190.00 165.00 95.00 140.00 155.00 170.00 170.00 170.00 190.00 190.00	101.28 100.77 97.92 96.04 82.71 65.70 99.92 99.48 101.05 100.37 108.54 99.14 96.08 98.93 76.16	92.99 92.15 89.68 87.79 74.71 58.65 91.01 90.54 91.88 91.55 89.66 90.21 87.66 90.42 68.80	99.24 98.52 95.49 94.12 80.82 63.85 97.57 97.04 98.33 97.85 95.80 96.58 93.62 96.43 73.87	100.94 99.73 97.36 95.48 82.38 65.98 98.25 99.45 99.15 97.12 97.81 94.92 97.79 75.16	98.61 97.79 95.11 93.36 80.16 63.54 96.82 96.33 97.68 97.23 97.78 95.94 93.07 95.89 73.50

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Desorption Efficiency Study - Level 3

	Extract conc.	C1	C2	С3	C4 %	Average Rec.
MEK	370.00	99.69	100.85 99.88	99.40	98.23	99.54
ETHYLACETATE	350.00	98.78		98.82	97.82	98.83
2-BUTANOL N-BUTANOL METHOXYACETONE	380.00	96.79	97.87	96.51	95.40	96.64
	330.00	95.38	96.61	95.10	94.27	95.34
	190.00	85.83	87.10	85.60	84.97	85.88
ETHOXYETHANOL	280.00	81.10	78.81	77.96	77.52	78.85
MIBK1	310.00	98.84	99.33	97.67	96.82	98.17
TOLUENE	340.00	98.12	98.74	97.00	95.95	97.45
BUTYLACETATE	260.00	99.14	99.86	98.49	97.85	98.83
ETHYLBENZENE M & P XYLENE PMGE ACETATE	340.00	98.08	98.78	97.52	96.81	97.80
	340.00	97.76	97.40	96.17 °	95.46	96.70
	380.00	97.26	97.89	96.73	95.99	96.97
O-XYLENE	350.00	93.79	94.46	93.37	92.72	93.59
2-EOE ACETATE	380.00	96.97	97.90	96.79	96.07	96.93
2-MOE ETHER	380.00	79.70	79.86	79.62	79.61	79.70

Average Desorption Efficiencies (percent)

	Level 1	Level 2	Level 3	Average
MEK	104.64	98.61	99.54	100.93
ETHYLACETATE	103.01	97.79	98.83	99.88
2-BUTANOL	100.67	95.11	96.64	97.48
N-BUTANOL	93.16	93.36	95.34	93.95
METHOXYACETONE	49.02	80.16	85.88	71.69
ETHOXYETHANOL	22.29	63.54	78.85	54.89
MIBK1	103.43	96.82	98.17	99.47
TOLUENE	102.46	96.33	97.45	98.74
BUTYLACETATE	104.11	97.68	98.83	100.21
ETHYLBENZENE	104.59	97.23	97.80	99.87
M & P XYLENE	120.48	97.78	96.70	104.98
PMGE ACETATE	103.97	95.94	96.97	98.96
O-XYLENE	101.18	93.07	93.59	95.94
2-EOE ACETATE	104.74	95.89	96.93	99.19
2-MOE ETHER	68.22	73.50	79.70	73.81

MID-PACIFIC ENVIRONMENTAL LABORATORY Instrument ID: 3400-2 (DB624 60m column) Date: 4/25/91

MDL Study (4/25/91)

		1					EX	Extract	Mean	STD	Ext. MDL	RDL	RDL
	A1	A2	A3	A4	AS	A6	A7	conc.	(nd/mr)	(n-1)	(nd/wr)	(ng/m])	(ug/tube)
		•	30 00	30 66	20 AG	37 75	37.66		38.39	0.49		S	20
MEK	36.78		20.00	20.00	35.33	35.03	35, 17		35.67	0.54		ស	20
ETHYLACETATE	30.27	47.00	00000		27.62	37.10	37.08	38.00	37.80	0.63	1.97	വ	20
2-BUTANOL	38.01		2000		20.12	20.00	20.70		30.39	0.47		ហ	20
N-BUTANOL	30.90		20.00	2000	300	20.00	200		20.0	0.17		10	40
METHOXYACETONE	9.38	ָה מי	9.14	T 9 . V	90.0	000	71.0		200	74.0		2	40
ETHOXYETHANOL	5.98			6.25	6.04	1.20	00.00		0000	* 0		2	0 0
MIBKI	32.43			31.63	31.44	30.88	30.95		31.65	0.00		n (	2
TICTE TO THE NEW	35, 21			34.38	34.15	33.54	33.69		34.39	0.63		N	<b>x</b> 0 <sup>†</sup>
TOLOGORA SERVICE	27.70	27.08		26.80	26.49	26.16	26.17		26.73	0.47		ស	20
BOLLLACEIALE	70.75			35, 18	34.75	34.20	34.26		35.06	0.68		73	œ
ETHILBENZENE	22.00			43.94	40.38	42.09	44.29		41.52	4.06		7	œ
M & F AILENE	000			20 10	18.74	38.29	38.33		39.06	0.63		ഹ	20
PMGE ACETATE	34.40					24.00	24 24		34 98	0.55		2	œ
O-XYLENE	35.41			33.43	24.02	24.62	***			70.1		10	40
2-FOE ACETATE	40.64			39.91	37.61	37.28	38.98		39.0L	1.34		2 6	2 4
2-MOE ETHER	25.33	26.28	26.98	25.11	25.48	27.16	26.08		26.06	0.80		OT	04
						111111111111111111111111111111111111111					 		

\* Bad calibration curve for M&P-Xylene.

RDL = Reporting limit based on instrument sensitivity and MDL study.

## APPENDIX F

## REDUCED DATA FOR THE BASELINE TEST SERIES

Date:	18 April, 1991	1991				Booth:		215							
Start Time:	17:17					11	1.79	P=29.92 "Hg	_						
Stop Time:	18:22					P.	29.88	T=68 °F							
	_	_	T in	Sample	Volume	Collected	2-Butanone (MEK)	(MEK)	Ethyl	Ethyl Acetate	_	2-Butanol		n-Butanol	nol
			1	3		CTD							-		1
	_	Sample	н.	prowrate   collected	rollected			1	A 1 h. h.			(100/cm/	- (Ym/cm)	(ad/tithe)	(mo/m3)
Site Location	Date	Number	(min)	(1/min)	= E	3	(ug/tube)	(cm/gm)	(agni /6n)	(cm/gm) (	(Sn)		l (cui/Sui	(nom) (fin)	Com (Sun)
	118 April	- Y	00 00	1 559 1	0.00	> × 00.0	20 <	N/A	< 20	A/N >	<u> </u>	> 12	N/A	< 21 ·	A/A
- r		5 2	4	1 315	2 %	86.72 x	87	0.553484	< 20	<b>v</b>	<u>~</u>	21 < (	0.242149	< 21 •	0.242149
<b>*</b>		20	00.00	1 7,668	0.00	0.00 × ×	> 02	A/N	> 20	v	· —	21 < 1	N/A	< 21 •	₩.
1 4		25	26.00	1.371	104.20	104.12 x	27	0.259326	> 20	٧	<u>~</u>	21 < (	0.201698	< 21 •	0.201698
r w	2 5	. 52	78.00	1.399	109.12	109.04 x	160	1.467376	\$	< 0.183422	<u> </u>	21 < (	0.192593	< 21 •	0.192593
· «	_ <u>~</u>	77	77.00	1.426	109.80	109.72 x	120	1.093717	> 20	< 0.182286	<u>~</u>	×	0.191400	< 21 •	0.191400
	2 2	57	77.00	1.371	105.57	105.49 x	39	0.369717	> 20	< 0.189598	<u>~</u>	21 *	0.199078	< 21 •	0.199078
. ec	3 5	252	90.09	1.381	82.86	82.80 ×	62	0.350257	> 20	< 0.241556	<u>~</u>	v	0.253634	< 21	0.253634
0	2 2	67	78.00	1.012	78.94	78.88 ×	089	8.621201	> 20	< 0.253564	<u>~</u>	21 <	0.266242	< 21 .	. 0.266242
. פר	118		0.00	1.018	0.00	0.00 ×	25	N/A	< 20	A/N ^	<u>~</u>	> 12	N/A	< 21 .	V.∀
= =	2		76.00	1.313	8.8	99.71 x	83	0.832403	< 20	< 0.200579	<u>~</u>	21 <	0.210608	< 21	0.210608
	2 4		75.00	1.284	57.78	57.74 x	65	1.125822	> 50	< 0.346406	<u>*</u>	> 12	0.363727	< 21	0.363727
. T	18	42	3.00	1.355	4.07	× 90.4	140	34.46684	\$	< 4.923834	<u>~</u>	v	5.170026	< 21.	5.170026
14	18		77.00	1.35	103.95	103.87 x	1100	10.59015	> 20	< 0.192548	<u>×</u>	<b>v</b>	0.202175	× 21 ·	0.202175
15	=		76.00	0.956	72.66	72.60 ×	160	2.203852	> 50	٧	<u>~</u>	21 ¥	0.289255	× 21 ·	0.289255
91	18		75.00	1.369	102.68	102.60 ×	170	1.656983	> 20	<b>v</b>	<u>·</u>	51 *	0.204686	> 51.	0.204686
17	- 18		77.00	1.331	102.49	102.41 x	1500	14.64726	> 50	<b>v</b>	<u>×</u>	21 <	0.205061	, 51 ,	0.205061
82	18	_	77.00	1.317	101.41	101.33 ×	1800	17.76356	° ×	v	<u> </u>	,	0.207241	× 51	0.20724
5	118		76.00	1.098	83.45	83.38 x	350	4.197455	> 20	< 0.239854	<u>v</u>	2	0.251847	× 21	c 0.251847
20	18		73.00		99.15	99.07 x <	> 02	0.201869	> 20	v	<u> </u>	21 ×	0.211963	× 21	c 0.211963
2 2	138		78.00	_	102.10	102.02 x	1100,	10.78182	> 20	~	<u>*</u>	<b>21 ×</b>	0.205834	× 21	c 0.205834
2	- =		77.00		101.56	101.48 x	240	5.320987	> 20	1 < 0.197073	<u>*</u>	2	0.206927	< 21	c 0.206927
1 12	- 12		76.00		100.17	100.09 x	140	1.398727	> 50	0.199818	<u> </u>	e S	0.209809	× 21	< 0.209809
72	188		75.00		95.70	95.63 x	120	1.254883	02 >	0.209147	<u>×</u>	21 4	0.219604	× 51	c 0.219604
	:			- 200	71 38	71 23 %	200	2.804100	20	0 < 0.280410	_ <u>*</u>	> 12	0.294430	< 21	< 0.294430
(Duplicate) 10					07 07	× 25 07	160	2 207R13	20	~	·	> 12	0.301587	< 21	< 0.301587
(Duplicate) 15		8 3	00.7		105 16	105 06 ×	2 2	0.285558	20 20	~	· ~	> 12	0.199891	< 21	< 0.199891
Painter UN	118 Apr 11				106.09	104.00 x	5300	50.95909	\$ 20	٧	×	> 12	0.201913	< 21	< 0.201913
Painter UR	110 Apr 11				0.00	0.00 × ×	> 02	N/A	< 20	V	<u> </u>	> 12	N/A	× 21	A/N. >
BIBIN	: id	_	-	_											

Painter UH = Underneath painter respirator hood. Painter OH = Outside painter respirator hood.

Travis AFB
Date: 18 April, 1991
Start Time: 17:17
Stop Time: 18:22

_			Metho	Methoxyacetone	tone	***	Ethoxyethanol	anol	4-Met	nyl-2-Pentu	4-Methyl-2-Pentanone(MIBK)		Toluene	-		Butyl Acetate	etate
_		Sample	8 8 8 8 8 8 8 8											(27,10)		(4,4)	( <u>Y</u> m/ cm/
Site Location   Date	_	Number	(ug/tube)		(mg/m3)	_	(ng/tube)	(mg/m3)	- -	(ug/tube)	(mg/m3)	8	(ng/tnpe)	(Sm/gm)	_	(agn) (fin)	(CIII/BIII)
1   18 April	orit	1 19	· ·	> 99	۸/A	<u> </u>	73 <	N/A	<b>v</b>	20 <	N/A	v	8.2 <	N/A	٧	20 <	N/A
2   18 April	orit	62	· ·	v	0.645732	<u>×</u>	73 4	0.841757	×	> 02	0.230618	<b>v</b>	8.2 <	0.094553	<b>v</b>	> 02	0.230618
	orit	47	•	v	N/A	<u> </u>	73 <	N/A	<u>~</u>	> 02	N/A	<b>v</b>	8.2 <	N/N	<b>v</b>	> 02	N/A
4 118 Ap	April	52	·	> 99	0.537862	<u>~</u>	23 4	0.701141	<u>,</u>	ĸ	0.720351		9	0.096046	<b>v</b>	<b>50 ×</b>	0.192093
5   18 Ap	April	65	~	> 99	0.513581	<u>×</u>	73 <	0.669490	<u>~</u>	> 02	0.183422	<b>v</b>	8.2 <	0.075203	<u> </u>	× 02	0.183422
6 118 Ap	April	77	·	> 99	0.510401	<u>×</u>	73 <	0.665344	<u> </u>	> 02	0.182286	<u>*</u>	8.2 <	0.074737	<b>v</b>	> 02	0.182286
7   18 Ap	April	57	~	26 < (	0.530876	_	73 <	0.692036		130	1,232392		17	0.161159	_	28	0.265438
8 118 Ap	April	55	~	~	0.676358	<u>×</u>	73 <	0.881681	_	110	1.328561	_	ç	0.229478		31	0.374412
18	April	67	<b>v</b>	٧	0.709981	<u>~</u>	73 4	0.925511	_	వే	1.064971	<b>v</b>	8.2 <	0.103961	v	> 02	
10 (18 Ap	April	2	•	v	NA	<u> </u>	73 ^	N/A	<u>~</u>	> 02	N/A	<b>v</b>	8.2 <	E/N	<u>v</u>	> 02	A/N
11 118 Ap	April	95	•	> 99	0.561621	_	007	4.011582	_	20	0.501447		100	1.002895	<u>v</u>	20	0.200579
12   18 Ap	April	20	·	·	0.969939	_	73 <	1.264385		300	5.196102	_	82	0.658173		8	1.385627
18	April	42	·	> 95	13.78673	_	23 ^	17.97199	_	120	29.54300	_	14	3.446684	_	22	5.416218
18	April	59	•	> 99	0.539135	<u>×</u>	ž,	0.702801	_	350	3.369593		35	0.336959	_	62	0.596899
18	April	45	· ·	> 99	0.771348	<u> </u>	, K	1.005507	_	890	12.25892	_	100	1.377407	_	230	3.168037
18	April	51	v	> 95	0.545829	<u> </u>	73 <	0.711528	_	980	9.552023	_	120	1.169635	_	260	2.534210
18	April	83	· ·	> 95	0.546831	<u> </u>	73 \$	0,712833	_	550	5.370663	_	58	0.566360	_	110	1.074132
18	April	41	·	v	0.552644	<u> </u>	73 <	0.720411	-	1000	9.868644	_	110	1.085550	_	230	2.269788
138	April	58	~	v	0,671592	<u> </u>	73 \$	0.875469	_	1600	19,18836	_	180	2.158691	_	400	4.797092
18	April	26	~	> 95	0.565235	<u> </u>	73 ^	0.736824	<u>~</u>	> 02	0.201869	<u>v</u>	8.2 <	0.082766	<u>×</u>	20 <	0.201869
18	April	53	<b>v</b>	> 95	0.548893	_	2	0.715521		170	1.666282	_	16	0.156826	_	%	0.254843
118	April	3	~	> 99	0.551806	_	73 ^	0.719318		150	1.478052	_	16	0.157658		3	0.305464
198	April	69	<b>v</b>	> 95	0.559490	<u>~</u>	73.	0.729336	_	260	7.593090	_	16	0.909172		200	1,998181
<u>~</u>	April	87	·	> 95	0.585612	<u>~</u>	73.	0.763387	_	950	6.483563	_	7.7	0.773844		160	1.673177
_	-								·								
(Duplicate) 10   18 April	pril	19	·	> 99	0.785148	<u>~</u>	73 \$	1.023496	_	52	0.729066	<u>×</u>	8.2 <	0.114968	<u>~</u>	× 02	_
(Duplicate) 15  18 April	pril	63	*	> 99	0.804234	<u>~</u>	3,	1.048377	_	820	12.20713	_	001	1.436133		230	3.303106
Painter UH   18 April	pril	38	·	> 99	0.533043	<u>~</u>	73 4	0.694859	<b>v</b>	<b>50 *</b>	0.190372	<u>·</u>	8.2 <	0.078052	~	2	0.190372
	pril	24	<b>v</b>	> 99	0.538435	<u> </u>	73 <	0.701889	_	1200	11.53790	_	130	1.249940	_	270	2.596029
	pril	7	<u> </u>	> 95	N/A	<u>~</u>	3,	N/A	<u> </u>	> 02	N/A	<u>×</u>	8.2 <	€ Z	<u>~</u>	Ř	K Z
		11	400	2001	404040	4	77										

Painter UH = Underneath painter respirator hood. Painter OH = Outside painter respirator hood.

18 April   18 April				Ethylbenzene	ızene	Total	Total Xylenes		PMGE Acetate	cetate	2-Ethoxyethyl Acetate	ethyl	Acetate	2-Methoxye	2-Methoxyethyl Ether	
118   April   67   62   62   62   62   62   67   68   68   68   68   68   68   68	Site Location   Date			(ug/tube)	(mg/m3)	(ug/tub			(ug/tube)	(mg/m³)	(ug/tu	28	(mg/m3)	(ug/tube)		
18 April   52   62   62.2   0.04553   62   0.07503   62   0.07505   63   64   0.07205   64   0	1   18 Apr	_	<u> </u>		N/A	80	٧	<u> </u>	20	N/A	×	¥1 ×	NA	> 54	N/A -	W/N
18 April   57   6 8.2 ¢ 0.07878   6 8.2 ¢ 0.07878   6 5.0 ¢ 0.17828   6 41 ¢ 0.158791   6 54 ¢ 0.17858   7 6 8.2 ¢ 0.07878   6 5.0 ¢ 0.07828   6 41 ¢ 0.158791   6 54 ¢ 0.17828   7 6 8.2 ¢ 0.07878   6 5.2 ¢ 0.08878   6 5.2 ¢ 0.07878   6 5.2 ¢ 0.08778   6 5.2 ¢ 0.07878   6 5.2 ¢ 0.	18		<u> </u>	8.2 <	0.094553	8.3	·	53 -	20 -	< 0.230618	<u>~</u>	× 14	0.472768	< 54	< 0.622670	0.553484
18 April   52   < 6.2 < 0.078758   < 2.0 < 0.183422   < 41 < 0.375071   < 54 < 0.5518552   < 18.2 < 0.078758   < 2.0 < 0.183422   < 41 < 0.375071   < 54 < 0.551852   < 54 < 0.551852   < 18.2 < 0.078773   < 2.0 < 0.183422   < 41 < 0.375048   < 54 < 0.452772   < 54 < 0.452772   < 64 < 1.8 April   < 57   < 6.2 < 0.078773   < 2.0 < 0.183428   < 41 < 0.376486   < 54 < 0.452772   < 54 < 0.452772   < 64 < 1.8 April   < 57   < 6.2 < 0.077773   < 2.0 < 0.183428   < 41 < 0.378648   < 54 < 0.452772   < 54 < 0.451772   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   < 64 < 0.45177   <	3   18 Apr	_	<u>~</u>		N/A	, 89 , 19	~	<u> </u>	50 -	√N/A	<u>~</u>	× 1 ×	N/A	> 54	W/A >	W/W
18 April   55   4	18	_	<u> </u>		0.078758	× ×	~	58 -	. 20	< 0,192093	<u>~</u>	× 17	0.393791	. 54	< 0.518652	1.075724
18 April   57   6	18	_	<u> </u>		0.075203	, w	<b>v</b>	03	20	< 0.183422	<u>*</u>	> 17	0.376015	> 54	< 0.495239	1.467376
18 April   55   < 8.2 < 0.077735   < 8.2 < 0.077735   < 8.2 < 0.077735   < 8.2 < 0.077735   < 8.2 < 0.077735   < 8.2 < 0.077735   < 8.2 < 0.077735   < 8.2 < 0.077735   < 8.2 < 0.077735   < 8.2 < 0.077735   < 8.2 < 0.077735   < 8.2 < 0.077735   < 8.2 < 0.077355   < 8.1 < 0.045591   < 8.4 < 0.045591   < 8.4 < 0.045591   < 8.4 < 0.045591   < 8.4 < 0.045591   < 8.4 < 0.045991   < 8.4 < 0.045991   < 8.4 < 0.045991   < 8.4 < 0.045991   < 8.4 < 0.045991   < 8.4 < 0.045991   < 8.4 < 0.045991   < 8.4 < 0.045991   < 8.4 < 0.045991   < 8.4 < 0.045991   < 8.4 < 0.045991   < 8.4 < 0.045991   < 8.4 < 0.045991   < 8.4 < 0.045991   < 8.4 < 0.045991   < 8.4 < 0.045991   < 8.4 < 0.045991   < 8.4 < 0.045991   < 8.4 < 0.045991   < 8.4 < 0.045991   < 8.4 < 0.045991   < 8.4 < 0.045991   < 8.4 < 0.045991   < 8.4 < 0.045991   < 8.4 < 0.045991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049991   < 8.4 < 0.049	18	_	<u>×</u>		0.074737	.8	~	37   <	50	< 0.182286	<u>*</u>	× 14	0.373686	> 54	< 0.492172	1.093717
18 April   55   c	7   18 Apr	_	<u>×</u>		0.077735	A	~	35	. 20 .	< 0.189598	<u>~</u>	× 1 ×	0.388677	> 54	< 0.511917	2.028708
18 April   49   < 8.2 < 0.103951   < 8.2 < 0.103951   < 20 < 0.253564   < 41 < 0.519907   < 54 < 0.0686624   < 8.2 < 0.013951   < 20 < 0.253564   < 41 < 0.719907   < 54 < 0.71918   < 64   < 14   M   M   < 41   M   < 41   M   M   < 41   M   M   < 41   M   M   < 41   M   < 41   M   M   < 41	18		<u> </u>		0.099038	.8	~	38	50	< 0.241556	<u>~</u>	> 15	0.495191	< 54	< 0.652203	2.282710
18 April   64   < 6.2 < 0.04237   < 6.2 < 0.04237   < 20 < 0.200579   < 41 < 0.710134   < 54 < 0.541563   < 18 < 0.541563   < 18 < 0.041117   < 54 < 0.041117   < 54 < 0.541563   < 18 < 0.041117   < 54 < 0.042337   < 20 < 0.200579   < 41 < 0.710134   < 54 < 0.541563   < 6.241563   < 6.241564   < 6.241564   < 41 < 0.710134   < 54 < 0.541563   < 6.241564   < 6.241564   < 6.241564   < 6.241564   < 6.241564   < 6.241564   < 6.241564   < 6.241564   < 6.241564   < 6.241564   < 6.241564   < 6.241564   < 6.241564   < 6.241564   < 6.241564   < 6.241564   < 6.241564   < 6.241564   < 6.241564   < 6.241564   < 6.241564   < 6.241564   < 6.241564   < 6.241564   < 6.241564   < 6.241564   < 6.241564   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24156   < 6.24	18		<u> </u>	8.2 <	0.103951	8	v	- 190	20.	c 0.253564	<u>~</u>	× 1.5	0.519807	> 54	< 0.684624	9.686173
18 April   46   4 8.2 < 0.042237   4 8.2 < 0.200579   4 14 0.411187   4 5 4 0.541563   5 18 April   50   4 8.2 < 0.0420237   4 8.2 < 0.200579   4 14 0.411187   4 5 4 0.95328   4 18.24456   4 14 0.041187   4 5 4 0.95328   4 18.24458   4 14 0.04038   4 18.24458   4	<u>~</u>		<u> </u>	8.2 <	NA	× ×	~	· _	20 -	· N/A	<u>~</u>	× 1.4	N/A	> 54	UN V	N/A
18 April   50   < 8.2 < 0.142026   < 8.2 < 0.142026   < 8.2 < 0.142026   < 8.2 < 0.142026   < 8.2 < 0.142026   < 8.2 < 0.142026   < 8.2 < 0.142026   < 8.2 < 0.142026   < 8.2 < 0.142026   < 8.2 < 0.142026   < 8.2 < 0.142026   < 8.2 < 0.142026   < 8.2 < 0.142026   < 8.2 < 0.078934   < 8.2 < 0.078934   < 8.2 < 0.078934   < 8.2 < 0.078934   < 8.2 < 0.078934   < 8.2 < 0.078934   < 8.2 < 0.078934   < 8.2 < 0.078934   < 8.2 < 0.078934   < 8.2 < 0.078934   < 8.2 < 0.078934   < 8.2 < 0.078934   < 8.2 < 0.078934   < 8.2 < 0.078934   < 8.2 < 0.078934   < 8.2 < 0.078934   < 8.2 < 0.078934   < 8.2 < 0.078934   < 8.2 < 0.078934   < 8.2 < 0.078937   < 8.2 < 0.078934   < 8.2 < 0.078934   < 8.2 < 0.078934   < 8.2 < 0.078934   < 8.2 < 0.078934   < 8.2 < 0.078934   < 8.2 < 0.078934   < 8.2 < 0.080937   < 8.2 < 0.080937   < 8.2 < 0.078934   < 8.2 < 0.080937   < 8.2 < 0.080937   < 8.2 < 0.080937   < 8.2 < 0.080937   < 8.2 < 0.080932   < 8.2 < 0.078934   < 8.2 < 0.080932   < 8.2 < 0.078934   < 8.2 < 0.080932   < 8.2 < 0.078934   < 8.2 < 0.080932   < 8.2 < 0.080932   < 8.2 < 0.078934   < 8.2 < 0.080932   < 8.2 < 0.080932   < 8.2 < 0.078934   < 8.2 < 0.080932   < 8.2 < 0.080932   < 8.2 < 0.080932   < 8.2 < 0.080932   < 8.2 < 0.080932   < 8.2 < 0.080932   < 8.2 < 0.080932   < 8.2 < 0.080932   < 8.2 < 0.080932   < 8.2 < 0.080932   < 8.2 < 0.080932   < 8.2 < 0.080932   < 8.2 < 0.080932   < 8.2 < 0.080932   < 8.2 < 0.080932   < 8.2 < 0.080932   < 8.2 < 0.080933   < 8.2 < 0.080932   < 8.2 < 0.080933   < 8.2 < 0.080932   < 8.2 < 0.080933   < 8.2 < 0.080932   < 8.2 < 0.080933   < 8.2 < 0.080932   < 8.2 < 0.080933   < 8.2 < 0.080932   < 8.2 < 0.080933   < 8.2 < 0.080932   < 8.2 < 0.080933   < 8.2 < 0.080932   < 8.2 < 0.080933   < 8.2 < 0.080932   < 8.2 < 0.080933   < 8.2 < 0.080932   < 8.2 < 0.080933   < 8.2 < 0.080932   < 8.2 < 0.080933   < 8.2 < 0.080932   < 8.2 < 0.080933   < 8.2 < 0.080932   < 8.2 < 0.090933   < 8.2 < 0.090933   < 8.2 < 0.090933   < 8.2 < 0.090933   < 8.2 < 0.090933   < 8.2 < 0.090933   < 8.2 < 0.090933   < 8.2 < 0.0909	18		<u>~</u>		0.082237	, 00°	~	37   <	20 -	< 0.200579	<u> </u>	× 1.4	0.411187	> 54	< 0.541563	2.537325
18 April   55   < 8.2 < 0.078944   < 8.2 < 0.078944   < 20 < 0.923634   < 41 < 0.09366   < 54 < 13.29435   5	118	_	<u> </u>		0.142026	, 89 , 7	v	> 92	. 20	< 0.346406	<u>*</u>	× 1.5	0.710134	< 54	< 0.935298	8.365725
18 April   59   < 8.2 < 0.078944   < 8.2 < 0.078944   < 20 < 0.027548   < 41 < 0.394723   < 54 < 0.519880   < 118 April   51	18	_	<u>~</u>		2.018772	× 8.	٧	22	50	< 4.923834	<u>~</u>	> 15	10.09386	> 54	< 13.29435	72.87275
18 April   51   6 8.2 < 0.112947   6 8.2 < 0.112947   6 20 < 0.275481   6 41 < 0.564737   6 54 < 0.743800   1	18		<u>~</u>		0.078944	× 08	~	7 77	02	< 0.192548	<u>·</u>	> 17	0.394723	> 54	< 0.519880	14,89360
18 April   51   < 8.2 < 0.079925   < 8.2 < 0.079925   < 20 < 0.194939   < 41 < 0.399625   < 54 < 0.526335   < 18 April   66   < 8.2 < 0.080071   < 20 < 0.195296   < 41 < 0.400358   < 54 < 0.527301   < 18 April   66   < 8.2 < 0.080071   < 20 < 0.195296   < 41 < 0.400358   < 54 < 0.527301   < 18 April   66   < 8.2 < 0.080922   < 20 < 0.197372   < 41 < 0.40644   < 54 < 0.527301   < 18 < 0.527301   < 18 April   56   < 8.2 < 0.080922   < 8.2 < 0.080922   < 20 < 0.197372   < 41 < 0.40644   < 54 < 0.532906   < 54 < 0.527301   < 18 April   56   < 8.2 < 0.080373   < 8.2 < 0.080373   < 20 < 0.201869   < 41 < 0.40464   < 54 < 0.545048   < 18 < 0.545048   < 18 < 0.545048   < 18 < 0.545048   < 18 < 0.545048   < 18 < 0.545048   < 18 < 0.545048   < 18 < 0.545048   < 18 < 0.545048   < 18 < 0.545048   < 18 < 0.545048   < 18 < 0.545048   < 18 < 0.545048   < 18 < 0.545048   < 18 < 0.545048   < 18 < 0.545048   < 18 < 0.545048   < 18 < 0.545048   < 18 < 0.545048   < 18 < 0.54604   < 18 < 0.54604   < 18 < 0.54604   < 18 < 0.54604   < 18 < 0.54604   < 18 < 0.54604   < 18 < 0.54604   < 18 < 0.54604   < 18 < 0.54604   < 18 < 0.54604   < 18 < 0.54604   < 18 < 0.54604   < 18 < 0.54604   < 18 < 0.40662   < 18 < 0.54604   < 18 < 0.54604   < 18 < 0.40662   < 18 < 0.54604   < 18 < 0.54604   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.54607   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662   < 18 < 0.40662	18	_	<u> </u>	-	0.112947	× 88	~	>   27	50	c 0.275481	<u>~</u>	× 1.7	0.564737	> 54	< 0.743800	19.00822
18 April   68   < 8.2 < 0.080071   < 8.2 < 0.080071   < 20 < 0.195296   < 41 < 0.400358   < 54 < 0.527301   5	18	_	<u>~</u>	8.2 <	0.079925	9.6		02	. 20	< 0.194939	<u>~</u>	× 14	0.399625	> 54	< 0.526335	15.00642
18 April   56   < 8.2 < 0.080922   < 8.2 < 0.098340   < 20 < 0.197372   < 41 < 0.404614   < 54 < 0.532906   3	138	_	~	8.2 <	0.080071	A 8.	~	171	50	< 0.195296	<u>~</u>	> 17	0.400358	> 54	< 0.527301	21.65842
18 April   58   < 8.2 < 0.098340   < 8.2 < 0.098340   < 20 < 0.239654   < 41 < 0.491701   < 54 < 0.647607   3	18	-	<u>~</u>	8.2 <	0.080922	× ×	v	22   4	. 20	< 0.197372	<u> </u>	> 17	0.404614	> 54	< 0.532906	30.98754
18 April   56   < 8.2 < 0.082766   < 8.2 < 0.082766   < 20 < 0.201869   82	118	_	<u>~</u>		0.098340	× 88.	~	× 1 079	50	< 0.239854	<u>~</u>	× 17	0.491701	> 54	< 0.647607	30.34160
18 April   53   < 8.2 < 0.080373   < 8.2 < 0.080373   < 20 < 0.196033   < 41 < 0.401868   < 54 < 0.529289   < 8.2 < 0.080800   < 8.2 < 0.080800   < 20 < 0.197073   < 41 < 0.404000   < 54 < 0.532098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232208   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098   < 6.232098	18	_	<u>~</u>		0.082766	× 88	~	99,	50	< 0.201869	_	82	0.827666	> 24	< 0.545048	0.827666
18 April   60   < 8.2 < 0.080800   < 8.2 < 0.080800   < 20 < 0.197073   < 41 < 0.404000   < 54 < 0.532098         18 April   69   < 8.2 < 0.081925   < 8.2 < 0.081925   < 20 < 0.199818   < 41 < 0.409627   < 54 < 0.53509       18 April   64   < 8.2 < 0.085750   < 8.2 < 0.085750   < 20 < 0.209147   < 41 < 0.428751   < 54 < 0.54697       18 April   61   < 8.2 < 0.114968   < 20 < 0.280410   < 41 < 0.578840   < 54 < 0.757107       18 April   64   < 8.2 < 0.114968   < 8.2 < 0.114968   < 20 < 0.287226   < 41 < 0.578840   < 54 < 0.75511       18 April   65   < 8.2 < 0.078842   < 8.2 < 0.117762   < 20 < 0.190372   < 41 < 0.598814   < 54 < 0.775511       18 April   54   < 8.2 < 0.078842   < 8.2 < 0.078852   < 20 < 0.190372   < 41 < 0.590263   < 54 < 0.514005       18 April   71   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078853   < 8.2 < 0.078853   < 8.2 < 0.078854   < 8.2 < 0.078854   < 8.2 < 0.078854   < 8.2 < 0.078854   < 8.2 < 0.078854   < 8.2 < 0.078854   < 8.2 < 0.078854   < 8.2 < 0.078854   < 8.2 < 0.078854   < 8.2 < 0.078854   < 8.2 < 0.078854   < 8.2 < 0.078854   < 8.2 < 0.078854   < 8.2 < 0.078854   < 8.2 < 0.078854   < 8.2 < 0.078854   < 8.2 < 0.078854   < 8.2 < 0.078854   < 8.2 < 0.07885   < 0.078854   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.07885   < 0.	118	_	<u>~</u>		0.080373	× 88.	~	173	20	< 0.196033	<u>×</u>	> 17	0.401868	> 54	< 0.529289	12.85978
18 April   69   < 8.2 < 0.081925   < 8.2 < 0.081925   < 20 < 0.199818   < 41 < 0.409627   < 54 < 0.535509   < 18 April   48   < 8.2 < 0.085750   < 8.2 < 0.085750   < 20 < 0.209147   < 41 < 0.428751   < 54 < 0.564697   < 18 April   61   < 8.2 < 0.114968   < 8.2 < 0.114968   < 20 < 0.280410   < 41 < 0.574840   < 54 < 0.757107   < 18 April   65   < 8.2 < 0.114762   < 20 < 0.287226   < 41 < 0.574840   < 54 < 0.775511   < 18 April   65   < 8.2 < 0.078052   < 20 < 0.190372   < 41 < 0.598814   < 54 < 0.775511   < 18 April   54   < 8.2 < 0.078842   < 8.2 < 0.078052   < 20 < 0.190372   < 41 < 0.590263   < 54 < 0.514005   < 18 April   < 41 < 0.390263   < 54 < 0.514005   < 18 April   < 17   < 8.2 < 0.078842   < 8.2 < 0.078052   < 20 < 0.192298   < 41 < 0.390263   < 54 < 0.519205   < 18 April   < 17   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078841   < 54 < 0.514005   < 18 April   < 54   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 < 0.078842   < 8.2 <	18	-	<u>~</u>		0.080800	× ×	v	000	20.	< 0.197073	<u>·</u>	> 17	0.404000	> 24	< 0.532098	7.262162
18 April   48   < 8.2 < 0.085750   < 8.2 < 0.085750   < 20 < 0.209147   < 41 < 0.428751   < 54 < 0.564697	138	_	<u>~</u>		0.081925	× ×	v	>   52	20 3	< 0.199818	<u>*</u>	× 17	0.409627	< 54	< 0.539509	11.89917
18 April   61   < 8.2 < 0.114968   < 8.2 < 0.114968   < 20 < 0.280410   < 41 < 0.574840   < 54 < 0.757107   :	18	_	<u>~</u>		0.085750	× ×	v	50 +			<u>~</u>	× 17	0.428751	> 24	< 0.564697	10.18546
18 April   61   < 8.2 < 0.114968   < 8.2 < 0.114968   < 20 < 0.280410   < 41 < 0.574840   < 54 < 0.757107	_	_	_					_								
18 April   63   < 8.2 < 0.117762   < 8.2 < 0.117762   < 20 < 0.287226   < 41 < 0.58814   < 54 < 0.775511		_	<u>~</u>			× 88	٧	890			<u>~</u>	> 17	0.574840	> 54	< 0.757107	3.533166
18 April   66   4 8.2 < 0.078052   4 8.2 < 0.078052   4 20 < 0.190372   4 11 < 0.390263   4 20 < 0.514005   4 20 < 0.192298   4 20 < 0.394211   4 20 < 0.192298   4 390263   4 20 < 0.192298   4 390263   4 390	_	_	<u>×</u>			<b>80</b>	v	162   4	20	< 0.287226	<u>*</u>	× 17	0.588814	> 54	< 0.775511	19.24418
18 April   54		_	<u>~</u>			× ×	v	52   4	20	< 0.190372	<u>×</u>	× 15	0.390263	> 54	< 0.514005	0.285558
118 April   71   8.2 < N/A   8.2 < N/A   50 < N/A   41 < 11 < N/A   54 < N/A		_	<u>~</u>			6		503	20	< 0.192298	<u>*</u>	× 17	0.394211	> 54	< 0.519205	66.34297
		_	<u>~</u>			œ	٧	Ť	ν 50	A/N >	<u>×</u>	> 17	N/A	> 24	N/A v	N/A

Painter UH = Underneath painter respirator hood. Painter OH = Outside painter respirator hood.

Date: 18 April, 1991 Start Time: 17:17 Stop Time: 18:22

Travis AFB

Stop Time:	70:11	11:02					•											
			Sample		Ethoxyethanol	anol	4-Het	4-Methyl-2-Pentanone(MIBK)	none(MIBK)		Toluene			Butyl Acetate	state		Ethylbenzene	zene
Site Location	;	Date	Number		(ug/tube)	(mg/m3)		(ug/tube)	(mg/m3)	bn)	(ug/tube)	(mg/m3)		(ug/tube)	(mg/m3)		(ug/tube)	(mg/m3)
-	8	April	54		23	0.780		20 <	712 0	·	× ×	0 088		000			c c	Č
2	138	April	50	v	23	0.907	~	20 <	0.248		, v	0.102	· v	2 5		· v	× × ×	0.0
æ	18	April	13	٧	23 4	1.937	v	20 <	0.531	· •	8.2 <	0.218		50 × 02	0.531	· ×	8.2 4	0.218
4	<u>2</u>	April	ž	v	73 <	0.753		160	1.651		23	0.237		43		<b>v</b>	8.2 <	0.08
w.	2	April	9	<b>v</b>	73 ^	0.709	~	> 02	0.194	v	8.2 <	0.080	~	20 <		٠,	8.2 <	0.080
901	<u>e</u>	April	52	~	24	0.713	_	54	0.234	<b>v</b>	8.2 <	0.080	~	> 02		٧	8.2 <	0.080
7	8	April	28	~	23 <	0.758	_	150	1.557		23	0.239		39		<u> </u>	8.2 <	0.085
<b>*</b> 0 (	8 9	April	23	<b>v</b>	2	0.767		250	2.626		38	0.399		29	0.704	٧	8.2 <	0.086
<b>5</b>	2	April	25	~	2	0.899		27	0.579	<b>v</b>	8.2 <	0.101	٧	> 02		<u> </u>	8.2 <	0.101
2;	2 9	April	6 :	<u> </u>	2	1.022	-	90	1.400		16	0.224	_	54		<b>v</b>	8.2 <	0.115
= \$	2 9	April	25	<b>v</b>	21	0.773		510	2.400		ĸ	0.773		140		v	8.2 <	0.087
2.5	2	40.	2 2	<b>v</b>	21	0.806		077	4.859		65	0.718		120		<u>~</u>	8.2 <	0.091
2 :	2 9	ν γ	9 2	<b>v</b>	21	0.745		320	3.264		33	0.337	_	94		<u>~</u>	8.2 <	0.084
4 6	2 5	April	55	~	21	0.756		450	7.662		92	0.673	_	130		<b>v</b>	8.2 <	0.085
<u> </u>	2 9	April	מ מ	v	21	1.097	-	1100	16.527		150	2.254		320	4.808	<b>v</b>	8.2 <	0.123
2 !	2 5	April	72	~	21	0.77		1400	14.793		190	2.008	_	400		<u> </u>	8.2 <	0.087
2 :	2 5	April	ရ (	<b>v</b>	21	0.748		300	3.074		37	0.379		8		<u> </u>	8.2 <	0.084
20 9	2 9	<b>A</b> pr. 1	3	~	21	0.765		930	0,740		110	1,152	_	210		<u> </u>	8.2 <	0.086
2 6	20 9	April	<u>د</u> د	<b>v</b>	× 1	0.889	*	2300 **	28.025		310	3.777	_	099		<u> </u>	8.2 <	0.100
2.5	9 9	April	* (	~	21	0.796		2000	21.808		280	3.053		570	6.215	<u> </u>	8.2 <	0.089
2.5	2 :	April	2 6	~	21	0.751		170	1.748		4	0.195		52		٧	8.2 <	0.084
22	2 :	April	77	v	2	0.757		300	3.111		77	0.456		80		<b>v</b>	8.2 <	0.085
23	2	April	37	~	2	0.780	_	<u>&amp;</u>	8.440		110	1.13	_	220	2,350	<b>v</b>	8.2 <	0.088
54	200	April	-	v	3 4	0.797		710	7.755		100	1.092		200		<b>v</b>	8.2 <	0.090
(Duplicate) 10 18		April	12	٧	24	1.067		120	1.753		18	0.263		33	0.482	~	8.2 <	0.120
(Duplicate) 15	18	April	5	~	73 <	1.149		1100	17.319		150	2,362		310	4.881	•	8.2 <	0.129
Painter UN	18	April	Ξ	~	73 <	1.265	**	1700 **	29.450		230	3.984		740	7.622	<b>v</b>	8.2 <	0.142
Painter OH		April	34	~	72 ~	0.881	<u> </u>	> 02	0.241	~	8.2 <	00.0	,	> 00	170 0	`	0	000
B ack	•	-											,	>4		,	7 3.0	0.03

Painter UH = Underneath painter respirator hood. Painter OH = Outside painter respirator hood.

•	Sample (min) 60.0 61.0 26.0 73.0 71.0 70.0 70.0 70.0 70.0 70.0 70.0 70	Sample ((/min) (1.543 1.369 1.	3 STP (1) (2) 93.6 × < 80.5 × < 37.7 × < 96.9 ×	2-Butanone (MEK)	CMEKO											
Date  18 April	(min) 60.0 60.0 70.0 73.0	(/min) 1.543 1.305 1.369 1.369 1.394				Ethyl Acetate	etate		2-Butanol		J-C	n-Butanol		Metho	Methoxyacetone	
1 18 April 3 18 April 5 18 April 6 18 April 7 18 April 10 18 April 10 18 April 11 18 April 12 18 April 13 18 April 14 18 April 14 18 April 15 18 April		1.543 1.305 1.433 1.369 1.394	×××××	(ug/tube)	(mg/m3)	(ug/tube)	(mg/m3)	(Gng)	(ug/tube) (i	(mg/m3)	(ug/tube)		(mg/m3)	(ug/tube)	;) (mg/m3)	ري ا
18 April 18 April 18 April 18 April 18 April 18 April 18 April 18 April 18 April		1,305	××××	> 02	0.214	> 02	0.214		21 <	0.224	· · ·	> 12	0.224	ıñ v	, ,	0.598
18 April 18 April 18 April 18 April 18 April 18 April 18 April 18 April		1.433	$\times \times \times$	> 02	0.248	> 02 >	0.248	٧	> 12	0.261		> 12	0.261	> 5	<b>v</b>	0.695
18 April 18 April 18 April 18 April 18 April 18 April 18 April 18 April		1.369		> 02	0.531	> 02 >	0.531	٧	> 12	0.557	·•	21 <	0.557	> 29	v	788
18 April 18 April 18 April 18 April 18 April 18 April 18 April		1.394		38	0.392	> 02 >	0.206	<b>v</b>	> 12	0.217	v	× 12	0.217	٠ د	v	578
18 April 18 April 18 April 18 April 18 April 18 April 18 April		1.426		9	0.631	> 02 >	0.194	<b>v</b>	21 <	0.204	v	<b>51</b> ×	0.204	۰ کر د	v	544
18 April 18 April 18 April 18 April 18 April 18 April				88	0.273	> 50 <	0.195	v ·	× ;	0.205	· ·	, v	0.205	× ×	v 1	597
18 April 18 April 18 April 18 April 18 April		100.1	4.0.4 4.0.4 4.0.4	* *	0.43/	2 2	0.200	/ V	21 ×	0.2.0	· ·	· ·	0.221	, v	, v	88.
18 April 18 April 18 April 18 April		1.147		350	4.310	× 20 ×	0.246	· •	21 <	0.259		21.	0.259	> 56	•	9
18 April 18 April 18 April 18 April	_	0.981	71.4 x	2	0.980	> 02 >	0.280	<b>v</b>	> 12	0.294	· · ·	> 12	0.294	,	v	784
18 April 18 April 18 April		1.315	× 4.46	110	1.165	> 02 >	0.212	~	> 12	0.222	· •	> 12	0.222	> 56	v	.593
18 April 18 April	_	1.279	× 9.06	82	0.905	> 02 >	0.221	٧	> 12	0.232	· · ·	> 12	0.232	,	<b>v</b>	618
18 April	_	1.346	98°0 X**	** 0061	19.382	> 02 >	0.204	<b>v</b>	> 12	0.214	v	21 <	0.214	Ň	<b>v</b>	.571
		1.344	96.5 ×	530	5.491	> 02 >	0.207	<b>v</b>	> 12	0.218	v	× 12	0.218	Š.	v	.580
18 April	_	76.0	× 9.99	210	3.155	> 02 >	0.300	<b>v</b>	> 12	0.316	v	× 12:	0.316	v v	v	75
18 April	7 69.0	1.356	× 9°96	270	2.853	× 50 ×	0.211	<b>v</b> .	7 7	0.222	· ·	· ·	0.222	v ,	v	295
18 Apr 1		1.34	× 0.79	2100	615.12	× ×	0.502	v 1	V 12	0.613	v		0.00	ň ử	, ,	787
18 April	27.0	1.51	80.0 X	200	580	2 5	0.264	, v	7 7	0.256	, v	, <u>, , , , , , , , , , , , , , , , , , </u>	0.256	2, 2	/ v	0.682
18 April		1.314	91.7 x	430	4.689	× 02 ×	0.218	~	21 <	0.229		<b>21 ×</b>	0.229	٠ د	v	611
18 April	_	1.317	97.2 x	920	9.460	> 20 >	0.206	v	21 <	0.216	· ·	> 12	0.216	Š	•	576
18 April	_	1.324	× 7°96	190	1.970	> 02 >	0.207	~	> 12	0.218	· •	21 <	0.218	v v	, v	581
18 April	_	1.322	93.6 x	180	1.923	> 02 >	0.214	~	> 12	0.224	· ·	21 <	0.224	š v		0.598
	7 70.0	1.293	91.6 x	150	1.638	> 02 >	0.218	٧	> 12	0.229	·•	21 <	0.229	v ĭŇ	° ·	612
4 CO ( 4 CO )	21.0	0 053	× 7.89	140	2.046	110	1.607	٧	>12	0.307	~	> 12	0.307	v.	٧	818
April		0.01	63.5 x	200	3,149	> 20 >	0.315	~	21 <	0,331	v	21 <	0.331	× 55	•	885
	_	1.297	57.7 x	1000	17.324	> 02 >	0.346	<b>v</b>	> 12	0.364	•	> 12	0.364	> 56	•	0.970
18 April	-	1.3	82.8 x <	> 02	0.241	<b>&gt;</b> 02 <b>&gt;</b>	0.241	~	> 12	0.253	· •	21 ×	0.253	v v	•	929
18 April		-	0.0 × ×	20	K/A	<b>\$</b>	N/A	·	21	W/W	· •	7	K/A	v v		N/A

Painter UH = Underneath painter respirator hood. Painter OH = Outside painter respirator hood.

Travis AfB Date: Start Time: Stop Time:	18 April, 10:02 11:02	1991													
		Samole	- :	Total Xylenes	lenes		PMGE Acetate	tate	2-Ethox	yethyl	2-Ethoxyethyl Acetate	2-M	2-Methoxyethyl Ether	Ether	Totals
Site Location	Date	Number (ug/tube)	ĝ	/tube)	(mg/m³)		(ug/tube)	(mg/m3)	(ug/tube)	(aqn	(mg/m3)	2	(ug/tube) (	(mg/m3)	(mg/m3)
		_	-			_									
-		- 52 -	<u>~</u>	8.2 <	0.088	٧	> 02	0.214	٧	> 1.5	0.438	٧	> 75	0.577	< 4.171059
~		50	~	8.2 <	0.102	٧	> 02	0.248	٧	× 1.7	0.509	٧	> 75	0.671	< 4.850909
m		13	×	8.2 <	0.218	٧	> 02	0.531	<b>v</b>	<b>* 1 *</b>	1.088	v	24 <	1.433	< 10.36439
4		31	~	8.2 <	0.085	v	> 02	0.206	<b>v</b>	× 1.4	0.423	<b>~</b>	> 75	0.557	2,723539
S	18 April	16	~	8.2 <	0.080	٧	> 02	0.194	٧	> 17	0,398	٧	> 75	0.525	0.631479
•		25	٧	8.2 <	0.080	٧	> 02	0.195	<b>v</b>	<b>41 &lt;</b>	007.0	v	> 75	0.527	0.507758
~		28	~	8.2 <	0.085	٧	> 02	0.208	٧	<b>~ 1 7</b>	0.425	•	> 75	0.560	2.656532
60	18 April	33	~	8.2 <	0.086	~	> 02	0.210	٧	× 15	0.431	v	> 75	0.567	4.369796
6		23	~	8.2 <	0.101	٧	> 02	0.246	<b>v</b>	× 1.5	0.505	v	> 75	0.665	5.134591
10	18 April	19	v	8.2 <	0.115	٧	> 02	0.280	<b>v</b>	<b>* 1 *</b>	725.0	٧	> 75	0.756	2.939335
-	18 April	32	~	8.2 <	0.087	*	> 02	0.212	v	× 1.5	0.434	~	> 75	0.572	8.820479
12		18	~	8.2 <	0.091	v	> 02	0.221	<b>v</b>	× 14	0.453	~	> 75	0.596	7.806963
5		56	<u> </u>	8.2 <	780°0	٧	> 02	0.204	<b>v</b>	<b>* 1 *</b>	0.418	<b>v</b>	> 75	0.551	23.45269
14	18 April	51	~	8.2 <	0.085	v	> 02	0.207	<b>v</b>	41 <	0.425	v	> 75	0.559	12,17339
15		38		16	0.240	٧	> 02	0.300	<b>v</b>	<b>41</b> <	0.616	٧	> 75	0.811	26.98433
92		_		20	0.211	٧	> 02	0.211	<b>v</b>	× 1,5	0.433	٧	> 75	0.571	24.09114
17	18 April	_	~	8.2 <	0.084	v	> 02	0.205	<b>v</b>	× 15	0.420	v	> 75	0.553	25.58659
82		_	_	6.6	0.104	٧	> 02	0.209	٧	× 1.5	0.429	v	> 75	0.566	27.85873
19		35		33	0.405	٧	> 02	0.244	<b>v</b>	<b>41</b> ×	0.500	٧	> 45	0.658	46.82553
50		_	_	5	0.316	٧	> 02	0.218	<b>v</b>	<b>41 ×</b>	0.447	٧	> 75	0.589	36.08141
21		_	<b>v</b>	8.2 <	0.084	٧	> 02	0.206	<b>v</b>	<b>* 1 *</b>	0.422	v	> 45	0.555	11.66099
22		22	~	8.2 <	0.085	٧	<b>50 ×</b>	0.207	<b>v</b>	× 15	0.425	<b>v</b>	54 ×	0.560	6.367650
23	18 April	37		2	0.107	٧	> 02	0.214	٧	41 <	0.438	v	24 <	0.577	13.99500
57	18 April	7	v	8.2 <	060°0	٧	> 02	0.218	<b>v</b>	v 14	0.448	v	> 75	0.590	12.67047
(Duplicate) 10	18 April		٧	8.2 <	0.120	٧	20 <	0.292	· ·	× 17	0.59		> 75	0.789	6.151232
(Duniticate) 15	18	_		16	0.252	٧	20 <	0.315	٧	> 17	979 0	~	> 75	0.850	27, 96300
Painter UH	8	_		ħ	0.260	٧	20 <	0.346	•	· 17	0.710	· •	> 75	0.935	58.64045
Painter OH	18 April	35	~	8.2 <	0.099	٧	20 <	0.241	~	× 1.7	0.495	~	54 4	0.652	< 0.823250
	18 April		~	8.2	N/N	~	20	N/A	٧	17	V/N		54	X/X	N/N
		-		!			-		_	:					

Painter UH = Underneath painter respirator hood. Painter OH = Outside painter respirator hood.

Booth: STP T= 67.7 P=29.92 "Hg P= 29.88 T=68 °F

		_	_	: —	_	_	_	_	_	_		_	_	_
	tate	6 1 1 1 1	(mg/m3)	· · · · · · · · · · · ·	0.521560	0.347380	N/N	0.315004	0.306326	0.316799	0.368078	0.324819	0.381078	0.480884
	Ethyl Acetate	1 1 1 2 1 1	(ug/tube)		20 <	> 02	> 02	<b>50 ×</b>	> 02	> 02	> 02	> 02	20 <	> 02
		i i	3		<b>v</b>	<b>v</b>	<b>v</b>	v	v	<b>v</b>	<b>v</b>	<b>v</b>	<b>v</b>	v
	(MEK)		(mg/m3)	_	1.486446	0.851082	N/A	3.622552	0.306326	0.316799	1.435507	2.760967	4.382403	5.770617
	2-Butanone (MEK)		(ug/tube)		25	67	> 02	230	20 <	20 <	78	170	230	240
	_	_	_	_	-	_	<u> </u>	_	<u> </u>	<u> </u>	_	_	_	
Volume	Collected	a stp	3	; ; ; ;	38,35	57.57	0.00	63.49	65.29	63.13	54.34	61.57	52.48	41.59
	Volume	Sampled  Flowrate  Collected   a STP	(3)		38.38	57.62	0.00	63.54	65.34	63.18	54.38	61.62	52.52	41.62
	Sample   Volume	Flowrate C	(1/min)   (1)	-	1.066	1.067	0	1.059	·		Ì	·	0.991	0.991
	Time   Sample	Flowrate	(min) (cc/min)	-	36.00   1066.00	11067.000	0.000	11059,000	11089,000	60.00   1053.00	1026.00	1027.000	991.00	42.00   991.000
	Time	Sampled	(min)	1	36.00	54.00	0.00	00.09	60.00	00.09	53.00	00.09	53.00	45.00
		ACUREX #		. –	12993	9662	5666	2002	12994	10994	8383	12015	11050	12995
		Sample ACUREX	Number			. <del>.</del>	75	*	101		1 40F	205	75F	
			Date		16 April	16 April	17 April	17 Anril	17 April	17 April	118 April	118 April	10 Anril	119 April
			tion	-	10:30	14:45	Rlank	10.00	16.00	Arm Dim	11.00	17.00	11.30	15:00
			Site Location		Exhanct Duct 10:30   16 April	Exhaust Duct 14:45  16 April	Exhaust Duct Blank 17 April	Exhaust Dict 10.00 117 April	Exhaust Duct, 16:00   17 April	Exhanst Duct, 10:00   11 April	Cohoust Duct 11-00 118 April	Exhaust Duct 17:00 118 April	Exhaust Dict 11:30 10 April	Exhaust Duct, 15:00  19 April

		2-Butanol	lou	9-u	n-Butanol		Meth	Methoxyacetone	etone	Ethox	Ethoxyethanol		-Methyl-	2-Penta	4-Methyl-2-Pentanone(MIBK)
		****				:			-	1 1 1 1 1 1	* * * * * * * * * * * * * * * * * * * *	_ :		2	
Site Location	Date	(ug/tube) (mg/m3)	(mg/m3)	(ug/tube) (mg/m3)	(ex	mg/m3)	(ug/tı	(əqr	(ug/tube) (mg/m3)	(ug/tub	(ug/tube) (mg/m3)	13)	(ug/t	(ug/tube)	(mg/m3)
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1											* * * * * * * * * * * * * * * * * * *	-	1 5 1 0 1 1		
Exhaust Duct, 10:30  16 April   <	16 April		21 < 0.547638	•	11 < 0	21 < 0.547638	<b>v</b>	> 99	56 < 1.460368	٧ >	73 < 1.903694	3694	<b>v</b>	> 02	0.521560
Exhaust Duct, 14:45   16 April	16 April	· ·	21 < 0.364749	v	21 < 0	0.364749	<b>v</b>	> 99	0.972666	٧ >	73 < 1.267939	1939		210	3.647498
Exhaust Duct, Blank   17 April	17 April	< 21 <	N/A	< <	21 < N	N/A	<b>v</b>	> 99	56 < N/A	7	73 × N/A	-	v	> 02	N/A
Exhaust Duct, 10:00  17 April	17 April	< 21 <	0.330754	~ ~	21 < 0	0.330754	<b>v</b>	> 99	0.882012	<b>~</b>	73 < 1.149766	9426		93	1.464771
Exhaust Duct, 16:00  17 April	117 April		21 < 0.321643	٧ ٧	21 < 0	0.321643	<b>v</b>	> 99	56 < 0.857714	۷ >	73 < 1.118092	3092		48	0.735184
Exhaust Duct, 4pm Dup 17 April	17 April	~	21 < 0.332639	×	21 < 0	0.332639	<b>v</b>	> .95	56' < 0.887038	<b>'</b>	73 < 1.156317	5317		82	1.298877
Exhaust Duct, 11:00   18 April	118 April	•	21 < 0.386482	C3	21 < 0	0.386482	<b>v</b>	> 99	56 < 1.030620	<b>2</b>	73 < 1.343487	3487		230	4.232905
Exhaust Duct, 17:00   18 April	18 April	v	21 < 0.341060	7	11 < 0	21 < 0.341060	<b>v</b>	> 95	56 < 0.909495	< >	73 < 1.185591	5591		180	2.923376
Exhaust Duct, 11:30  19 April   <	119 April		21 < 0.400132	×	11 < 0	21 < 0.400132	<b>v</b>	> 99	56 < 1.067019	<b>~ ~</b>	73 < 1.390936	936		001	1.905392
Exhaust Duct, 15:00  19 April  <	119 April		21 < 0.504929	×	11 < 0	21 < 0.504929	•	> 95	56 < 1.346477	× 7	73 < 1.755229	5229		88	2.067804

(ug/tube) (mg/m3)   (ug/tube) (mg/m3)   (ug/tube)     < 20 < 0.521560   < 8.2 < 0.213839   < 8.2 <		_	Toluene	ne –		Butyl Acetate	tate	_	Ethylbenzene	zene	_	Total Xylenes	enes	_	PMGE Acetate	tate
(ug/tube) (mg/m3)   (ug/tube) (mg/tube) (mg/tube) (mg/tube) (mg/tube) (mg/tube) (mg/					-		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	_		8 8 8	_			_		1 t t t t t t t t t t t t t t t t t t t
21 0.547638   < 20 < 0.521560   < 8.2 < 0.213839   <	Site Location		(ug/tube)	(mg/m3)	ž	1/tube)	(mg/m3)	_	(ug/tube)	(mg/m3)	_	(ug/tube)	(mg/m3)	_	(ug/tube) (mg/m3)	(mg/m3)
21 0.547638   < 20 < 0.521560   < 8.2 < 0.213839   < 8.2 < 0.503702   53 0.920559   < 8.2 < 0.142426   < 8.2 < N/A   < 20 < N/A   < 8.2 < N/A   < 8.2 < N/A   < 10.330754   < 8.2 < 0.129151   < 10.330754   < 8.2 < 0.129151   < 10.330754   < 8.2 < 0.129151   < 10.350759   < 8.2 < 0.12987   < 10.350759   < 8.2 < 0.129887   < 10.369279   < 10.336799   < 8.2 < 0.129887   < 10.341060   39 0.633398   < 8.2 < 0.150912   < 10.341060   39 0.633398   < 8.2 < 0.150912   < 10.341060   39 0.633398   < 8.2 < 0.150542   < 11.024486   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.1504266   < 8.2 < 0.150426   < 8.2 < 0.150426   < 8.2 < 0.150426   <	0 0 1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0					1		<u> </u>	* * * * * * * * * * * * * * * * * * *		-	0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0	_	5 2 6 6 6 6 6 6 6 6	
29 0.503702   53 0.920559   < 8.2 < 0.142426   <	xhaust Duct. 10:30	116 April	21	0.547638	<b>v</b>	> 02		<u> </u>	8.2 <	0.213839	<u>~</u>	8.2 <	0.213839	<u> </u>	> 02	0.521560
< 8.2 < N/A   < 20 < N/A   < 8.2 < N/A   < 8.2 < 0.129151   < 27 0.425256   21 0.330754   < 8.2 < 0.129151   < 8.2 < 0.129151   < 10 0.153163   < 20 < 0.316799   < 8.2 < 0.125593   < 8.2 < 0.125593   < 8.2 < 0.125693   < 8.2 < 0.129887   < 8.2 < 0.129887   < 8.2 < 0.129887   < 8.2 < 0.129887   < 8.2 < 0.129887   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   < 8.2 < 0.150912   <	xhaust Duct. 14:45	116 April	58				0.920559	<u>~</u>	8.2 <	0.142426	<u>~</u>	8.2 <	0.142426	<u>~</u>	> 02	0.347380
27 0.45526	xhaust Duct. Blank	117 April			_	> 02		<u> </u>	8.2 <	N/A	<u> </u>	8.2 <	N/A	<u>~</u>	> 02	20 < N/A
10 0.153163   < 20 < 0.306326   < 8.2 < 0.125593   <	xhaust Duct, 10:00	117 April				12	0.330754	<u>~</u>	8.2 <	0,129151	<u> </u>	8.2 <	0.129151	<u> </u>	> 02	0.315004
17 0.269279   < 20 < 0.316799   < 8.2 < 0.129887   <   35 0.644137   61 1.122640   < 8.2 < 0.150912   <   21 0.341060   339 0.633398   < 8.2 < 0.133176   <   13 0.247701   27 0.514456   < 8.2 < 0.156242   <   4 0.577061   <   8.2 < 0.197162   <   4 0.577061   <   8.2 < 0.197162   <   4 0.577061   <   8.2 < 0.197162   <   4 0.577061   <   8.2 < 0.197162   <   4 0.577061   <   8.2 < 0.197162   <   4 0.577061   <   8.2 < 0.197162   <   4 0.577061   <   8.2 < 0.197162   <   4 0.577061   <   8.2 < 0.197162   <   4 0.577061   <   8.2 < 0.197162   <   4 0.577061   <   8.2 < 0.197162   <   4 0.577061   <   8 0.54706   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061   <   9 0.547061	xhaust Duct. 16:00	117 April	10	0.153163	<u> </u>	> 02	0.306326	<u>~</u>	8.2 <	0.125593	<u> </u>	8.2 <	0.125593	<u>~</u>	> 02	0.306326
35 0.644137   61 1.122640   < 8.2 < 0.150912   <	Exhaust Duct 4cm Duc	117 April	17	0.269279	~	> 02		<u> </u>	8,2 <	0.129887	<u> </u>	8.2 <	0.129887	<u> </u>	> 02	0.316799
21 0.341060   39 0.633398   < 8.2 < 0.133176   <	Exhaust Duct. 11:00	118 April	33	0.644137		19	1,122640	<u>×</u>	8.2 <	0.150912	<u> </u>	8.2 <	0.150912	<u> </u>	> 02	0.368078
13 0.247701   27 0.514456   < 8.2 < 0.156242   <	Exhaust Duct. 17:00	118 April	1 21	0.341060		39	0.633398	<u>×</u>	8.2 <	0.133176	<u> </u>	8.2 <	0.133176	<u>~</u>	> 02	0.324819
11 0.264486   24 0.577061   < 8.2 < 0.197162   <	Exhaust Duct, 11:30	119 April		0.247701		27	0.514456	<u> </u>	8.2 <	0.156242	<u>×</u>	8.2 <	0.156242	<u> </u>	× 20 20	0.381078
	Exhaust Duct, 15:00	119 April	=	0.264486	_	54	0.577061	<u>×</u>	8.2 <	0.197162	<u> </u>	8.2 <	0.197162	<u>~</u>	× 02	0.480884

		_		2-	2-Ethoxyethyl Acetate	-	cetate	_	2-Methoxyethyl Ether	yl Ether	_	
					* * * * * * * * * * * * * * * * * * *		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	_		# # # # # # # # # # # # # # # # # # #	_	
Site Location	5	_ :	Date	_	(ug/tube) (mg/m3)		mg/m <b>3</b> )	_	(ug/tube) (mg/m3)	(mg/m3)	Totals	=
				_			9 9 1 1 1 1 9	_	* * * * * * * * * * * * * * * * * * *	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-	7
Exhaust Duct, 10:30  16 April	10:30	16	April	<u> </u>	41 <		41 < 1.069198		> 75	54 < 1.408212	2.04	4
Exhaust Duct, 14:45  16 April	14:45	116	April	<u>×</u>	41 <		41 < 0.712130	Y	> 75	54 < 0.937928	5.87	~
Exhaust Duct, Blank   17 April	Blank	117	April	<u>×</u>	41 <	_	N/A	<u> </u>	> 45	N/A	2	4
Exhaust Duct, 10:00 (17 April	10:00	117	April	<u> </u>	× 1 ×		41 < 0.645759	Y	> 72		5.84	4
Exhaust Duct, 16:00  17 April	16:00	117	April	~	× 1.7	0	41 < 0.627969	٧	> 45	54 < 0.827082	0.89	6
Exhaust Duct,4pm Dup 17 April	Pa Duck	117	April	<u>×</u>	×14	0	41 < 0.649438	٧	> 45	54 < 0.855358	1.57	7
Exhaust Duct, 11:00  18 April	11:00	118	April	<u>v</u>	<b>41</b> ×	0	41 < 0.754561	٧	> 75	54 < 0.993812	7.44	4
Exhaust Duct, 17:00 [18 April	17:00	118	April	_	× 14	0	41 < 0.665880	٧	> 75	54 < 0.877013	6.65	ıc
Exhaust Duct, 11:30  19 April	11:30	13	April	<u>*</u>	> 1.7	0	41 < 0.781210	٧	> 75	54 < 1.028912	7.05	2
Exhaust Duct, 15:00   19 April	15:00	119	April	<b>Y</b>	× 1 ×	0	41 < 0.985813	٧	> 75	54 < 1.298389	89.8	00

Travis AFB NIOSH 500

Particulate

Date: 16 April 1991

Start Time: 14:48 Stop Time: 15:48

STP P=29.92 "Hg T=68 °F

Booth: **T**=

66.6 P= 29.87

						Volume			
			Time	Sample	Volume	Collected	Weight	Weight	
		Sample	Sampled	Flowrate	Collected	@ STP	Gain	Gain	
Site Location	Date	Number	(min)	(1/min)	(1)	(1)	(g)	(mg)	(mg/m3)
				1		1			
1	16 April	12	65.00	3.1	201.50	201.70	0.00016	0.2	0.793
2	16 April	15	54.00	3.02	163.08	163.24	0.00000	0.0	0.000
3	16 April	3	63.00	3.13	197.19	197.38	0.00014	0.1	0.709
4	16 April	8	62.00	3.093	191.77	191.95	0.00000	0.0	0.000
5	16 April	11	65.00	3.094	201.11	201.31	0.00009	0.1	0.447
6	16 April	19	63.00	3.098	195.17	195.37	0.00000	0.0	0.000
7	16 April	13	64.00	2.961	189.50	189.69	0.00055	0.6	2.899
8	16 April	14	62.00	3.133	194.25	194.44	0.00047	0.5	2.417
9	16 April	17	63.00	3.056	192.53	192.72	0.00021	0.2	1.090
10	16 April	16	63.00	3.059	192.72	192.91	0.00076	0.8	3.940
11	16 April	18	63.00	3.033	191.08	191.27	0.00311	3.1	16.260
12	16 April	4	62.00	3.074	190.59	190.78	0.00118	1.2	6.185
13	16 April	5	63.00	3.074	193.66	193.85	0.0008	0.8	4.127
14	16 April	9	63.00	3.068	193.28	193.47	0.00291	2.9	15.041
15	16 April	39	63.00	3.016	190.01	190.20	0.00691	6.9	36.331
16	16 April	33	62.00	3.062	189.84	190:03	0.00526	5.3	27.680
17	16 April	1	63.00	3.079	193.98	194.17	0.0143	14.3	73.648
18	16 April	37	64.00	3.077	196.93	197.12	0.00662	6.6	33.583
19	16 April	27	63.00	3.077	193.85	194.04	0.00435	4.4	22.418
20	16 April	30	62.00	3.098	192.08	192.27	0.00465	4.7	24.185
21	16 April	6	63.00	3.023	190.45	190.64	0.0002	0.2	1.049
22	16 April	2	63.00	3.076	193.79	193.98	0.00088	0.9	
23	16 April	32	63.00	3.054	192.40	192.59	0.00538	5.4	27.935
24	16 April	36	62.00	3.107	192.63	192.82	0.00201	2.0	
Painter OH	16 April	25	0.00	3.064	0.00	0.00	•	0.0	N/A
Painter UH	16 April	24	63.00	3.086	194.42	194.61	0.00000	0.0	
(Duplicate) 10			63.00	•	•	201.74		0.7	
(Duplicate) 15	16 April	35	0.00	3.178	0.00	0.00	•	0.5	
Blank	16 April	7	0.00	0	0.00	- 0.00	•	0.0	****
				1	1	0.00		0.0	
Exhaust Duct	16 April	1	l	1.067	0.00	0.00	l	0.0	

Painter OH = Outside painter respirator hood. Painter UH = Underneath painter respirator hood.

Travis AFB NIOSH 500 Particulate

Date: 17 April 1991 STP Booth:

Start Time: 16:05 P=29.92 "Hg T= 68 Stop Time: 17:18 T=68  $^{\circ}$ F P= 29.93

Volume
| Time | Sample | Volume | Collected | Weight | Weight |
| Sample | Sampled | Flowrate | Collected | @ STP | Gain | Gain |

	!		Time	Sample	Volume	Collected	Weight	Weight	
					Collected	@ STP	Gain	Gain	
Site Location	Date	Number	(min)	(1/min)	(1)	(1)	(g)	(mg)	(mg/m3)
			 		 I	· · · · · · · · · · · · · · · · · · ·		 l 1	
1	17 April	40	84.00	3.052	256.37	   256.45	0.00003	0.0	0.117
	17 April	58	70.00	3.01	210.70	210.77	0.00003	0.0 1	
	17 April	22	83.00	3.038	252.15	252.24	0.00000	0.0 *	
	17 April	34	82.00	3.102		254.45	0.00000	0.0	
	17 April	52	84.00	2.87		241.16	0.00008	0.1	- 0 0
	17 April	46	82.00	3.096	253.87		0.00000	•	
	17 April	29	83.00	2.964	246.01		0.00000		
	17 April	23	82.00	3.102	254.36	254.45	0.00042	0.4	
	17 April	43	83.00	3.045	252.74	252.82	0.00018	0.2	
	17 April	59	83.00	3.039	252.24	252.32	0.0000	0.0 *	
11	17 April	45	82.00	3.02		•	0.00095	1.0	3.835
	17 April	20	82.00	3.036	248.95			0.4	1.687
	17 April	31	82.00	3.041	249.36	249.45	0.00078	0.8	3.127
	17 April	38	82.00	3.038		249.20	•	1.8	7.183
15	17 April	`48	82.00	2.963		243.05	0.00012	0.1	0.494
16	17 April	49	82.00	3.043	249.53	249.61	0.00219	2.2	8.774
17	17 April	42	83.00	3.045	252.74	252.82	0.00218	2.2	8.623
18	17 April	44	83.00	3.071	254.89	254.98	0.00522	5.2	20.472
19	17 April	41	82.00	3.048	249.94	250.02	0.00635	6.3	25.398
20	17 April	53	82.00	3.084	252.89	252.97	0.00357	3.6	14.112
21	17 April	51	82.00	3.012	246.98	247.07	0.00044	0.4	1.781
. 22	17 April	55	82.00	3.062	251.08	251.17	0.00065	0.7	2.588
23	17 April	47	82.00	3.026	248.13	248.21	0.00115	1.2	4.633
24	17 April	21	82.00	3.05	250.10	250.18	0.00072	0.7	2.878
Painter OH	17 April	50	78.00	3.008	234.62	234.70	0.00085	0.9	3.622
	17 April	57	78.00	3.036	236.81	236.89	0.00000	0.0 *	0.000
(Duplicate) 10		66	82.00	3.16	259.12	259.21	0.00044	0.4	1.697
(Duplicate) 15	17 April	54	82.00	3.144	257.81	257.89	0.0024	2.4	9.306
		- 1				0.00	j	0.0	N/A
Blank	17 April		0.00	0	0.00	0.00	1	0.0	N/A
	17 April	1	60.00	1.053	63.18	63.20	İ	0.0	0
Exh. Duct Dup	17 April	1	60.00	1.089	65.34	65.36	1	0.0	0

Painter OH = Outside painter respirator hood.

Painter UH = Underneath painter respirator hood.

				P=29.92 "Hg T=68 "F	/olume	p= 29.87		Painter	H0 H0	onderneatu p Outside pain	ter res	idi palmier respirator hood. painter respirator hood.	ood.
-	  Sampl	Time Sample Sampled	23	Sample   Volume  C  Flowrate Collected	Collected    a STP	Lead		Zinc		Strontium		Chromium	F = 7 = 1.
Site Location	Date   Numbe	Number  (min)	((/min)	= = =	= =	aldwes/6n	m/gn :	ng/sample	e ug/m3	ng/sample	l cm/gu	ug/sampte	cııı/6n
	_		_	- 3			0 24	-	0 27	1 07		0.57	3.52
1 7				159.90	101.78	C	10.80		, ,	1.32	9.51	0.33	2.38
2 12	16 April 26	6.00	2.985	157.22	158.83	, (1)	0.01		, ,	2.49	15.65	1.23	7.73
3 1 10	April			171.47	173.49	4 1,5 4	8,65	1.5	<b>v</b>	2.60	14.99	0.77	47.4
2 - 2	April			164.78	166.71	1,5	00.6	1.5	00°6 >	2.25	13.50	1.73	10.38
	April		_	166.59	168.55	< 1.5	8.90	1.5	< 8.90	5.13	30.44	1.20	7,12
	April	_	-	156.72	158.56	< 1.5 ·	95.6	1.5	95.6 >	13.80	87.03	8.27	52.16
8 16	April			179.60	181.71	< 1,5 +	8.26	1.5	~	17.64	97.08	9.21	50.69
	Aprili	-	_	152.90	154.69	< 1.5 ·	02.6	1.5	oz°6 >	15,11	97.68	79.7	49.58
	April		_	160.65	162.54	< 1.5	6 9.23	1.5	v	69.5	35.01	2.27	13.97
	6 April 65		00   2.968	151.37	153.15	< 1.5 ·	62.6	< 1.5	•	52.11	340.26	29.52	192.76
	April	25   58.00	3.009	174.52	176.57	< 1.5 ·	8.50	< 1.5	•	32.75	185.48	18.18	102.96
_	6 April	8   52.00	3.001	156.05	157.89	< 1.5	6 9.50	1.5	<b>v</b>	25.05	158.66	13.26	83.98
14 116	April	44   53.00	00   2.989	158.42	160.28	< 1.5	9.36	1.5	<b>v</b>	28.00	174.70	18.75	10.98
15   16	April	24   56.00	_	162.96	164.87	× 1.5	o.10	5.1 > 1.5	v	146.40	887.95	81.86	496.50
16 116	April	39   58.00	_	172.20	174.23	× 1,5	8.61	1.5	v	02.001	66.50	06.70	24.700
17   16	April	10   52.00	_	156.78	158.62	× 1.5	97.6	- 1.5	<b>~</b>	59.85	1 12.778	55.72	212.38
18   16	April	00.45   19	_	_	163.52	1.5	< 9.17	· ·	<b>v</b>	147.50	20.20%	405 50	240.74
19   16	April		_	_	170.99	×	8.77	\$	6.6	170.60	10.0%	812.00	4682 00
		_	_	_	181.17	\$ 1.5	87.8	C	,	24.80	2000	12 43	87 17
_	April			143.09	144.17	C	0.30	51	, ,	15.86	96.19	6.36	38.57
	April		010.5   00		171 84		× × ×	1.5		90.29	525.42	47.10	274.09
5 2		00 1 20 00 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			170.21	4 1.5	< 8.37	1.5	٧	43.58	243.17	25.43	141.90
					170.36	× 1.5	8.80	1.5	٧	10.14	59.52	6.41	37.63
(Duplicate) 15 16 April					164.46	< 1.5	< 9.12	1.5	< 9.12	183.50	1115.76	92.88	564.73
painter IN 11		28   36.00		-	110.07	< 1.5	< 13.63	1.5	< 13.63	13.37	121.47	96.9	63.23
					93.87	< 1.5	< 15.98	1.5	< 15.98	1 27.18	289.54	16.53	176.09
	_		_	_	0.00	< 1.5	× N/A	1.5	₩ > !	1.43	 ≪	0.20	N/N
	le Aprili	1 36.00	00   1.055		9	89	8.7	 	8.7	1 54.46,	2	38.67	47

Ď.		_	ارة -	_	1.37	2.37	6.11	5.17	4.62	4.44	16.71	20.30	8.42	6.58	64.30	59.77	34.70	63.49	98	ය _	7	22	52	<u>-</u>	22.79	26.03	33	25.06	15.34	07	20	0.74		
, hoc			Cm/gu		-	2	9	2	4	4	16	2	80	9	3	20	M W	63	287.98	174.63	127.04	260.72	341.25	128.51	22	56	156.33	8	\$	232.40	168.20	0	M/A	(
th painter respirator hood painter respirator hood.		Chromium	ug/sample		0.33	0.54	1.41	1.17	0.99	1.04	3.72	4.58	1.95	1.50	14.36	13.02	7.91	14.42	63.06	38.13	29.33	59.76	77.64	29.33	5.19	90.9	35.06	20.15	3.65	53.01	16.14	0.15	0.30	1
inter r er resp			ug/m³	-	3.93	8.42	13.09	9.63	16.39	7.77	34.46	37.23	22.03	5.36	132.68	122.84	73.40	121.34	512.40	311.34	230.26	503.03	80°289	240.90	07.77	49.56	283.00	163.20	25.31	406.35	327.64	3.84	N/A	
Underneath pa Outside paint		Strontium	ug/sample		0.95	1,92	3.02	2.18	3.51	1.82	7.67	8.40	5.10	1.22	29.63	26.76	16.73	27.56	112.20	. 67.98	53.16	115.30	156.32	54.98	10.11	11.54	63.47	36.35	6.02	69.26	31.44	0.78	1.23	3
B B	_	_	ug/m3	_	6.21	6.57	6.50	6.62	7.01	6.41	6.74	6.65	6.48	6.58	6.72	6.89	6.58	09.9	6.85	6.87	6.50	9.54	6.59	6.57	6.59	95.9	69.9	6.73	6.31	6.58	15,63	7.38	NA	,
Painter UH Painter OH		Zinc	ug/sample		1.5 <	1.5 <	1.5 <	1.5 <	1.5 <	1.5 <	1.5 <	1.5 <	1.5 <	1.5 <	1.5 <	1.5 <	1.5 <	1.5 <	1.5 <	1.5 <	1.5 <	1.5 <	1.5 <	1.5 <	1.5 <	1.5 <	1.5 <	1.5 <	1.5 <	1.5 <	1.5 <	1,5 <	1.5 <	
Pal	_	2	in   £m/6n	_	6.21   <	>   75.9	>   05.9	>   29.9	>   10.7	>   17.9	>   72.9	>   59.9	>   85.9	6.58   <	6.72   <	>   68.9	>   85.9	>   09.9	6.85   <	>   28.9	>   05.9	>   95"9	>   6.59	>   25.9	>   65.9	>   55.9	>   69.9	6.73   <	6.31   <	6.58   <	15.63   <	7.38   <	<u>×</u>	-/
60.7 29.77			ng/sample ug,		1.5 < (	1,5 < (	v	1.5 < 6	1.5 < 7	1.5 < 6	1.5 < 6	1.5 < 6	v	v	<b>v</b>	¥	1.5 < 6	1.5 < 6	1.5 < 6	•	1.5 < 6	•	<b>v</b>	<b>v</b>	<b>v</b>	v	v	•	1.5 < (	1.5 < (	1.5.<	1.5 <	1.5 × M/A	
7= 6 P= 29		Lead	s/bn		~	~	¥	~	~	v	v	~	~	<b>~</b>	~	<b>v</b>	~	<b>v</b>	~	~	~	<b>~</b>	<b>~</b>	<b>~</b>	<b>v</b>	<b>v</b>	v	v	v	<b>v</b>	v	<b>v</b>	<b>v</b>	
<u>;</u>	Volume  Collected	a STP	- co	_	241.61	228.15	230.78	226.43	214.11	234.14	222.57	225.63	231.55	227.79	223.32	217.84	227.94	227.12	218.97	218.34	230.87	229.21	227.51	228.23	227.69	232.84	224.27	222.73	237.87	228.10	95.96	203.37	00.00	
P=29,92 "Hg T=68 °F	Volume  C	굣	- 0	_	239.47	226.13	228.73	254.42	212.21	232.06	220.59	223.63	229.50	225.77	221.34	215.91	252.95	225.11	217.03	216.41	228.83	227.18	225.50	226.21	225.68	230.78	222.29	220.75	235.76	226.08	95.11	201.56	0.00	
<b>.</b> -	Sample	41	(Ct/min)		3.11	3.015	3.091	3.117	2.756	3.136	2.981	3.106	3.06	3.051	3.032	3.041	3.053	3.042	2.973	3.048	3.051	3.07	3.089	3.186	3.009	3.077	3.045	3.066	3.186	3.14	3.068	3.054	0	
	Time	Sample Sampled			77.00	75.00	74.00	72.00	77.00	74.00	74.00	72.00	75.00	24.00	73.00	71.00	74.00	24.00	73.00	71.00	75.00	74.00	73.00	71.00	22.00	23.00	73.00	22.00	74.00	72.00	31.00	96.00	00.00	
	-	empte   S	Number  (min)	_	26	25	10	22	53	51	95	1 25	24	20 I	- 29	12	27	31	20	18	29	13	2	63	3 -	19	8	7	11	2	7	21	17	
10:03 11:59	-	Se	Date	-	17 April				17 April	17 April	17 Aprili	17 April	17 April	17 April	17 April				17 April	17 April	17 April	17 April	17 April	17 April	17 April	17 April								
Start Time: 1 Stop Time: 1			Site Location		-	2	м	4	2	9	7	8	_	101	_	12	13	14	15	16	1.21	18	_		_	_	23	54	(Duplicate)10 17 April	(Duplicate) 15 17	Painter UH	Painter OH	Blank	

Travis AFB

Isocyanates

Date: 19 April, 1991

Start Time: 11:26 Stop Time: 12:26

Booth: STP:

T= 64.3 P=29.92 "Hg

P= 29.8 T=68 °F

						Volume		
		1	Time	Sample	Volume	Collected	HMDI	HMDI
	1	Sample	Sampled	Flowrate	Collected	@ STP	per Filter	Concentration
Site Location	Date	Number	(min)	(1/min)	[ (1) [	(1)	(ug)	(ug/m3)
		1						
	19 April	8	66.0		: :	205	< 1.0	< 4.9
	19 April	6	55.0		: :	183	< 1.0	< 5.5
3	19 April	2	65.0	3.048	198	199	< 1.0	< 5.0
4	19 April	4	64.0	3.115	199	200	< 1.0	< 5.0
5	19 April	20	66.0	3.069	203	204	< 1.0	< 4.9
6	19 April	14	64.0	3.144	201	202	< 1.0	< 4.9
7	19 April	7	64.0	3.015	193	194	< 1.0	< 5.2
8	19 April	13	61.0	3.094	189	190	< 1.0	< 5.3
9	19 April	22	65.0	3.160	205	207	< 1.0	< 4.8
10	19 April	23	64.0	3.069	195	198	< 1.0	< 5.1
11	19 April	51	64.0	3.158	202	203	< 1.0	< 4.9
12	19 April	43	63.0	3.112	196	197	< 1.0	< 5.1
13	19 April	15	65.0	3.125	203	204	< 1.0	< 4.9
14	19 April	5	64.0	3.149	202	203	< 1.0	< 4.9
15	19 April	59	64.0	3.167	203	204	1.3	6.4
16	19 April	58	63.0	3.119	196	198	1.0	5.1
17	19 April	34	65.0	3.136	204	205	< 1.0	< 4.9
18	19 April	18	64.0	3.120	200	201	1.5	7.5
	19 April	19	64.0	3.131	200	202	2.5	12.4
	19 April	9	63.0	3.162	199	200	2.2	11.0
	19 April	21	65.0	3.120	203	204	< 1.0	< 4.9
	19 April	25	64.0		202	203	< 1.0	< 4.9
23	19 April	1	64.0		200	201	< 1.0	< 5.0
24	19 April	35	63.0	:		199	< 1.0	< 5.0
Exhaust Duct	19 April	10	55.0		174	175	< 1.0	< 5.7
(Duplicate) 10		11	64.0		:	201	< 1.0	< 5.0
	19 April	24	64.0	:		203	1.6	7.9
Painter UH	19 April	54	65.0			204	< 1.0	< 4.9
Painter OH	19 April	41	65.0		202	203	< 1.0	< 4.9
Blank	19 April	16	0.0		N/A	N/A	< 1.0	N/A
Diana	-5 April			","	,		i	i i
Exhaust Duct	19 April	Tube	53.0	0.991	53	53	i	i i

Painter UH = Underneath painter respirator hood. Painter OH = Outside painter respirator hood.

Travis AFB

Isocyanates

Date:

19 April, 1991

Start Time: 15:15 Stop Time: 16:00

Booth: T= 65.6

STP P=29.92 "Hg

P= 29.88

T=68 °F

Va	ume

							Volume					
					Sample	Volume	Collected	н	MDI	1	HMDI	
	I					Collected	Ø STP	per	Filter	Conc	entration	٦İ
Site Location		Date	Number	(min)	[ (]/min)	(1)	(1)	1 (	ug)		ug/m3)	i
										1		1
		April	26	49.0	3.105	152	153	<	1.0	<	6.6	İ
2		9 April	17	40.0	3.341	134	134	<	1.0	<	7.5	ĺ
		April	*	47.0	3.012	142	142	<	1.0	j <	7.0	i
4	-	April	•	46.0	3.041	140	140	<	1.0	<	7.1	İ
5		April	*	48.0	3.057	147	147	<	1.0	<	6.8	İ
		April	•	47.0	3.133	147	148	<	1.0	<b> </b> <	6.8	i
7	119	April	53	47.0	3.019	142	142	<	1.0	· <	7.0	i
		April	31	45.0	3.103	140	140	<	1.0	<	7.1	i
		April	46	48.0	3.132	150	151	<	1.0	<	6.6	i
	-	April	48	47.0	3.044	143	144	<	1.0	<	7.0	i
11	19	April	30	47.0	3.035	143	143	<	1.0	<	7.0	i
	•	April	37	46.0	3.116	143	144	<	1.0	· <	7.0	i
	-	April	12	47.0	3.118	147	147	<	1.0	<	6.8	i
		April	47	47.0	3.143	148	148	<	1.0	<	6.7	į.
		April	32	46.0	3.176	146	147		1.2	İ	8.2	i
	•	April	33	46.0	3.155	145	146	<	1.0	<	6.9	İ
		April	38	47.0	3.128	147	147	<	1.0	<	6.8	İ
		April	42	47.0	3.133	147	148	<	1.0	<	6.8	Ĺ
		April	40	47.0	3.120	147	147		2.8		19.0	İ
		April	52	45.0	3.159	142	143	<	1.0	<	7.0	Ì
		April	3	47.0	3.109	146	147	<	1.0	<	6.8	i
		April	55	47.0	3.150	148	149	<	1.0	<	6.7	i
	:	April	28	46.0	3.131	144	144	<	1.0	<	6.9	i
	-	April	49	46.0	3.128	144	144	<	1.0	<	6.9	İ
		April	36	42.0	3.159	133	133	<	1.0	<	7.5	İ
Exh. Duct Dup.			44	42.0	3.129	131	132	<	1.0	<	7.6	İ
Exh. Duct Blnk			27	42.0	N/A	N/A	N/A	<	1.0		N/A	İ
(Duplicate) 10			70	47.0	3.130	147	148	<	1.0	<	6.8	ĺ
(Duplicate) 15	19	April	50	46.0	3.168	146	146		1.3		8.9	İ
	19	April	72	48.0	3.098	149	149	<	1.0	<	6.7	İ
	19	April	71	48.0	3.185	153	153	<	1.0	<	6.5	
Blank	19	April	56	0.0	N/A	N/A	N/A	<	1.0		N/A	ĺ
				1	1		İ		j			İ
Exhaust Duct	19		Charcoal	42.0	0.991	42	42					
			Tube	1		1	1		j			

Painter UH = Underneath painter respirator hood. Painter OH = Outside painter respirator hood.

## APPENDIX G REDUCED DATA FOR THE POSTMODIFICATION TEST SERIES

	10	
2	XYLENE: (ug)	20.6 100 100 100 100 100 100 100 10
PAGE 1 OF	ETHYL BENZENE (ug)	
AT	BUTYL ACETATE (ug)	nd 22 25 25 25 25 25 25 25 25 25 25 25 25
GRAY TOPCOAT	TOLUENE (ug)	nd 69 878 878 899 105 115 115 115 116 110 110 110 110 110 110 110 110 110
PRIMER, G RAMP	MIBK (ug)	nd nd nd nd nd nd nd nd nd nd nd nd nd n
T GREEN AUXILIARY	MEK (ug)	nd 183 nd 184 nd 185 nd
PAINT: 0BJECT: /	RUN TIME (min)	23222222222222222222222222222222222222
TS 8485	POST-CAL (ml/min)	1003 1003 1003 1003 1003 1003 1003 1003
AFB 300TH TES PROJECT	RE-CAL ml/min)	1010 1010 1000 1000 1000 1000 1000 100
TRAVIS AFB PAINT BOOTH T ACUREX PROJEC	PUMP #	2252 2252 2252 2362 2362 2362 2373 2373 2373 2373 237
#1	ACUREX SAMPLE #	90045384 90045885 90045886 90045886 90045886 90045886 900457884 90047584 90047586 90047586 90044384 90044788 90044384 90044384 90044384 90044384 90044384 90044388 90044384 90044388 90044384 90044388 90044388 90044384 90044388 90044388 90044388 90044388 90044388 90044388 90044388 90044388
ORGANICS #1 06-16-92 NIOSH 1300	ACUREX TUBE #	2222 2222 2322 2333 333
TEST: C DATE: C METHOD: N	GRID LOC	10 23 33 11 11 11 11 11 11 11 12 13 14 14 15 16 17 18 18 18 18 18 18 18 18 18 18 18 18 18

BN & LJL LJL	XYLENES (mg/M3)		
. 2 ALS: ALS:	ETHYL BENZENE (mg/M3)	######################################	
PAGE 2 OF 2 D E INITIALS: Q A INITIALS:	BUTYL ACETATE (mg/M3)	A MO 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	A W W W W W W W W W W W W W W W W W W W
	TOLUENE (mg/M3)		<pre></pre>
#1 0	MIBK (mg/M3)	> \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\	21.8 25.2 25.2 25.2 25.3 25.3 4 ADL 6 ADL 6 ADL 6 ADL 6 ADL 6 ADL 6 ADL 6 ADL 6 ADL 6 ADL 7 ADL 7 ADL 8 ADL
	MEK (mg/M3)	> > 5	5
	AVG FLOW (L/MIN)	1.011 1.013 1.002 1.002 1.003	1.010 1.010 1.010 1.010 1.018 1.018 1.018 1.007 1.007 1.020
	ACUREX SAMPLE #	90044384 90044384 90045685 90045686 90044586 90044586 90047182 90047182 90047384 90047384 9004788 9004788 90044182 90044182 90044182	90047889 90049788 90049788 90049182 90049483 90049483 90048384 90048384 90048386 90048788
ORGANICS #1 06-16-92 NIOSH 1300	ACUREX TUBE #	11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	35 27 7 6 7 7 6 7 7 8 8 8 8 8 8 8 8 8 8 8 8
TEST: 0 DATE: 0 METHOD: N	GRID LOC	11282222222222222222222222222222222222	P over 1A 2A 3A 1B 2B 2B 2B 2B 2B 2B 2B 2B 2B 2B 2B 2B 2B

INLET GRID B field Blank < MDL 1.6 4.4 3.5 1.5 D E INITIALS:BN & LJL Q A INITIALS:LJL ₽ ¥ 9 2 8 EXHAUST DUCT: RECIRC DUCT: 10.1 8.6 8.8 GRID HOL: 0.0115 mg/SAMPLE PAINTER MOL: 0.0115 mg/SAMPLE · MOL 2 4 **3**0 4 12 9 54 5.6 11.5 11.6 5.4 13.4 15 < MDL **EXHAUST GRID** Ξ 49 ຊ TRAVIS AFB
PAINT BOOTH TESTS
ACUREX PROJECT 8485 OSHA TUA:590 mg/H3 0.2 2.7 5.1 4.5 9.4 2.8 PAINT TYPE: LT GREEN PRIMER, GRAY TOP UNITS: Mg/M3 0 22 # 2 N • 2.6 2.4 2.2 2.7 2.4 1.9 2 17 2 OBJECT: AUXILIARY RAMP Painter Over 0.4 INLET GRID A Painter Under < MDL ORGANICS #1 DATE: 06-16-92 METHOD: NIOSH 1300 GRID CHART 1 - MEK 1.9 1.9 2.1 ¥ ঠ ≨

. . . . . . . . . . . . . . . . . INLET GRID B Field Blank < MDL 5.8 2.2 2.3 # YOF > D E INITIALS:BN & LJL Q A INITIALS:LJL RECIRC DUCT: < MOL . 8 EXHAUST DUCT: 7.3 0.2 GRID MOL: 0.0095 mg/SAMPLE PAINTER MOL: 0.0095 mg/SAMPLE 3.2 1.0 4.9 . ₩DL 2 2 42 54 4.8 9.8 3.5 8.4 2.8 15 \* MOL 4 **EXHAUST GRID** = ສ TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485 OSHA TWA: 205 mg/H3 9.4 5.6 38.6 4.5 2.7 PAINT TYPE: LT GREEN PRIMER, GRAY TOP UNITS: Mg/H3 2.5 18 2 14 25 9 ~ 9.04 4.0 5.6 5.9 3.7 4.4 ₽ 4 2 OBJECT: AUXILIARY RAMP Painter Over 21.8 . . . . . . . . . . . . . . . ORGANICS #1 DATE: 06-16-92 METHOD: NIOSH 1300 Painter Under < MDL INLET GRID A GRID CHART 2 - MIBK 25.6 29.7 22.5 ¥ న ž

. . . . . . . . . . . . . . INLET GRID B Field Blank < MDL 0: D E INITIALS:BN & LJL Q A INITIALS:LJL -0.7 18 • PDL RECIRC DUCT: < MOL 38 恕 EXHAUST DUCT: 5.9 3.3 3.3 1.4 GRID MOL: 0.0114 mg/SAMPLE PAINTER MOL: 0.0114 mg/SAMPLE 교 왕 \* 2 2 24 1.2 1.5 2.3 · HOL **EXHAUST GRID** 5 4 = 23 TRAVIS AFB
PAINT BOOTH TESTS
ACUREX PROJECT 8485 OSHA TWA:375 mg/N3 4:0 1.2 1.3 5.7 2.0 2.5 mg/H3 13 9 22 4 9 ~ PAINT TYPE: LT GREEN PRIMER, GRAY TOP UNITS: 1.2 1: 1.6 2.1 5.4 1.7 2 17 21 OBJECT: AUXILIARY RAMP GRID CHART 3 - TOLUENE Painter Over 2.3 ORGANICS #1 DATE: 06-16-92 METHOD: NIOSH 1300 Painter Under < MOL INLET GRID A 1.3 1.4 1.3 ¥ న \$

ORGANICS #1
DATE: 06-16-92
METHOD: NIOSH 1300

GRID CHART 4 - BUTYL ACETATE

TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485

D E INITIALS:BN & LJL Q A INITIALS:LJL

0.3 4 MDL + MDL + MDL	\$ 7°0 8	1.1 12 0.9	3 1.4 24 0.9 28 0.3	15 16 1.1 38 0.3		GRID WOL: 0.0116 mg/SAMPLE EXHAUST DUCT: 0.8
2 0.4 3	7 9.0 9	11 0.5	22 0.8 23	1,8		6 6 8 8 8
1 0.4	5 0.3	9 0.5	21 0.7	13 8.0	17 0.5	PAINT TYPE: LT CREEN PRIMER, GRAY TOP UNITS: mg/M3
Painter Over < MDL Painter Under < MDL	INLET GRID A	**	۶۶ ۲۰۰۰	3A 0.4		PAINT TYPE: LT GREEN

INLET GRID 8 Field Blank < MDL D E INITIALS:BN & LJL Q A INITIALS:LJL 18 \* HOL 28 \* 38 < PDL EXHAUST DUCT: < HOL RECIRC DUCT: < MOL PAINTER MOL: 0.0117 mg/SAMPLE 24 × MDL 76 104 ^ GRID HOL: 0.0117 mg/SAMPLE 12 < MOL 30 \* **30** \* 30 10H > , <del>M</del> √ HDI A MOL ± , 23 < HOL 15 < PDL 19 \* #DL EXHAUST GRID TRAVIS AFB
PAINT BOOTH TESTS
ACUREX PROJECT 8485 OSHA TWA: 435 mg/H3 14 < PDL 18 \* 101 10 \* PDL 22 • MDL PAINT TYPE: LT GREEN PRIMER, GRAY TOP UNITS: Mg/M3 ) MOI > , 10 10 10 TOM > 13 < HDL 21 < MDL 17 < MOL √ MDL **10** OBJECT: AUXILIARY RAMP GRID CHART 5 - ETHYL BENZENE Painter Over < MOL Painter Under < MDL ORGANICS #1 DATE: 06-16-92 METHOD: NIOSH 1300 INLET GRID A \*\* \* MOL ₩ • 70H ¥

TRAVIS AFB
PAINT BOOTH TESTS
ACUREX PROJECT 8485

INLET GRID B Field Blank < MDL D E INITIALS:BN & LJL Q A INITIALS:LJL 38 • PDL 18 • FOL 28 < MOL EXHAUST DUCT: < MDL 0.3 GRID MDL: 0.0368 mg/SAMPLE 24 < PDL 20 < **H**OL 12 < MDL V MOL **JQ!** > 16 19 \* MOL 15 < MOL 11 , #0L TOH > ¥ MOL **EXHAUST GRID** 23 7.0 22 < POL 10 × MOL 18 < MDL PAINT TYPE: LT GREEN PRIMER, GRAY TOP UNITS: MG/MS JOH V · 동 기 4 ~ 0.3 9 \* #DL 13 < POL 17 \* PDL 10H > ^ #0L 21 GRID CHART 6 - XYLENES Painter Over ORGANICS #1 DATE: 06-16-92 METHOD: NIOSH 1300 . . . . . . . . . . . . . Painter Under < MDL INLET GRID A \* . #0L 34 4 **H**DL า**ด**ะ ส`

RECIRC DUCT: < NOL

PAINTER MOL: 0.0368 mg/SAMPLE

OSHA TWA: 435 mg/H3

OBJECT: AUXILIARY RAMP

		1	
F 2	XYLENES (ug)		2
2AGE 1 0F	ETHYL BENZENE (ug)		2
-	BUTYL ACETATE (ug)	nd 19 135 141 151 151 151 151 151 151 151 151 15	7
, GRAY TOPCOAT 30TTOMS	TOLUENE (ug)	nd hd hd hd hd hd hd hd hd hd hd hd hd hd	r 5
LT GREEN PRIMER, GRAY AUXILIARY RAMP BOTTOMS	MIBK (ug)	156 156 166 178 178 178 178 178 178 178 178	7
T GREEN P UXILIARY	MEK (ug)	209 nd 71 nd 71 109 109 109 109 109 109 109 10	)
PAINT: L OBJECT: A	RUN TIME (min)	7.3 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5	)
.S 1485	POST-CAL R (ml/min)	1018 1078 1176 1176 1176 1176 11067 1067 1167 1170 1170	4
TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485	RE-CAL Pml/min) (	1033 1034 1091 1102 1103 1103 1058 1058 1058 1039 1039 1030 1030 1030 1050 1050 1050 1050 1050	4
TRAVIS PAINT B ACUREX	)# dWnd	200 200 200 200 200 200 200 200 200 200	ì
#2 AM 30	ACUREX SAMPLE #	900407&8 900419&20 900419&20 900419&10 900409&10 900499&500 900499&500 900411&2 900411&2 900411&2 900413&4 900413&4 900413&4 900413&4 900413&4 900413&4 900413&4 900413&4 900413&4 900413&8 900413&8 900413&8 900413&8 900413&8 900413&8 900413&8 900413&8 900518&2 900413&8 900413&8 900413&8 900518&2 900413&8 900518&2 900403&4 900521&2 900521&2 900521&2	
ORGANICS #2 06-17-92 AM NIOSH 1300	ACUREX TUBE #	113 46 116 116 117 118 117 117 117 117 118 118 118 118	)
TEST: 0 DATE: 0 METHOD: N	GRID LOC	1 10 22 23 24 14 14 14 15 16 16 16 17 17 18 18 18 18 18 18 18 18 18 18 18 18 18	

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A Sampl XYLENES (mg/M3) & LJL LJL 1.1 1.6 1.0 0.3 < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < ETHYL BENZENE (mg/M3) PAGE 2 OF 2 D E INITIALS: Q A INITIALS: BUTYL ACETATE (mg/M3) TOLUENE (mg/M3) MIBK (mg/M3) MEK (mg/M3) 2 2 2 2 2 9 AVG FLOW (L/MIN) 1.026 1.082 1.082 1.057 1.059 1.059 1.059 1.059 1.054 1.054 1.060 900407&8 900419&20 9005431&2 9005409&10 9005409&10 900411&2 900411&2 900411&2 900411&2 900411&2 900411&2 900511&2 900511&2 900511&2 900511&2 900511&2 900511&2 900511&2 900511&2 900511&2 900511&2 900511&2 900511&2 900518&2 ACUREX SAMPLE # ORGANICS #2 06-17-92 AM NIOSH 1300 ACUREX TUBE # TEST: (DATE: (METHOD: N GRID ط م

INCET GRID B 5.8 2.1 2.4 28 • #DL D E INITIALS:BN & LJL Q A INITIALS:LJL 38 • PDL 8 EXHAUST DUCT: RECIRC DUCT: 20 no sample 8 nosample 24 no sample 4 no sample 5.4 13.3 GRID HDL: 0.0115 mg/SAMPLE PAINTER MOL: 0.0115 mg/SAMPLE 42 \$ 3 no sample 23 no sample 57.9 4.6 11.3 6.7 **EXHAUST GRID** 4 \$ Ξ TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485 18 no sample OBJECT: AUXILIARY RAMP BOTTOMS OSHA TWA:590 mg/M3 5.9 6.0 5.0 1.3 4.6 3.3 PAINT TYPE: LT GREEN PRIMER, GRAY TOP UNITS: mg/M3 10 22 14 9 3.6 3.3 1.3 3.3 1. JOH V 17 2 2 INLET GRID A Painter Under 0.2 Painter Over 11.5 TEST: ORGANICS #2 DATE: 06-17-92 AM METHOD: NIOSH 1300 GRID CHART 1 - MEK 2A < MOL 1.2 5.3 ž <

INLET GRID B 6.4 5.6 2.2 28 • #DL 호 · D E INITIALS:BN & LJL Q A INITIALS:LJL 9 EXHAUST DUCT: RECIRC DUCT: 20 no sample 8 no sample 24 no sample 4 no sample GRID MOL: 0.0095 mg/SAMPLE PAINTER NDL: 0.0095 mg/SAMPLE 5.4 4.1 9 12 23 no sample 3 no sample 7.4 5,3 7.7 4.0 EXHAUST GRID 4 5 Ξ PAINT BOOTH TESTS ACUREX PROJECT 8485 18 no sample OBJECT: AUXILIARY RAMP BOTTOMS OSHA TWA:205 mg/M3 5.9 10.3 11.5 3.5 5.4 1.7 PAINT TYPE: LT GREEN PRIMER, GRAY TOP UNITS: mg/M3 7 25 0 4.7 2.8 5.8 3.6 1.6 **→ HDL** 1 2 Ñ Painter Over 6.9 INLET GRID A Painter Under < MDL TEST: ORGANICS #2 DATE: 06-17-92 AM METHOD: NIOSM 1300 GRID CHART 2 - MIBK 1.6 1.7 ฮ ส` Š ≨

INLET GRID B -: 3.1 1.6 D E INITIALS:BN & LJL Q A INITIALS:LJL 38 \* **10**1 Sa NOL E EXHAUST DUCT: RECIRC DUCT: 8 no sample ou semble 20 nosemple 24 no sample 2.2 2.8 GRID MDL: 0.0114 mg/SAMPLE PAINTER MOL: 0.0114 mg/SAMPLE 12 4 3 no sample 23 no semple 2.0 2.8 4.8 2.1 **EXHAUST GRID** 4 Ξ 15 TRAVIS AFB
PAINT BOOTH TESTS
ACUREX PROJECT 8485 18 no sample OBJECT: AUXILIARY RAMP BOTTOMS OSHA TWA:375 mg/H3 3.0 5.6 6.3 0. 1.7 1.2 PAINT TYPE: LT GREEN PRIMER, GRAY TOP UNITS: mg/H3 9 22 14 1.0 1.9 1.8 3.2 2.5 **A FOL** 13 17 21 GRID CHART 3 - TOLUENE INLET GRID A \*\*\*\*\*\* . . . . . . . . . . . . . . . Painter Over 3.8 Painter Under < MOL TEST: ORGANICS #2 DATE: 06-17-92 AM METHOD: NIOSH 1300 1.0 0.9 78 \* HDE 34 ۲

INLET GRID B 6.0 0.5 7.0 38 D E INITIALS:BN & LJL Q A INITIALS:LJL 28 \* HDL = EXHAUST DUCT: RECIRC DUCT: 24 no semple 20 nosample 8 no sample 4 nosample 0.7 1.0 GRID MOL: 0.0116 mg/SAMPLE PAINTER MOL: 0.0116 mg/SAMPLE 42 \$ 3 no sample 23 no sample 1.6 9.0 1.0 1.6 **EXHAUST GRID** 4 \$ = TRAVIS AFB
PAINT BOOTH TESTS
ACUREX PROJECT 8485 18 nosample OBJECT: AUXILIARY RAMP BOTTOMS OSHA TWA:710 mg/H3 0.5 0. 2.1 0.3 SH/Bm 7.0 9 22 # PAINT TYPE: LT GREEN PRIMER, GRAY TOP UNITS: 9.0 0.5 1.0 8.0 0.3 A MOL 4 2 7 GRID CHART 4 - BUTYL ACETATE TEST: ORGANICS #2 DATE: 06-17-92 AM METHOD: NIOSH 1300 Painter Under < MOL INLET GRID A Painter Over 1.1 0.3 0.3 704 × × ā \$

INLET GRID B D E INITIALS:BN & LJL Q A INITIALS:LJL 28 • HDL 24 × 10 × . . 10 . 10 . 10 EXHAUST DUCT: < MOL RECIRC DUCT: < MOL 24 no sample 20 no sample 4 no sample 8 no sample 12 • HDL 16 • HDL GRID MOL: 0.0117 mg/SAMPLE PAINTER MOL: 0.0117 mg/SAMPLE 3 no sample 23 no sample 19 • **F**OL V MOI JOH Y JOH > **EXHAUST GRID** 15 TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485 18 no sample OBJECT: AUXILIARY RAMP BOTTOMS OSHA TWA:435 mg/H3 22 < MDL 10 < MDL PAINT TYPE: LT GREEN PRIMER, GRAY TOP UNITS: mg/M3 JOH V JOH V 9 21 < MDL 13 < PDL 17 < HDL \$ **₹** ¥ MDL < MOL GRID CHART 5 - ETHYL BENZENE Painter Over Painter Under < MDL TEST: ORGANICS #2 DATE: 06-17-92 AM METHOD: NIOSH 1300 INLET GRID A 2A < MDL 14 4 MDL .¥ . #DL

TEST: ORGANICS #2 DATE: 06-17-92 AM METHOD: NIOSH 1300

GRID CHART 6 - XYLENES

TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485

D E INITIALS:BN & LJL Q A INITIALS:LJL

	INLET GRID	18 × MDL	28 NDL	38 *		LE EXHAUST DUCT: < MOL
4,	8 no sample	12 < HDL	24 no semple	16	20 no sample	GRID MOL: 0.0368 mg/SAMPLE
3 nosample	7 < HOL	11 < MOL	23 no sample	15 < MOL	19 < PDL	GRID MOL: 0.0
2 < MOL	10H >	10 < MOL	22 < MOL	14 < MOL < MOL	18 no sample	11S: mg/H3
1 < MDL	5 * <b>3</b> 0L	9 * #0F	21 < MDL	13 A PDL	17 < 401.	
Painter Over < MOL Painter Under < MOL	INLET GRID A	۲.	2A MDL	Ş ≸		PAINT TYPE: LT GREEN PRIMER, GRAY TOP UNITS:

TEST: OPATE: OPATE: N	ORGANICS #3 06-17-92 PM NIOSH 1300	#3 00	TRAVIS AFB PAINT BOOTI ACUREX PRO	TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485	STS 8485	PAINT: OBJECT:	LT GREEN PRIMER METAL & WOOD BOX	PRIMER 1000 BOX			PAGE 1 OF	2
GRID LOC	ACUREX TUBE #	ACUREX SAMPLE # F	# JWN #	PRE-CAL PUMP #(m]/min)	POST-CAL (ml/min)	RUN TIME (min)	MEK (ug)	MIBK (ug)	TOLUENE (ug)	BULYL ACETATE (ug)	BENZENE (ug)	XYLENES (ug)
P over 18	132 132 132 132 100 100 100 100 100 100 100 100 100 10	900813&4 900825&6 900827&8 900839&50 900839&40 900839&40 900831&2 900851&2 900853&4 900853&4 900853&4 900853&4 900853&4 900853&6 900853&6 900853&6 900853&6 900853&6 900853&6 900853&6 900853&6 900853&6 900853&6 900853&6 900853&6 900853&6 900853&6 900853&6 900853&6 900853&6 900853&6 900853&6 900858 900858 900858 900858 9008058 9008058 9008058 9008058 9008058 9008058 9008058 9008058 9008058 9008058 9008058 9008058 9008058 9008058 9008058	255 264 275 276 276 277 277 278 278 278 278 278 278 278 278	1068 1169 11163 11163 11034 1034 1036 1036 1047 1057 1057 1057 1057 1057 1057 1057 105	1046 1175 1175 1175 1175 1175 1177 1177 117	00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	412 nd 14 14 65 470 601 601 601 601 601 601 601 60	339 nd nd nd nd 196 314 467 1113 805 nd 270 1385 834 659 609 1094 71 81 nd 484 477 nd 484 477 nd 236 nd 236 nd 236 nd 236 nd 236 nd 247 nd 236 nd 247 nd 247 nd 256 nd 267 1094 10	nd nd nd 17 nd 18 18 118 118 119 119 119 119 119 119 1	191 191 191 191 191 191 191 191	999999999999999999999999999999999999999	
ADDITIONAL 10 22 RECIRC	ORGAN] 91 146 98	ORGANIC SPECIES 91 900829830 146 90083182 98 90027283	10 17 39	1094 1096 1067	1072 1125 997	50 49 46	2-METHOXY ETHYL ETHER 51 62 nd	ETHYL ACETATE nd nd nd 706				

TEST: ORGANICS #3 DATE: 06-17-92 PM METHOD: NIOSH 1300

BN & LJL LJL PAGE 2 OF 2 D E INITIALS: Q A INITIALS:

XYLENES (mg/M3)	eno sample eno sample	
ETHYL BENZENE (mg/M3)	Sample Sa	
BUTYL ACETATE (mg/M3)	eno sampleno eno sampleno eno sampleno eno sampleno 6.55 6.55 6.56 6.96 4.1 4.1 6.9 6.9 6.9 6.9 6.9 6.9 6.9 6.9 6.9 6.9	
TOLUENE (mg/M3)	Sample Mol. 19 Co. 19 C	
MIBK (mg/M3)	no sampleno « MDL « MDL « MDL « MDL « MDL » «	ETHYL ACETATE A MDL MDL 14.9
MEK (mg/M3)	no sampleno (MOL ) (MOL	2-METHOXY ETHYL ETHER 0.9 1.1
AVG FLOW (L/MIN)	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	
ACUREX SAMPLE #	90081384 90081384 90081384 90081384 90081386 900813884 90081382 90081382 90081382 90081384	
ACUREX TUBE #	1040 1040 1040 1040 1040 1040 1040 1040	
A GRID LOC T	EXH EXH EXH EXH EXH EXH EXH EXH	ADDITIONAL 10 22 RECIRC

INLET GRID B 28 no sample 5.7 4.9 23.7 D E INITIALS:BN & LJL Q A INITIALS:LJL RECIRC DUCT: < MOL 38 9 EXHAUST DUCT: 20 20 4 nosemple 12 no semple 11.0 23.9 28.7 GRID MOL: 0.0115 mg/SAMPLE PAINTER MOL: 0.0115 mg/SAMPLE 2 **5**7 80 12.6 23.6 23.2 46.2 108.3 **→ EXHAUST GRID** = 15 2 23 PAINT BOOTH TESTS ACUREX PROJECT 8485 2 nosample OSHA TWA:590 mg/H3 15.6 16.2 13.3 2.1 18.1 UNITS: mg/H3 18 22 14 10 9 5 no sample 8.0 16.3 9.9 13.4 17 < MOL 13 7 0 OBJECT: METAL & WOOD BOX PAINT TYPE: LT GREEN PRIMER Painter Over 2.7 INLET GRID A Painter Under no sample TEST: ORGANICS #3
DATE: 06-17-92 PM
METHOD: NIOSH 1300 GRID CHART 1 - MEK 2.6 7.2 7.6 ¥ న **¥** 

INLET GRID B 28 no semple 5.5 14.1 12.8 9.4 D E INITIALS:BN & LJL Q A INITIALS:LJL 38 # **EXHAUST DUCT:** RECIRC DUCT: 4 no sample 20 no sample 12 no sample 13.1 1.5 GRID MDL: 0.0095 Mg/SAMPLE PAINTER MOL: 0.0095 mg/SAMPLE 8.5 16 54 1.2 8.3 16.1 18.7 8.4 OH V EXHAUST GRID N 4 Ξ \$ TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485 2 nosample OSHA TWA: 205 mg/M3 20.02 8.9 20.6 25.5 7.9 UNITS: Mg/H3 13 9 22 7 5 no sample 22.6 8.9 18.1 6.5 17 < MOL 13 21 0 OBJECT: METAL & WOOD BOX PAINT TYPE: LT GREEN PRIMER Painter Under no sample \*\*\*\*\*\*\*\*\*\*\* INLET GRID A TEST: ORGANICS #3 DATE: 06-17-92 PM METHOD: NIOSH 1300 GRID CHART 2 - MIBK Painter Over 4.7 9.9 2.6 6.4 ĸ న ₹

INLET GRID B 28 no sample 0.3 D E INITIALS:BN & LJL Q A INITIALS:LJL 0.3 18 • FDL 38 < 10L EXHAUST DUCT: RECIRC DUCT: 20 no sample 4 no sample 12 no semple 0.3 0.3 GRID MDL: 0.0114 mg/SAMPLE PAINTER MOL: 0.0114 mg/SAMPLE YOK > 16 24 80 0.5 0.4 0.5 3.4 19 \* FOL 10H > EXHAUST GRID Ξ 5 ĸ TRAVIS AFB
PAINT BOOTH TESTS
ACUREX PROJECT 8485 2 no sample OSHA TUA:375 mg/H3 9.0 9.0 0.2 0.7 104 > UNITS: Mg/M3 9 18 22 7 5 nosample 9.0 0.5 21 < MDL 17 < MDL JOH > **£** OBJECT: METAL & WOOD BOX PAINT TYPE: LT GREEN PRIMER GRID CHART 3 - TOLUENE Painter Over < MDL INLET GRID A Painter Under no sample TEST: ORGANICS #3 DATE: 06-17-92 PM METHOD: NIOSH 1300 3A NOL אַ אַ אַ 14 < 10L

D E INITIALS:BN & LJL Q A INITIALS:LJL TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485 TEST: ORGANICS #3 DATE: 06-17-92 PM METHOD: NIOSH 1300

ဆ ခ်္ဂ လုံ ဆုံ O  ၂	EXHAUST GRID	3 4 4 ple no sample	1.8 7 2.2 8 1.3	5.5 11 12 5.5 4.1 no sample	6.9 23 4.7 24 3.0	5.4 15 4.7 16 3.2	19 20 2.4 . 2.3 no sample
- 5 5 5		0 6 0 0 0 0 0 0	·	10	22	71	85

INLET GRID B 28 no sample D E INITIALS:BN & LJL Q A INITIALS:LJL 18 A 1901 왕 **(원** EXHAUST DUCT: < HOL RECIRC DUCT: < MOL 4 nosample 12 no sample 20 no sample PAINTER MDL: 0.0117 mg/SAMPLE GRID MOL: 0.0117 mg/SAMPLE 56 . . ₹Ð! ₩ \* 년 \* 5% 80 # × 101 × YOH > < MOL 15 < HDL < HOL 19 < MOL 23 **EXHAUST GRID** TRAVIS AFB
PAINT BOOTH TESTS
ACUREX PROJECT 8485 2 no sample OSHA TWA: 435 mg/H3 10 × MOL 14 ^ 130L Y MOL < MOL 13 \* FDL UNITS: Mg/HG 22 5 no sample 21 < 101 13 < FOL < HDL <u>5</u> 17 < HDL OBJECT: METAL & MOOD BOX PAINT TYPE: LT GREEN PRIMER GRID CHART 5 - ETHYL BENZENE Painter Over < MOL Painter Under no sample TEST: ORGANICS #3 DATE: 06-17-92 PM METHOD: NIOSH 1300 INLET GRID A 2A MOL 34 YOF . . . ₹

INLET GRID B 28 nosample 38 4 MDL D E INITIALS:BN & LJL Q A INITIALS:LJL A HOL EXKAUST DUCT: < MOL RECIRC DUCT: < MOL 8 20 no sample 12 no sample 4 nosample GRID MDL: 0.0368 mg/SAMPLE PAINTER MOL: 0.0368 mg/SAMPLE 24 < MDL 16 < MOL ₩ • 00 0.3 23 \* #DL 19 \* MOL 10H > 15 < MDL JOH Y **EXHAUST GRID** = TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485 2 no sample OSHA TWA: 435 mg/H3 1.0 7.0 6 × MOL 14 < PDL 18 < MDL UNITS: mg/M3 0 22 5 no sample 21 < HOL 17 < HDL 13 < PDL **M** • **M** • A MOL OBJECT: METAL & WOOD BOX PAINT TYPE: LT GREEN PRIMER GRID CHART 6 - XYLENES Painter Over TEST: ORGANICS #3
DATE: 06-17-92 PM
METHOD: NIOSH 1300 Painter Under no sample INLET GRID A 2A MOL ¥ , <del>10</del>1 ₹

- 5	XYLENES (ug)	pu	מס	p	pu	pu	pu	nd.	nd.	ב	0	ב ב	יים פיים	ָב ב	בי דב בי	2 2		10	pu	pu	pu	nd	nd	ou.	nd	nd	nd	pu	nd	nd	pu	pu.	nd n	ב ב	2 2
PAGE 1 OF	ETHYL BENZENE : (ug)	pu	2	pu	nd	pu	pu	ng.	nd -	ב ב	5 7	27	י מ	7 5	2 2	2 2		200	pu	ng.	pu	pu	nd	nd	nd	nd	nd	nd	nd	ng	nd .	nd	ם ו	2 2	n d
	BUTYL ACETATE (ug)	pu	nd	밀	pu	13	pu	nd	nd	77	27	na 20	200		2 2	2 72		32	pu	pu	pu	nd	pu	16	nd	nd D	nd	nd	nd	nd	pq.	nd	ם ב	1	nd h
	TOLUENE (ug)	pu	nd	pu	nd	pu	nd D	pu.	ם ב	יד ם מ	2 T	ם פ	ב ב ב	2 2	2 2	2	Pu	nd	pu	pu	nd	nd	nd n	nd	D.	ը.	nd	nd	pu.	nd	nd	nd	ם קם	2 2	2 2
PRIMER	MIBK (ug)	pu	pu	nd	nd	nd	pu	0	27	2 2	10	07 Pu		13	24	nd Pu	pu	pu	25	56	20	pu	111.	nd	132	nd	pu.	nd	<u>.</u>	nd	ם כ	ם יים	מש	20	nd 55
LT GREEN P LADDERS	MEK (ug)	pu	nd	pu		31		וים		200	201	101	40	7.1	117	75	56	20	128	200	106	94	420	455	421	nd	nd T	pu	4 . X	45		nd 43	47 25	199	76
PAINT: 1 08JECT:	RUN TIME (min)	0	1		0	30	5 <u>3</u>	-	200	280	200	60	30	200	29	29	22	59	59	30	30	29	52	30	67	0.0	28	0 0	53	67	62	200	200	312	30
TS 8485	POST-CAL (ml/min)	1080	1128	1082	1060	878	1043	1002	1000	705	1016	1029	1077	1046	1029	1046	1082	1043	1037	1078	1014	530	1053	1046	400	1071	1040	2001	1026	1040	1019	010	1033	1049	1028
TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485	PRE-CAL   PUMP #(m]/min)	1055	1071	1089	1060	890	1001	1001	1000	1060	1023	1041	1089	1053	1036	1042	1060	1050	1077	1089	1066	800	1022	1033	0 0 0	1020	1044	1004	105/	1001	7001	020	1025	1009	1030
TRAVIS PAINT E ACUREX		1	24	50	Σ, .	ດເ	35	, c	3 4	<u></u>	0	32.0	15	17	31	37	2	12	10	ത	`:	410	3.5	11	000	3 5	77	ر د د	2 0	0 0	17	0 0	28	36	39
#4 0	ACUREX SAMPLE #	900867888	900869870	90087384	9008/286	9008//88	9008/8880	90000182	90088586	90088788	900889890	900891&2	900907&8	900909810	90091182	900913&4	900893&81	90092182	900894872	900895&6	90089788		30030182	00000004	00000000	0002000	90027000	000000	30000182	90000004	000000000	90031280	900919820	90027488	900279880
ORGANICS #4 06/18/92 NIOSH 1300	ACUREX TUBE #	174														151	167	127	1/0			,, ,						177	161						
TEST: C DATE: C METHOD: N	GRID LOC	₩.	~ (	א ני	<del>1</del> u	ი u	0 1	. α	) on	10	11	12	21	22	23	24	13	13 DUP	վ . գի լ	15	17	α.	18 210		200	2000		200	77	7 6	, <del>.</del>	3 6	38	EXHAUST	RECIRC

| March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | March | Marc XYLENES (ug/M3) & LJL LJL BN BN ETHYL BENZENE (ug/M3) PAGE 2 OF 2 D E INITIALS: Q A INITIALS: BUTYL ACETATE (ug/M3) TOLUENE (ug/M3) MEK (Mg/M3) AVG FLOW (L/MIN) 1.068 1.100 1.100 1.006 1.008 1.008 1.008 1.008 1.008 1.008 1.008 1.008 1.008 1.008 1.008 1.008 1.008 1.008 1.009 900867&88 900869&70 900873&4 900877&86 900877&86 900887&8 900881&2 900881&2 900881&2 900881&2 900881&2 900881&2 900881&2 900881&2 900891&2 900891&2 900891&2 900891&2 900891&2 900891&2 900897&8 ACUREX SAMPLE # ORGANICS #4 06/18/92 NIOSH 1300 ACUREX TUBE # TEST: (DATE: (METHOD: N P over P under 1A 3A 3A 3B EXHAUST RECIRC 18 ۵.

INLET GRID B 1.5 1.2 6.2 2.5 D E INITIALS:BN & LJL Q A INITIALS:LJL 18 101 8 쁡 EXHAUST DUCT: RECIRC DUCT: 4 no sample 8 no sample 20 no sample 2.3 2.5 3.4 GRID MOL: 0.0115 mg/SAMPLE PAINTER MOL: 0.0115 Mg/SAMPLE 12 54 18 7 no sample 16.6 3.6 3.9 6.2 JOH > EXHAUST GRID 4 Ξ 23 5 TRAVIS AFB
PAINT BOOTH TESTS
ACUREX PROJECT 8485 OSHA TUA:590 mg/N3 14.0 14.6 1.3 2.1 2.3 4.2 UNITS: mg/H3 JŒ > 0 13 22 14 1 no sample 1.2 2.4 6.4 7 1.2 5 14 21 0 PAINT TYPE: LT GREEN PRIMER OBJECT: LADDERS Painter Over < MDL Painter Under no sample TEST: ORGANICS #4 DATE: 06/18/92 METHOD: NIOSH 1300 INLET GRID A GRID CHART 1 - MEK 1.7 9. 1.5 **¥** S z

D E INITIALS:BN & LJL. Q A INITIALS:LJL			INLET GRID	1 <b>9</b>	28 < HOL	38 < MOL		EXHAUST DU RECIRC DU
		o sample	8 nosemple	12 < MDL	24 × MOL	16 0.6	20 no sample	395 mg/SAMPLE 395 mg/SAMPLE
STS F 8485	EXHAUST GRID	3 < HOL	7 no semple	11 0.6	23 0.8	1.7	19 5.2	GRID MDL: 0.0095 mg/SAMPLE PAINTER MDL: 0.0095 mg/SAMPLE
TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485		2 MDL 3	70H >	10 < FDL	22 0.4	14 0.8	18 3.7 < HOL	UNITS: mg/H3 OSHA TWA:205 mg/H3
		1 no sample	5 × PDL	104 > 6	74 × 190	13	104 >	
TEST: ORGANICS #4 DATE: 06/18/92 METHOD: NIOSH 1300	GRID CHART 2 - MIBK	Painter Over  < MDL  Painter Under no sample	INLET GRID A	ਹੁੰ ≚ `	2A < #DL	AV Av		PAINT TYPE: LT GREEN PRIMER OBJECT: LADDERS

INLET GRID B D E INITIALS:BN & LJL Q A INITIALS:LJL 18 ^ #DL 28 \* MDL 38 • PDL EXHAUST DUCT: < MDL RECIRC DUCT: < NOL 4 no sample 20 no sample 8 nosample 24 < MDL GRID MDL: 0.0114 mg/SAMPLE PAINTER MDL: 0.0114 mg/SAMPLE 12 < MDL 16 A MOL 7 no sample A FOL 11 < MOL JOH V 15 < 1901. < HOL 4 EXHAUST GRID 23 TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485 OSHA TWA:375 mg/H3 22 < MOL 10 A MOL 14 < MDL 18 \* #0! #0! 10H > UNITS: mg/H3 **10** 1 no sample 21 < MOL 5, 15, 15, 15, 9 \* 10 10 A MOL 17 < MOL PAINT TYPE: LT GREEN PRIMER OBJECT: LADDERS GRID CHART 3 - TOLUENE Painter Over TEST: ORGANICS #4 DATE: 06/18/92 METHOD: NIOSH 1300 . . . . . . . . . . . . . . . . . . Painter Under no sample INLET GRID A 1A ^ MOL ₹ \* 34 4 HDL

D E INITIALS:BN & LJL Q A INITIALS:LJL 4 no sample JOH > EXHAUST GRID TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485 Y MOL t no sample GRID CHART 4 - BUTYL ACETATE Painter Over Painter Under no sample TEST: ORGANICS #4 DATE: 06/18/92 METHOD: NIOSH 1300

INLET GRID B	18	28 < MDL	38 < PDL		EXHAUST DUCT: 0.4 RECIRC DUCT: < MOL
8 nosample	12 1.0	24 MDL	36 • • • • • • • • • • • • • • • • • • •	20 nosample	
7 nosample	11 < MOL	104 ×	15	19 < MOL	GRID MOL: 0.0116 Mg/SAMPLE PAINTER MOL: 0.0116 Mg/SAMPLE
10H > 9	10 • A	22 < HOL	14 < MOL	18 < MDL 0.5	UNITS: mg/H3 OSHA TUA:710 mg/H3
5 0.5	6	21 1.0	13.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4.4	17 < FOL	PRIMER UN
INLET GRID A	44 40L	A HOL	JOH Y		PAINT TYPE: LT GREEN P OBJECT: LADDERS

D E INITIALS:BN & LJL Q A INITIALS:LJL			INLET GRID	<b>호</b> *	28 < MDL	38 >		EXHAUST DUCT: < NOL RECIRC DUCT: < NOL
<b>6</b>	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	4 no sample	8 no sample	12 < MDL	24 < MDL	16	20 no semple	
ESTS T 8485	EXHAUST GRID	10 <b>£</b> > .	7 no sample	11 < MOL	23 ************************************		19 < MDL	GRID MOL: 0.0117 mg/SAMPLE PAINTER MOL: 0.0117 mg/SAMPLE
TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485	ЕХНА	2 < 10L	10t > 9	10 • FDL	22 < PDL	75 JG	18 < FDL < FDL	UNITS: Mg/N3
	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 no sample	5 × PDL	7 <b>H</b> OF <b>&gt;</b>	21 < PDL	13 < 70 * 70 * 70	17 < MDL	4 8 8 8 8 6 6 6 6
TEST: ORGANICS #4 DATE: 06/18/92 METHOD: NIOSH 1300 GRID CHART 5 - ETHYL BENZENE		Painter Over < MDL Painter Under no sample	INLET GRID A	<b>1</b>	24 BDL			PAINT TYPE: LT GREEN PRIMER OBJECT: LADDERS

INCET GRID B ₽ \* 85 A 105 D E INITIALS:BN & LJL Q A INITIALS:LJL 왕 ^ 101 4 no sample 20 no sample 8 no sample 12 • HOL 16 × MOL 년 오 오 7 no sample 19 < MOL 10E . **. . . .** JOH Y JOH V **EXHAUST GRID** 15 = 23 TRAVIS AFB
PAINT BOOTH TESTS
ACUREX PROJECT 8485 22 < HOL 18 , , 10E , 14 A 101 JOH > ) 19 19 1 no sample 21 < 90L 고 주 전 전 전 전 전 전 기 기 17 < 150L **101** × **10H** × GRID CHART 6 - XYLENES Painter Over < MDL Painter Under no sample INLET GRID A TEST: ORGANICS #4 DATE: 06/18/92 METHOD: NIOSH 1300 2A • MDL ¥ , ₩ 14 \* #0!

EXHAUST DUCT: < MDL RECIRC DUCT: < MDL

PAINTER MOL: 0.0368 mg/SAMPLE

OSHA TWA: 435- mg/N3

UNITS: mg/M3

PAINT TYPE: LT GREEN PRIMER OBJECT: LADDERS

GRID MDL: 0.0368 mg/SAMPLE

2	(ng)	ND ND ND ND ND ND ND ND ND ND ND ND ND N
PAGE 1 OF	ETHYL BENZENE X (ug)	NN NN NN NN NN NN NN NN NN NN NN NN NN
	BUTYL ACETATE (ug)	ND ND ND ND ND ND ND ND ND ND ND ND ND N
	TOLUENE (ug)	ND ND 1113 ND 152 ND 165 ND 16
OAT ILLET	MIBK (ug)	ND 415 ND 415 ND 415 ND 554 1073
WHITE TOPCOAT COMFORT PALLET	MEK (ug)	ND ND 76 ND 79 ND
PAINT: NOBJECT: C	RUN TIME (min)	
.TS 8485	POST-CAL (ml/min)	1045 1029 1044 1009 1009 1004 1043 1055 1055 1055 1065 1067 1073 1073 1073 1073 1073 1073 1073 107
TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485	PRE-CAL (ml/min)	1063 1077 1077 1077 1077 1077 1078 1078 1078
TRAVIS PAINT ACUREX	PUMP #(	33 222 23 23 24 24 25 25 25 25 25 25 25 25 25 25 25 25 25
ORGANICS #5 06-23-92 PM NIOSH 1300	ACUREX ACUREX TUBE # SAMPLE #	211 900943&4 198 900945&6 198 900945&8 238 900945&8 238 900953&4 183 900953&4 215 900957&8 216 900953&7 217 900965&6 227 900963&4 227 900965&8 228 900978&8 228 900978&8 229 900978&8 220 900978&8 221 900978&8 222 900978&8 223 900983&4 224 900983&8 225 9009988&8 227 900938&8 228 900983&8
TEST: OR DATE: O6 METHOD: NI	GRID LOC	1 2 3 4 4 5 6 6 6 7 7 8 8 9 9 10 11 11 12 13 14 13 14 15 16 17 18 19 10 10 11 11 11 11 12 13 13 14 15 16 17 18 18 19 10 10 10 10 10 10 10 10 10 10

no sampleno XYLENES (mg/M3) & LJL LJL ETHYL BENZENE (mg/M3) PAGE 2 OF 2 D E INITIALS: Q A INITIALS: BUTYL ACETATE (mg/M3) TOLUENE (mg/M3) sampleno sam MIBK (mg/M3) MEK (mg/M3) 2 2 2 2 2 2 2 AVG FLOW (L/MIN) 900392 90093182 90093387 90093586 90093586 90093840 900925 900925 900925 900925 900943&4 900945&6 900945&8 900945&8 900953&4 900955&6 900955&8 900955&8 90095&8 900963&4 900963&4 900963&4 900963&4 900963&4 900963&8 900963&8 900975&8 900975&8 900975&8 900975&8 900975&8 900975&8 900975&8 900975&8 900991 900987&8 900989&90 900390&1 ACUREX SAMPLE ORGANICS #5 06-23-92 PM NIOSH 1300 ACUREX TUBE # 11998 11998 11988 GRID LOC ۵,

INLET GRID B . . . . . . . . . . . . . . . Field Blank < MOL 2.6 1.0 3.3 6.2 D E INITIALS:BN & LJL Q A INITIALS:LJL 1.2 38 28 Ē EXKAUST DUCT: RECIRC DUCT: 20 no sample 24 no sample no semple 1.3 2.2 4.7 GRID MOL: 0.0115 mg/SAMPLE PAINTER MOL: 0.0115 mg/SAMPLE 2 8 1.3 3.8 7.0 9.1 15.6 1.7 **EXHAUST GRID** 19 = N ŧ TRAVIS AFB
PAINT BOOTH TESTS
ACUREX PROJECT 8485 2 no sample OSHA TWA:590 mg/N3 3.3 3.5 6.3 2.3 mg/H3 22 2 9 7 UNITS: 1 no sample 5 no sample 17 no sample 1.2 1.4 1.3 2 2 **OBJECT: CONFORT PALLET** PAINT TYPE: WHITE TOPCOAT Painter Over no sample Painter Under 8.6 TEST: ORGANICS #5 DATE: 06-23-92 PM METHOD: NIOSH 1300 INLET GRID A GRID CHART 1 - MEK 1.1 1.3 1.0 ž র ≤

D E INITIALS:BN & LJL Q a initials:LJL		Field Blank < MDL	INLET GRID B	5.3	28 6.8	38 W.7		EXHAUST DUCT: 6.4
<b>Q 0</b>	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8.2	8 9.6	12 12.9 no semple	24 no sample	13.0	20 no sample	
STS 8485	EXHAUST GRID	۲۶ و.ه	7 9.5	. 11 12.8	23 19.2	15 20.2 22.8	19 15.2	GRID MOL: 0.0095 mg/SAMPLE
TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485	ЕХНАС	2 no sample	6 9.3	10 16.9	22 20.7	14, 17.2	18 9.9 9.1	UNITS: mg/M3
	5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 no semple	5 no semple	2. 52. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	5.9	13 7.2	17 no sample	
TEST: ORGANICS #5 DATE: 06-23-92 PM METHOD: NIOSH 1300 GRID CHART 2 - MIBK		sample ter U	INLET GRID A	1A 4.2	2 <b>%</b> 5.6	£.3 ¥1		

6.6

RECIRC DUCT:

PAINTER MOL: 0.0095 mg/SAMPLE

OSHA TWA: 205 mg/H3

OBJECT: COMFORT PALLET

D A INITIALS: LJL	1 14	INLET GRID B	1.0	28 1.2	38 0.0		DUCT: 1.2
							EXHAUST DUCT:
	1.1	1.7	12 2.3 no semple	24 no sample	16 2.3	20 nosample	GRID MDL: 0.0114 mg/SAMPLE
	1.2	1.6	2.2	3.3	4.0	a Z.Z	MOL: 0
TH TESTS OJECT 8485 EXHAUST GRID	m	~	=	Σ.	<b>5</b>	19	GRID
ACUREX PROJECT 8485 ACUREX PROJECT 8485 EXHAUST GR	2 nosample	1.7	3.0	3.7	3.2	10 h	J/H3
ACUR	2 00	•	10	23	7	81	UNITS: mg/H3
	1 nosemple	5 no semple	6 0.1 0.8	1.2	13 1.3	17 no sample	5
	•						TE TOPCOAT
DATE: 06-23-92 PH METHOD: NIOSH 1300 GRID CHART 3 - TOLUENE	Painter Over no sample Painter Under 18.3	INLET GRID A	8.0	1.2	0.1		PAINT TYPE: WHITE TOPCOAT
06-23 N10SH RT 3	Painter Over no sample Painter Unde	INLET GRID A	<u>≤</u>	ا	ă		PAINT TY

INLET GRID B Field Blank < MDL 1.1 2.5 9. 1.7 1.3 D E INITIALS:BN & LJL Q A INITIALS:LJL 8 8 EXHAUST DUCT: RECIRC DUCT: 24 no sample 20 no sample no sample 2.4 3.4 GRID MDL: 0.0116 mg/SAMPLE PAINTER MOL: 0.0116 mg/SAMPLE 1.5 4 9 œ 5.5 5.7 4.1 2.5 3.3 1.8 EXHAUST GRID 2 4 n Ξ TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485 2 no sample OSHA TWA:710 mg/H3 4.8 2.3 5.6 2.5 4.7 UNITS: mg/H3 18 14 9 22 17 no sample 1 nosample 5 no sample 1.9 1.6 2 5 OBJECT: COMFORT PALLET PAINT TYPE: WHITE TOPCOAT GRID CHART 4 - BUTYL ACETATE Painter Over no sample TEST: ORGANICS #5 DATE: 06-23-92 PM METHOD: NIOSH 1300 Painter Under 17.3 INLET GRID A 5: 1.4 7¥ ^ #0L S న

INLET GRID B Field Blank < MDL D E INITIALS:BN & LJL Q A INITIALS:LJL 38 4 MOL 4 MOL . . HDL 28 • PDL EXHAUST DUCT: < MDL RECIRC DUCT: < MDL. 24 no sample 12 < MDL no sample 20 no semple GRID MOL: 0.0117 mg/SAMPLE PAINTER MOL: 0.0117 mg/SAMPLE 16 < PDL A MOL JOH > 8 0.3 11 4 HDL · HDL JOH > 10H > **1** EXHAUST GRID 4 23 5 TRAVIS AFB
PAINT BOOTH TESTS
ACUREX PROJECT 8485 2 no sample OSHA TUA:435 mg/M3 **M** × 22 < FDL \$7 , , € € UNITS: Mg/HG V MOL 14 < POL 9 9 S no sample 17 no sample j no sample 0.2 \* PDL 101 v 13 4 HDL 5 OBJECT: COMFORT PALLET PAINT TYPE: WHITE TOPCOAT GRID CHART 5 - ETHYL BENZENE Painter Over no sample INLET GRID A 1 4 8 8 8 8 8 8 8 8 8 8 8 8 8 8 Painter Under 1.1 TEST: ORGANICS #5 DATE: 06-23-92 PM METHOD: NIOSH 1300 ¥ ¥9 SY A MOL 24 \* MOL

1   1   2   3   MOL   4   MOL   1   1   MOL   1   MOL   1   MOL   1   MOL	DATE: 06-23-92 PM METHOD: NIOSH 1300		PAINT BOOTH TESTS ACUREX PROJECT 8485	ESTS :T 8485		Q A INITIALS:LJL
1	GRID CHART 6 - XYLENES			UST GRID		
5 sample 6 HOL 7 HOL 8 HOL  13 HOL 0.3 11 0.2 12 0.2  4 HOL 22 0.4 23 24 24  13 HOL 20.3 16 0.2  14 HOL 19 0.3 16 0.2  17 mo sample 4 HOL 0.3 10 0.3 10 0.2  18 HOL 19 0.3 10 0.3 10 0.2	Painter Over no sample Painter Under	1 nosample	sampl	3 < MDL	10H > 7	Field Blank
5 no sample 6 < MOL 7 < MOL 8 + MOL 9   21	1 6 9 1 0 1 0 1 1 1					
21	INLET GRID A	5 no sample				INLET GRID 8
9 0.2 10 0.3 11 0.2 0.2 no sample 21 2.4 no sample 22 0.4 2.3 0.3 24 no sample 23 13 14 0.3 15 0.3 16 0.2 34 no sample 24 no sample 25 0.4 0.3 0.5 no sample 25 0.3 no sample 25	٤					18 < MDL
21 2 2.3 24 23 24 28 24 28 24 28 24 28 24 28 24 28 28 24 28 28 24 28 28 28 28 28 28 28 28 28 28 28 28 28		¥ .			12 0.2 no semple	
13 14 0.3 16 0.2 38 17 0.4 17 18 19 0.3 19 0.3 10 sample	- HDL	21 < HDL			24 no semple	28 V HOT
17 18 19 20 no sample		13 < PDL				% *
THE PARTY OF THE P		17 no sample	18		20 no sample	<b>10.</b> •
UNITS: Mg/H3 GRID HOL: U.U300 Mg/SAMPLE EXHAUS! DUC!:	T TYPE: WH	NO NO	17S: mg/H3	GRID MDL: 0.0	368 mg/SAMPLE	I Exhaust du

XAY TOPCOAT PAGE 1 OF 2 IE	MIBK TOLUENE ACETATE BENZENE XYLENES (ug) (ug) (ug) (ug)
GUNSHIP GRAY C141 ENGINE	MEK M.
PAINT: (	RUN TIME (min)
STS 8485	POST-CAL (ml/min)
TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 848	PRE-CAL (ml/min)
IKAVIS PAINT E ACUREX	PUMP #(
#6 00 00	ACUREX SAMPLE #
06-30-92 PM NIOSH 1300	ACUREX TUBE #
DATE: 0 DATE: 0 METHOD: 1	GRID LOC

		. di di di
BN & LJL LJL	XYLENES (mg/M3)	2 11.1 2 1.10 2 1.11 2 1.00 2 1.00 2 1.00 2 1.00 3 1.00 3 1.00 1 1.00 3 1.00 1
	ETHYL BENZENE (mg/M3)	* MDL * MDL
PAGE 2 OF 2 D E INITIALS: Q A INITIALS:	BUTYL ACETATE (mg/M3)	0.00.00.4444.00.00.444.00.00.00.00.00.00
200	roluene (mg/M3)	0.7 0.8 0.8 0.8 0.8 0.7 0.7 0.7 0.9 1.1 1.1 1.1 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9
	MIBK (mg/M3)	12.5 12.5 12.5 10.1 10.1 16.9 16.9 16.9 16.9 16.9 16.7 17.4 17.4 17.4 17.4 17.4 17.4 17.4 17
	MEK (mg/M3) (	AML AND SAMPLE OF SAMPLE O
	AVG FLOW (L/MIN) (t	1.052 1.048 1.048 1.077 1.082 1.082 1.082 1.060 1.060 1.060 1.061 1.062 1.062 1.063
#6 PM 00	ACUREX AMPLE #	90099981000 90100182 90100182 90100188 90100788 90100788 90101384 90101788 90101788 90101788 90101788 90101788 90102384 90102384 90102384 90102384 90102384 90102384 90102384 90102384 90102384 90102386 90103384 90103182 90103182 90103188 90103188 90103188 90103188 90103188 90103188 90103188 90103188 90103188 90103188 90103188 90039788 90039788 90039788 90039788
ORGANICS #6 06-30-92 PM NIOSH 1300	ACUREX TUBE #	249 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9
TEST: 0 DATE: 0 METHOD: N	GRID LOC	2 DUP 2 2 3 DUP 4 4 4 4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6

INLET GRID B Field Blank < MDL 9.0 7.0 0.5 0.7 0.7 D E INITIALS:BN & LJL Q A INITIALS:LJL 8 20 Ē EXHAUST DUCT: RECIRC DUCT: 1.0 1.2 2.0 24 < MOL 7.3 GRID MDL: 0.0115 mg/SAMPLE PAINTER MOL: 0.0115 mg/SAMPLE 2 12 16 1.2 2.6 1.6 4.7 17.7 1: **EXHAUST GRID** 4 23 15 Ξ TRAVIS AFB
PAINT BOOTH TESTS
ACUREX PROJECT 8485 18 nosample OSHA TUA:590 mg/H3 6.0 0.0 0.7 1.1 1.3 UNITS: mg/H3 9 22 7 0.7 0.8 0.7 7.0 6.0 7.0 PAINT TYPE: GUNSHIP GRAY TOPCOAT 4 ĭ 2 'n 0 OBJECT: C141 ENGINE Painter Under Painter Over no sample TEST: ORGANICS #6 DATE: 06-30-92 PM METHOD: NIOSH 1300 INLET GRID A GRID CHART 1 - MEK 0.5 no sample 9.0 0.7 ş ٤ ā

INLET GRID B Field Blank < MDL 18.8 18.3 9.6 8.2 8 6.0 D E INITIALS:BN & LJL Q A INITIALS:LJL 器 2 恕 EXHAUST DUCT: RECIRC DUCT: 12.6 14.4 PAINTER MDL: 0.0095 mg/SAMPLE 14.3 15.6 GRID MDL: 0.0095 mg/SAMPLE 15.2 10.1 2 2 2 2 • 39.9 34.8 32.0 20.5 19.5 16.9 12.5 14.5 4 **EXHAUST GRID** ຄ 5 Ξ TRAVIS AFB
PAINT BOOTH TESTS
ACUREX PROJECT 8485 18 no sample OSHA TWA: 205 mg/M3 16.7 18.4 21.6 17.1 16.7 13.5 UNITS: mg/M3 \* 9 22 • ~ 11.5 13.3 13.7 14.4 12.6 15.1 PAINT TYPE: GANSHIP GRAY TOPCOAT 5 17 2 0 'n OBJECT: C141 ENGINE Painter Over no sample Painter Under ...... TEST: ORGANICS #6 DATE: 06-30-92 PM METHOD: NIOSH 1300 INLET GRID A GRID CHART 2 - MIBK 9.0 8.8 11.1 × న **≤** 

D E INITIALS:BN & LJL Q A INITIALS:LJL		Field Blank	INLET GRID B	1.0	28 1.0	E E		 Exhaust duct: 0.8
		9.0	0.5	1.3	2.1	7.0	<b>:</b>	
		4	€	12	%	2	23	GRID MDL: 0.0114 mg/SAMPLE
		0.8	7.0	£.0	£ .	7	7.0	ID MDL: 0.
TESTS CT 8485	EXHAUST GRID	м	^	=	n	<b>2</b>	5	185
TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485	EXH	0.8	8.0	6.0	4.0	6.0	18 no sample	mg/H3
TRA PAI		Z	<b>10</b>	10	22	<b>4</b>	<b>25</b> 6	UNITS: IN
		0.7	9.0	7.0	7.0	8	6.0	
		-	'n	•	7.	2	11	
ORGANICS #6 06-30-92 PM NIOSH 1300	RT 3 - TOLUENE	Painter Over   no sample   Painter Under   5.9	WLET GRID A	0.1	2A 0.5 no sample	, ,	· · · · · · · · · · · · · · · · · · ·	
TEST: ORGANICS #6 DATE: 06-30-92 PM METHOD: NIOSH 1300	GRID CHART 3 - TOLUENE	Painter Over   no sample   Painter Under   5.9	INLET GRID A	1.0 1.0	2A 0.5	s s		

6.0

RECIRC DUCT:

PAINTER MOL: 0.0114 mg/SAMPLE

OSHA TWA:375 mg/M3

OBJECT: C141 ENGINE

INLET GRID B Field Blank < MDL 5.5 5.3 3.0 3.4 2.5 D E INITIALS:BN & LJL Q A INITIALS:LJL 7 9 8 EXHAUST DUCT: RECIRC DUCT: 3.8 3.3 5.9 4.0 4.8 GRID MOL: 0.0116 mg/SAMPLE PAINTER HOL: 0.0116 mg/SAMPLE 2 42 ž 尽 0 M 3.6 6.3 11.1 5.0 7.7 **EXHAUST GRID** 2 6 = ĸ TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485 18 no sample OSHA TUA:710 mg/H3 8.4 5.4 6.2 3.9 6.9 UNITS: Mg/HG 2 22 # 4.0 4.3 3.9 3.4 3.6 4.4 PAINT TYPE: GUNSHIP GRAY TOPCOAT 2 17 ~ OBJECT: C141 ENGINE GRID CHART 4 - BUTYL ACETATE Painter Over no sample Painter Under 0.5 . . . . . . . . . . . . . . TEST: ORGANICS #6 DATE: 06-30-92 PM METHOD: NIOSH 1300 INLET GRID A 2.7 no sample 5.6 3.5 ş ٤

INLET GRID B Field Blank < MOL 0.2 0.2 0.3 D E INITIALS:BN & LJL Q A INITIALS:LJL # • #0 ∟ RECIRC DUCT: < NOL 28 B EXHAUST DUCT: 0.2 0.2 12 < PDL 24 NOL > 20 < MDL GRID MOL: 0.0117 mg/SAMPLE PAINTER MOL: 0.0117 mg/SAMPLE JOH Y 9 < MDL 0.2 0.2 0.5 0.5 0.2 **19** v EXHAUST GRID TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485 Ξ 23 45 4 18 nosample OSHA TWA:435 mg/H3 0.2 2.0 0.3 UNITS: mg/M3 JŒ V JOH > 2 22 # ~ 0.2 104 > 1 1 5 < MOL ( 21 **+10**L · HDL JOH V PAINT TYPE: GUNSHIP GRAY TOPCOAT ħ OBJECT: C141 ENGINE GRID CHART 5 - ETHYL BENZENE Painter Over no sample Painter Under < MDL TEST: ORGANICS #6 DATE: 06-30-92 PM METHOD: NIOSH 1300 INLET GRID A no semple MA MOL 2 × × ×

TEST: ORGANICS #6 DATE: 06-30-92 PM METHOD: NIOSH 1300

GRID CHART 6 - XYLENES

TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485

D E INITIALS:BN & LJL Q A INITIALS:LJL

Painter Over   no sample Painter Under   < MDL	<b>~</b>	6.0	6.0	1.1	7.0 4		Field Blank < MDL
INLET GRID A	īv	-	 1.1	1.0	8 1.0	Z !	INLET GRID B
14 0.8				•		2	0.8
<u></u>	6	1.0	10 1.3	11 2.3 2.2	12 1.0		
ZA 0.7 no semple	r.	<del>-</del>	72 1.2 1.0	1.7	24 MDL <	58	0.7
; *	13	1.0	14 1.5	15 2.5	16 0.8	5.	9.0
	21	6.0	18 nosample	40 3.8 3.0	20 0.7		
PAINT TYPE: GINSHIP GRAY	GRAY TOPCOAT	COAT UNITS:	UNITS: mg/H3	GRID MOL: 0.	GRID MDL: 0.0368 mg/SAMPLE	EXHAUST DUCT:	1.3
	5	OSHA TVA	OSHA TWA: 435 mg/H3	PAINTER MOL: 0	PAINTER HOL: 0.0368 mg/SAMPLE	RECIRC DUCT:	

TEST: DATE: METHOD:	SINGLE PASS 07-01-92 AM: NIOSH 1300	SINGLE PASS ORGANICS 37-01-92 AM1 VIOSH 1300		TRAVIS AF PAINT BOC ACUREX PF	TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485	35	PAINT: OBJECT:	GUNSHIP GRA	SUNSHIP GRAY TOPCOAT C141 ENGINE		PAGE 1 OF	2
GRID LOC	ACUREX TUBE #	ACUREX SAMPLE #	PUMP #	PRE-CAL PUMP #(ml/min)	POST-CAL (ml/min)	RUN TIME (min)	MEK (ug)	MIBK (ug)	TOLUENE (ug)	BUTYL ACETATE (ug)	ETHYL BENZENE ) (ug)	XYLENES (ug)
3 DUP 3 S S S S S S S S S S S S S S S S S S	2 22		28 28 28 29 29 29 29 29 29 29 29 29 29 29 29 29	1000 1000 1000 1000 1000 1000 1000 100	10020 10031 10031 1001 1001 1001 1001 10	671 688 687 688 688 688 688 688 688 688 688	ND ND 24 117 117 117 117 117 117 117 117 117 11	ND ND ND ND ND ND ND ND ND ND ND ND ND N		ND 36 ND 34 104 105 105 105 103 303 303 303 303 303 303 303 303 303		N N N N N N N N N N N N N N N N N N N
288 288	295 88F	90036382 900383 90038485	9 -	936 1036 997	1020	67 68 68	222	222	222	222	299	222
F BLANK EXHAUST SPLIT	304		337	1029 1020	1014 993		20 18	222 221	13 ND	74	Q Q	S S

TEST: DATE: METHOD:	SINGLE P/ 07-01-92 NIOSH 13(	PASS ORGANICS 2 AM1 300					PAGE 2 OF D E INITI Q A INITI	2 ALS: ALS:	BN & LJL LJL
GRID LOC	ACUREX TUBE #	ACUREX SAMPLE #	AVG FLOW (L/MIN)	MEK (mg/M3)	MIBK (mg/M3)	TOLUENE (mg/M3)	BUTYL ACETATE (mg/M3)	ETHYL BENZENE (mg/M3)	XYLENES (mg/M3)
	321	900389896	1.039	< MDL	1.0	< MDL	0.5	< MDL	< MDL
2	322		1.0435	동	, ADL	동	× ÆDĽ	₩ •	WDL v
က	297	9007998928	1.0395	0.2	2.3	0.5		₩	₩ •
3 DUP	248		1.022	0.0	5.6	· MOL		ADL V	A A
4	301		1.026	0.0	o.1 0.0	2.0		A0F v	- ADE
vo i	299	90105384	1.013	0.5	2.2	2 2 2	20.	ADL V	\ \ \
ω.	303		1,0035	0.0	4.1	- F	 	\ V	< MUL <
7	296	90105788	1.013	9.0	5.7	2	J	를 등 V '	
ω .	290		0.891	9.	λ, 4.				٧,
ത	302	90128687	-	aldwes or	no samp	no sample	dwes ou	=	(V)
10	291		1.0365	0.3	4.5	× MOL	4.4	¥0Ľ •	< MDL
11	292		0.981	0.7		0.4		0.2	1.3
11 DUP	293		1.0595	9.0	14.8	0.4		0.5	1.3
12	312		1.018	0.5	4.6	√ ¥DL ×	1.6	^ ÆDL	< MOL
21	244		0.979	× ADL	< MOL	< MOL	< MDL	^ ÆDL	· 전 ~
22	294	90131283	0.9875		4.4	0.2	1.4	JG₩ >	< MDL
22 DUID	302		1.041	0.3	4.3	V WDF	1.5	< MDL	^ MOL
	54		0.9855		14.3	0.4	5.4	0.5	1.5
22	320		1.0055		4.9	< MDL	1.6	< MDL	< MDL
· ·	312		1.026	. 1	1.4	0.4	< MDL	< MDL	< MDL
7	308		1.002	0.3	, S	0.2	1.7	< MDL	0.4
+ LC	300		1.026	0.0	12.2	- MDL	3.9	0.5	1.0
15 210	307	90132485	1.0355	0.8	14.0	0.5	4.6	0.5	2.7
16	308	90	1.0485	0.4	3.2	< MDL		< MDL	< MDL
17	000	90	1.019	< MDL	1.2	0.5	× MDL	< MDL	< MDL
a c	202		1 0385	0.5	i en	A MDP		YOU >	< MDL
9 0	200		0 9835	0 6		WD.		× MDE	- MDI
n C	200	00130880	1 0425	0	, 0	QW V	8	× MDI	V WDI
2 2 2 2	250		0 008	0.0	7				0.3
r over	O LO		000.0	, ica	MO.				
r under	2337		1010	707	12		N. I.		WDI
IA	311		1.0103	101	י א ער א	105	12	Jack v	NO.
2A	281F		1.025	- MUL	70L V	JOH V	7	100	NOI V
3A	280F	900364	1.038	A MUL	AUL >	10E >	A MUL	JOE V	7
18	295	O	0.9795	~ MDL	- MDL >	< MDL	- MDL	MUL V	× MUL
28	88F	9	1.028	< MDL	ADL ADL	· MDL	WDI v	- MDL	MUL >
38	318	90038485	0.9805	YDF >	< MOL	· MOL	× MDL	· MDL	· MDL
F BLANK				_	d	5	eno sample	-	eno sample
EXHAUST	304	900287&308	1.0215	0.3	3.4	0.5	1.1	JOH >	\ \ \ \ \
SPLIT		900309&26	1	0.3	3.7	< MDL	1.2	< MDL	< MUL

INLET GRID B Field Blank no semple D E INITIALS:BN & LJL Q A INITIALS:LJL 0.3 0.3 38 < PDL 10E V 180 EXHAUST DUCT: PAINTER MOL: 0.0115 mg/SAMPLE SINGLE PASS DUCT: 0.3 7.0 0.5 0.5 7.0 0.9 GRID MOL: 0.0115 mg/SAMPLE 12 9 ೭ 24 0.2 7.0 9.0 0.0 3.9 EXHAUST GRID 4 4 Ξ 23 TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485 OSHA TWA:590 mg/M3 0.3 0.3 0.3 0.3 0.5 ě V UNITS: Mg/M3 2 22 13 4 ~ 9 g no sample 0.2 21 < HOL 13 < 10L <u>6</u> 17 < 180 L PAINT TYPE: CLIMSHIP GRAY TOPCOAT 'n OBJECT: C141 ENGINE Painter Over TEST: S.P. ORGANICS DATE: 07-01-92 AM1 METHOD: NIOSH 1300 INLET GRID A Painter Under < MDL GRID CHART 1 - MEK 14 A 1901 ¥ ✓ 101 24 \* FBL

INLET GRID B .............. Field Blank no sample 3.4 3.7 D E INITIALS:BN & LJL Q A INITIALS:LJL 38 88 , 88 18 POL EXHAUST DUCT: PAINTER MDL: 0.0095 mg/SAMPLE SINGLE PASS DUCT: GRID MDL: 0.0095 mg/SAMPLE 2.5 3.4 4.6 4.9 3.2 6: 20 2 12 54 12.2 5.3 2.3 5.7 13.6 14.3 EXHAUST GRID \$ **‡** 2 = TRAVIS AFB
PAINT BOOTH TESTS
ACUREX PROJECT 8485 OSHA TWA: 205 mg/NG 3.3 4.5 5.5 4.4 UNITS: Mg/M3 JŒ v ₩ 2 # 22 9 9 no sample 1.2 21 < PDL 1.4 1.0 2.2 PAINT TYPE: GUNSHIP GRAY TOPCOAT 1 7 OBJECT: C141 ENGINE TEST: S.P. ORGANICS DATE: 07-01-92 AM1 METHOD: NIOSH 1300 INLET GRID A Painter Over 3.2 Painter Under < MOL GRID CHART 2 - MIBK 34 00. 14 A MDL 2A MOL

Q A INITIALS: LUL	Field Blank no sample	INLET GRID B	10 <b>4</b> >	28 < MDL	P. Y		-
	7 0.2	8 * *	12 <b>*</b> * * * * * * * * * * * * * * * * * *	24 MDL	55 JOS ,	20 • <b>10</b> 1	GRID WOL: 0.0114 mg/SAMPLE
TH TESTS OJECT 8485 EXHAUST GRID	3 0,2 < MDL	10H >	11 0.4 0.4	23 0.4	15 < MOL 0.2	19 • MOL	GRID WOL: 0.0114 mg/SAMPLE
PAINT BOOTH TESTS ACUREX PROJECT 8485 EXHAUST GR	2 < HDL	9 10H >	10	22 0.2 + MDL	14 0.2	18 < MDL	IS: mg/N3
	1 < HDL	S + 10L	9 no sample	21 < 70L	13 0.4	17 0.5	TOPCOMT UNITS:
DATE: 07-01-92 AN1 ETHOD: NIOSH 1300 NID CHART 3 - TOLUENE	Painter Over 0.4 Painter Under 0.5	INLET GRID A	JG *	2A < HDL	¥,		PAINT TYPE:GUNSHIP GRAY TOPCOAT

INLET GRID B Field Blank no sample 1.2 7 D E INITIALS:BN & LJL Q A INITIALS:LJL 38 \* PDL 38 \* **H**DF e V E EXHAUST DUCT: PAINTER MOL: 0.0116 Mg/SAMPLE SINGLE PASS DUCT: GRID MDL: 0.0116 mg/SAMPLE 8.0 9.0 1.2 4.6 1.6 1.0 12 9 2 ź 80 3.9 0.5 1.9 5.5 5.4 1.3 EXHAUST GRID 19 Ξ n \$ TRAVIS AFB
PAINT BOOTH TESTS
ACUREX PROJECT 8485 OSHA TWA:710 mg/M3 1.7 6.0 1.5 1.4 1:4 UNITS: Mg/M3 A MOL 9 \* ₽ 22 9 no sample 8.0 0.5 21 < MDL 17 < MOL 13 < MOL PAINT TYPE:GUNSHIP GRAY TOPCOAT OBJECT: C141 ENGINE GRID CHART 4 - BUTYL ACETATE Painter Over TEST: S.P. ORGANICS DATE: 07-01-92 AN1 METHOD: NIOSH 1300 Painter Under 0.5 INLET GRID A 10H × 34 • MOL ¥ ¥

INLET GRID B Field Blank no sample D E INITIALS:BN & LJL Q A INITIALS:LJL ₩ \* 로 \* 19 • 190 EXHAUST DUCT: < MOL PAINTER MOL: 0.0117 mg/SAMPLE SINGLE PASS DUCT: < NOL GRID MOL: 0.0117 mg/SAMPLE 24 < MDL 20 < MDL A MOL **M A D L** 12 < MDL 16 < **H**DL 0.5 0.2 0.5 19 < MDL ਹੁੰ ਦੇ • • TOH > **EXHAUST GRID** Ξ n 5 TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485 OSHA TWA:435 mg/H3 10 \* MOL 14 < PDL → MDL JOH > UNITS: Mg/H3 9 ~ 9 no sample 17 < MOL 10H > 13 < MOL < HOL A MOL 21 PAINT TYPE: GUNSHIP GRAY TOPCOAT OBJECT: C141 ENGINE GRID CHART 5 - ETHYL BENZENE Painter Over 0.2 TEST: S.P. ORGANICS DATE: 07-01-92 AM1 METHOD: NIOSH 1300 Painter Under 0.2 INLET GRID A 2A < MDL 34 ADL A

INLET GRID B Field Blank no sample D E INITIALS:BN & LJL Q A INITIALS:LJL 등 \* 보다 8 PP ~ EXHAUST DUCT: < MÖL PAINTER HOL: 0.0368 mg/SAMPLE SINGLE PASS DUCT: < NOL = . 70 × GRID MDL: 0.0368 mg/SAMPLE 24 MDL S YOL 76 • PDL 원 **(원** 12 < FDL JOH > 1.0 0.4 10H × 로로 오 EXHAUST GRID 13 = n TRAVIS AFB
PAINT BOOTH TESTS
ACUREX PROJECT 8485 OSHA TUA:435 mg/N3 7.0 9 9 UNITS: mg/M3 10 • 101 18 \* 191 JOH V 4 9 no sample 21 < MDL 17 < MDL تا م <del>اق</del> 10H > JOH V PAINT TYPE: GLMSHIP GRAY TOPCOAT OBJECT: C141 ENGINE GRID CHART 6 - XYLENES Painter Over TEST: S.P. ORGANICS DATE: 07-01-92 AM1 METHOD: NIOSH 1300 Painter Under < MDL INLET GRID A 14 FOL ZY NOT 3A < MOL

TEST: DATE: METHOD:	PARTICULATE 06-19-92 AM NIOSH 500	ATE #1 AM 0		TRAVIS AL PAINT BOX ACUREX PI	S AFB BOOTH TESTS ( PROJECT 8485	85	PAINT: OBJECT:	WHITE TOPCOAT LADDERS	COAT		0 E U	INITIALS: I	161 131 131		
GRID LOC	ACUREX SAMPLE #	FILTER # PUMP	# d#b	PRE-CAL (ml/min)	POST-CAL (ml/min)	RUN TIME	(RAW DATA PRE #1 (9)	(RAW DATA, BALANCE PRE #1 PRE #2 (g) (g)	ACCURACY POST #1 (g)	0.0001) POST #2 (9)	AVG FLOW (L/MIN)	AVG FLOW PRE AVG POST AVG	POST AVG (g)	PART UT	PARTICULATE (mg/M3)
	220006	33	&	1	6 8 8	45	0.0132	0.0132	0.0132	0.0132	3.006	0.0132	0.0132	0.0000	V MOL
~~	820006	162	*			45	0.0128		0.0127	0.0127	3.045	0.0128	0.0127	0.000	V MOL
P7	620006		24			42	0.0116		0.0116	0.0116	3.069	0.0116	0.0116	0.000	× MDL
7	900080		20			41	0.0118	0.0118	0.0118	0.0118	3.076	0.0118	0.0118	0.0000	, MDL
2	900081		35			45	0.0125	0.0125	0.0126	0.0126	3.023	0.0125	0.0126	0.0001	<b>8</b> .0
9	900082		2			32	0.0130	0.0130	0.0132	0.0132	3.084	0.0130	0.0132	0.0002	2.0
7	900083		19			41	0.0126	0.0126	0.0126	0.0125	3.044	0.0126	0.0125	0.000	\ <u>a_</u> >
00	900084		~			75	0.0121	0.0121	0.0120	0.0121	3.057	0.0121	0.0120	0.000	JŒ V
0	900085		32			45	0.0119	0.0120	0.0125	0.0125	3.010	0.0119	0.0125	0.0006	4.7
2	90008		30			42	0.0128	0.0128	0.0129	0.0130	3.041	0.0128	0.0130	0.0002	1.6
=	900087		26			45	0.0132	0.0131	0.0131	0.0131	3.016	0.0131	0.0131	0.000	<b>₩</b> >
12	90008		12			42	0.0132	0.0132	0.0132	0.0132	3.058	0.0132	0.0132	0.0000	JOH >
2	900089		36			17	0.0128	0.0128	0.0135	0.0134	3.003	0.0128	0.0134	0.0006	6.4
22	060006		22			37	0.0133	0.0133	0.0135	0.0135	3.069	0.0133	0.0135	0.0002	8.1
123	900091	116	18			15	0.0125	0.0125	0.0125	0.0126	3.050	0.0125	0.0125	0.000	10H >
24	900092		6			77	0.0125	0.0124	0.0124	0.0125	3.023	0.0125	0.0124	0.0000	10E v
13	900093		31	3091		41	0.0125	0.0125	0.0136	0.0136	3.068	0.0125	0.0136	0.0011	8.7
13 DUP			ສ	3075		75	0.0126		0.0135	0.0136	3.102	0.0125	0.0135	0.0010	7.7
1,4	900095	22	•	3036		42	0.0136		0.0140	0.0140	3.036	0.0135	0.0140	0.0005	3.9
15	960006	'n	ī.	3057		45	0.0125	0.0124	0.0126	0.0125	3.047	0.0124	0.0125	0.0001	<b>80</b>
16	60006		•	3082		45	0.0115	0.0115	0.0115	0.0115	3.068	0.0115	0.0115	0.000	실 *
17	860006		33	3000		75	0.0132	0.0131	0.0143	0.0143	3.053	0.0132	0.0145	1,00.0	9.0
	660006	102	፠.	3048		25	0.0132	0.0133	2710.0	0.0142	5.054	25.00.0	2410.0		) · c
18 000				2040		J.	0.0125		0710.0	0.0160	0.00	0.00	0310.0		
19	900101		<b>S</b> :			75	20.0	0.010	0.0120	9110.0	3.032	20.0	0.01		- 4
	200102					74	0.0163	0.0124	0.0123	0.0120	000	420.0	0.0160	0.000	
•			82			5	0.0120	0.0120	0.01	0.070	3.038	0.070.0		0.000	· ·
P under	900136		2			14	0.0128	0.0128	0.0128	0.0128	5.021	0.0128	0.0160		
<b>×</b>	200071		2			74	2210.0		2710.0	2710.0	5.081	0.0122	0.0122	0.000	
₹.	20006	-	\$	•		75	0.0118		0.0118	9110.0	3.023	9110.0	0.0178	0000	
Y.	900073		2'	3006		25	9110.0	96	91.0.0	0.0120	25.5	0.0120	0.0120		2 3 V V
9	900004		M)	5045		Ţ:	7110.0	9	0.0117	0.0118	5.035	0.011	20.0	0.000	
28	20002	157	13	3054	3048	3.	0.0132	0.0133	0.0132	0.0152	2.02 2.02 2.03	0.0132	0.0152		
90	9,000,0		72	2064		*	0.0164	0°0154	0.0163	4310.0	0.0	***	3		2
RECTRC											0	00	0	0.0000	2 2

INLET GRID B EXHAUST DUCT:no sample RECIRC DUCT: no sample D E INITIALS: BN & LJL Q A INITIALS: LJL 78 \* **H**DF 点 人 月 # \* #DL 24 × MDL JOH Y 12 \* #DL 16 • MOL **10** GRID MDL: 0.1 mg/SAMPLE PAINTER MOL: 0.1 mg/SAMPLE 20 3.1 8.0 ± , 23 • **30 JOH >** Y MOL 2 **EXHAUST GRID** 4 TRAVIS AFB
PAINT BOOTH TESTS
ACUREX PROJECT 8485 OSHA TUA: 40 mg/H3 2.0 1.6 3.9 7.0 1.8 UNITS: Mg/H3 <u>5</u> 2 # **\$** 22 2 8.6 7.7 0.8 4.9 4.7 <u>1</u>0. 17 21 5 PAINT TYPE: WHITE TOPCOAT OBJECT: LADDERS GRID CHART - PARTICULATE TEST: PARTICULATE #1 DATE: 06-19-92 AM METHOD: NIOSH 500 Painter Over 41.0 INLET GRID A Painter Under < MDL 74 101 101 34 \* NO 24 **HO**L

	T WT PARTICULA	٧	0.0000 < MDL	٧	٧	٧		0.0	7.1 2000	0.0002	0.0008	0.0008 7.5	9.5	2.6		0.0012 10.4				6.2 6000					0.0001		•	,	· •	0.000	٧	٧	0.000 × MDL		×	-
ויו ריו	POST AVG PART WT (9)					0.0134 0.0						0.0139 0.0													0.0120 0.0						0.0125 0.0					
INITIALS: BN INITIALS:	PRE AVG (9)																					0.0135			9110						0.0125			0.0121		
DD	AVG FLOW	3.032	3.077	3,095	3.059	3,103	3.026	3.097	3, 126	3.017	3.071	3,152	3,381	3.011	3.032	3.033	3.030	3.062	3.024	3.005	3.011	3.027	2.997	2.99	3.054		200.0	200 2	200	3,130	3.090	3.064	3.074	3,003	3,000	
	POST #2 (g)	0.0123	0.0122	0.0122	0.0117	0.0134	0.0116	0.0129	0.0133	0.0118	0.0123	0.0138	0.0126	0.0139	0.0128	0.0138	0.0124	0.0136	0.0127	0.0133	0.0143	0.0145	0.0139	0.0125	0.0120	0.00	0.0134	0.0125	0.0116	0.0124	0.0125	0.0134	0.0123	0.0130	0.0131	
PRIMER	POST #1	0.0122	0.0123	0.0121	0.0118	0.0134	0.0116	0.0129	0.0133	0.0118	0.0123	0.0139	0.0126	0.0140	0.0129	0.0138	0.0124	0.0136	0.0127	0.0133	0.0144	0.0145	0.0139	0.0125	0.0119	0.0100	0.00	0.0125	311	0.0124	0.0126	0.0136	0.0124	0.0130	0.0132	
LT GREEN BOWSER	PRE #2 (g)	0.0123				0.0133	0.0115	0.0128	0.0131	0.0116	0.0115	0.0131	0.0119		0.0120				0.0125	0.0124	0.0134				0.0119		0.0	125	4110	0.0125	0.0125	0.0134	0.0124	0.0121	0.0132	
PAINT: OBJECT:	PRE #1	0.0123							_											0.0124					0.0120		0.0131				0.0126		0.0124	0.0121	0.0132	
82	RUN TIME (min)																						8		2.5								45	17	200	)
RAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485	POST-CAL (ml/min)																								3051	••					•••					
TRAVIS AFB PAINT BOOT ACUREX PRO	PRE-CAL (ml/min)																								3057											
	FILTER # PUMP #	26 33																							183 26									80 27		
ULATE #2 92 PM 500	**																																			
: PARTICULATE :: 06-19-92 PM := NIOSH 500	ACUREX IC SAMPLE	1 900109	2 900110	3 9001	4 9001	5 900113	6 9001	7 9001	8 9001	9 9001	0 9001	1 9001	2 900120	_				24 900124	3 9001	4 9001		16 9001	7 900129		19 900131		000130		2A 9001		A 900105		B 900107	38 900108		
TEST: DATE: NETHOD:	GRID LOC										•	-	-	2	2		2 2 2 3	2	-	-	_	_	-	-	- 6	9	advar d	5	- ~	2A DUP			. 17	100	F BLANK	-

INLET GRID B field Blank < MOL EXHAUST DUCT: no sample RECIRC DUCT:no sample 7.3 85 A 104 D E INITIALS: BN & LJL Q A INITIALS: LJL 20. V 10. S 10.0 1.7 5.6 6.9 8.3 ^ ÆDL PAINTER MOL: 0.1 mg/SAMPLE GRID MDL: 0.1 mg/SAMPLE 2 16 12 2,5 80 6.5 7.9 7.5 10.4 8.0 10H > EXHAUST GRID \$ 2 ຄ = TRAVIS AFB
PAINT BOOTH TESTS
ACUREX PROJECT 8485 OSHA TWA: 77 mg/M3 7.9 5.6 6.9 6.9 mg/M3 0.8 j<del>o</del> **2**2 0 # 22 UNITS: 6.0 1.7 5.6 1.7 , <u>1</u>0, ^ MDL 17 13 7 PAINT TYPE: LT GREEN PRIMER OBJECT: BOWSER GRID CHART - PARTICULATE TEST: PARTICULATE #2 DATE: 06-19-92 PM METHOD: NIOSH 500 Painter Over INLET GRID A Painter Under < MOL 14 • #0! 7 FE FE 조 \*

	PART WT PARTICULAT (g) (mg/M3)			2	000		C. 0	- E	0.5	0.5	YOH Y	1.8	1.8		0	9	ָ ק ק				2.5	- c	0.	0.1	ر آو د	0.0	7.5	0.0	13.1		10±	_ ₩ •	\ #DL		) (		no somole	no sample	
	PART UT (g)	0 000	0.000	0 0001	2000	2000	0000	<b>0,000</b>	0.0001	0.0001	0.000	0.0004	7000 0	0.005	2000	0000	2000	2000	0000	0000	0000	0000	5.00.0	0.000	0.000	0.0013	0.0016	2100.0	0.0025	0000	0000	0000	0.000	0000	0000	900	0000	0.000	
BN & LJL LJL	OST AVG	0 0126	0.0123	0.0134	7010	2.00	0.0123	0.0133	0.0132	0.0128	0.012	0.0126	0.0139	0.110	0.0124	0122	35.00	0.0127	7.10.0	0.0	0.0155	0.0141	0.0149	0.0151	0.0132	0.0141	0.0132	2510.0	0.0153	0.0126	0.0125	0.0131	0.0126	0.0125	0.013	0.0.0		0	
INITIALS: EINITIALS:	PRE AVG POST AVG (g)	0 0126	0.0123	0 0133	0.000		0.0124	0.0133	0.0131	0.0127	0.0132	0.0122	0.0135	0.0134	0.0122	0.0124	0.000	20.0	0.0155	0.0153	20.00	40.0	0.0134	0.0127	0.0132	0.0128	0.0116	210.0	0.0128	0.0126	0.0126	0.0131	0.0126	0.0125	0.013	25.0		0	
0 Q A A	AVG FLOW (L/MIN)	3 005	3,035	770 2	10°0	7.00	2.022	3.058	3.048	3.035	3.031	3.048	3.014	4 030	4.050	200.5	200.5	7007	10.504	7.0	2.025	5.025	3.008	5.077	3.088	5.010	3.091	3.000	2.726	3.027	3.079	3.027	3.052	3.026	3.014	2.988	000	0.000	
& WHITE TOPCOAT & LADDERS	POST #2 (g)	0.0127	0.0123	7210 0	0.0134	0.0127	0.0124	0.0154	0.0132	0.0128	0.0120	0.0126	0.110	0 0130	7210.0	20.0	0.0122	0.0130	2410.0	44.000	0.0155	0.0141	0.0149	1510.0	0.0133	0.0141	0.0132	0.0132	0.0153	0.0125	0.0125	0.0131	0.0126	0.0125	0.0129	9,00	0.012		
SE & WHITE	POST #1 (g)	0 0126	0.0123	0.0136	0.0134	20.00	6,000	0.0135	0.0133	0.0128	0.0120	0.0126	0.0140	0110	0.00	20.0	2000	0.0169	2410.0	44.0.0	0.0155	1910.0	0.0149	1510.0	0.0132	1,000	0.0132	0.0132	0.0153	0.0126	0.0125	0.0131	0.0126	0.0125	0.0130	0.0116	0.0123		
RED H208ASE Bowser	PRE #2 (g)	0 0126	0.0123	0 0133	20.0	0.012	0.0124	0.0134	0.0131	0.0127	0.0131	0.0122	0.0130	0.0135	2010	20.00	0.0123	0.0	0.0135	0.0154	0.0150	0.0154	0.0134	0.0126	0.0132	0.0128	0.0116	0.0120	0.0128	0.0125	0.0126	0.0131	0.0126	0.0125	0.0130	0.0125	6310.0		
PAINT: OBJECT:	PRE #1	0 0126	0 0124	0 0133	2000	0.012	0.0124	0.0133	0.0131	0.0127	0.0132	0.0122	0110	0.013%	2000	0.00	0.0163	710.0	0.0130	0.0135	0.0130	0.0134	0.0134	0.0127	0.0132	0.0128	0.0116	0.0120	0.0128	0.0126	0.0126	0.0131	0.0126	0.0126	0.0130	0.0126	0.0163		
10	RUN TIME (min)	20	22	7.	7	2 £	21	7)	71	7	2	K	2	7 4	3.5	2*	- t	2,	21	21	21	e;	K :	K	7	2	2	22	2	2	2	2	2	2	69	\$ 9	60		
VIS AFB NT BOOTH TESTS REX PROJECT 8485	POST-CAL (ml/min)	2080	3021	202	2005	0000	5045	3085	3021	2997	3035	3033	2088	3012	1002	2000	7117	2703	3204	2000	3000	3000	3030	3129	3110	2074	3151	2954	5400	2988	3097	3003	3021	3012	3000	98	0067		
TRAVIS AFB PAINT BOOT ACUREX PRO	PRE-CAL (ml/min)	4030	\$70£	2012	2012	200	2000	3030	3075	3072	3027	3063	3030	3002	2002	3002	0000	3026	3204	3027	2000	2040	2985	3024	3066	3045	3030	3045	3051	3066	3060	3051	3082	3039	3027	3015	2051		
	*	α	<b>&gt;</b> <	א נ	3.	- ;	7	7	33	4	7		17		4 5	2 2	100	2 0	77	Ž,	<u>ج</u>	>	75	9	8	=	ກ	<b>4</b> 3	7	32	13	M	೩	27	8	9	<u> </u>		
F #3	FILTER # PUMP	2.9	87	5 5	2 -	=	2	2	<del>2</del>	92	-	5	100	105	3	0 1	2	0	132	8	215	27	7.	7.2	9	123	8	802	150	20	Z	144	3	32	8	17	4		
PARTICULATE 06-22-92 AM NIOSH 500	ACUREX SAMPLE # F	800000	00000	00000	¥0000	¥0001	20004	900013	900014	900015	90000	000017	90000	9000	00000	20000	20000	220004	900032	20006	900054	900025	920006	20006	900028	620006	900030	900031	990006	290006	900001	\$00006	200006	200006	900002	20000	2000		•
TEST: F DATE: ( METHOD: N	GRID LOC S		- ^	. P	n \	<b>†</b> 1	^	•	7	**	0	10	-		3.5	7 6	77		23 DUP	47	5.	7	15	91	17	18	19	2	õ	P under	4	2A	2A DUP	34	18	8 ;	SUMMERCE	DELLEC	

INLET GRID B RECIRC DUCT:no sample EXHAUST DUCT:no sample D E INITIALS: BN & LJL Q A INITIALS: LJL 38 • 101 28 • <del>10</del>1 18 • FDL 5.6 6.0 0.5 3.0 4.1 £. GRID MOL: 0.1 mg/SAMPLE PAINTER MOL: 0.1 mg/SAMPLE 2 42 2, \$ 8: N N N 7.0 7.2 0.5 0.5 4 EXHAUST GRID 5 Ξ 23 TRAVIS AFB
PAINT BOOTH TESTS
ACUREX PROJECT 8485 OSHA TUA: 77 mg/M3 6.0 1.8 22 < HOL 3.1 MQ/M3 10H > ig V ₽ 2 7 PAINT TYPE: RED HZOBASE & WHITE TOPCOAT UNITS: 6.0 2.3 0.5 17 < MOL ) 104 × ) FOI > LADDERS 5 2 OBJECT: BOWSER GRID CHART - PARTICULATE TEST: PARTICULATE #3 DATE: 06-22-92 AM METHOD: NIOSH 500 Painter Over 13.1 INLET GRID A Painter Under < MDL 3A MDL ~ 

TEST: DATE: METHOD:	PARTICULATE 06-24-92 AM NIOSH 500	LATE #4 2 AM 00		TRAVIS AFB PAINT BOOT ACUREX PRO	TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485	Z	PAINT: OBJECT:	BLUE WATERBASED COMFORT PALLET	RBASED		D E	INITIALS: INITIALS:	א ב ואן ואן		
GRID LOC	ACUREX	# FILTER # PUMP	*	PRE-CAL (ml/min)	POST-CAL (ml/min)	RUN TIME (min)	PRE #1 (g)	PRE #2 (g)	POST #1 (g)	POST #2 (g)	AVG FLOW	PRE AVG	PRE AVG POST AVG (g) (g)	PART WT (g)	PART WT PARTICULA (g) (mg/M3)
-	900040		2	3051	3030	2	0.0122	0.0122	0.0122	0.0122	3.041	0.0122	0.0122	0.0000	JQE V
2	900041	•	7	2994	3033	20	0.0132	0.0132	0.0132	0.0132	3.014	0.0132	0.0132	0.0000	Y MDL
m	900042		~	2975	3003	54	0.0122	0.0121	0.0123	0.0124	2.989	0.0121	0.0124	0.0003	1.9
4	900043	3 54	17	3051	3042	2	0.0115	0.0115	0.0121	0.0120	3.047	0.0115	0,0121	0.0006	2.8
2	90004	•	22	3009	3069	61	0.0125	0.0125	0.0125	0.0126	3.039	0.0125	0.0125	0.000	MO.
9	900045		19	3051	3097	20	0.0125	0.0125	0.0127	0.0127	3.074	0.0125	0.0127	0.0002	0.0
7	90004	•	8	3015	3110	70	0.0119	0.0118	0.0129	0.0128	3.063	0.0119	0.0128	0.0009	4.2
89	20004		37	3069	3100	2	0.0117	0.0117	0.0127	0.0127	3.085	0.0117	0.0127	0.0010	9.4
٥	900048		9	3042	3042	20	0.0130	0.0130	0.0134	0.0135	3.042	0.0130	0.0134	0.0004	1.9
o DUP	-		7	3009	2942	71	0.0130	0.0130	0.0134	0.0134	2.976	0.0130	0.0134	0.0004	1.9
9	900050		9	3048	3045	2	0.0123	0.0122	0.0133	0.0133	3.047	0.0122	0.0133	0.0011	5.2
-	900051		3	•	3036	2	0.0126	0.0126	0.0148	0.0149	3.058	0.0126	0.0148	0.0022	10.3
	-		F		3003	20	0.0133	0.0133	0.0151	0.0150	3.026	0.0133	0.0151	0.0018	8.5
12 DUP		139	M	3045	3063	2	0.0118	0.0118	0.0133	0.0134	3.054	0.0118	0.0133	0.0015	7.0
21			Ž,		3036	20	0.0131	0.0130	0.0135	0.0134	3.044	0.0130	0.0135	0.0005	2.3
22			8		3006	2	0.0119	0.0119	0.0129	0.0129	3.005	0.0119	0.0129	0.0010	8.4
22		2:	9:		3072	Ri	0.0118	0.0118	0.0141	0.0142	3.050	0.0118	0.0142	0.0024	11.2
77			=;		3045	<b>5</b> 1	0.0126	0.0125	0.0151	0.0151	3.021	0.0125	0.0151	0.0026	12.1
2 +	60000	7	2;	7667	2000	2	0.0122	0.0122	0.0126	0.0126	3.002	0.0122	0.0126	0.0004	5.0
ī.			7	2002	2020	2,5	0.0124	0.0124	0.0152	0.00	3.029	0.0124	0.0132	0.0000	0.0
15 015	900057		, «	3005	3000	22	0.012	0.0124	0.00	0.00	3.050	0.0124		2000	90
		80	20	3018	3063	2	0.0117	0.0117	0.0135	0.0135	3,00	0.0117	0.0135		, ur
17	900059		S	3057	3072	7	0.0122	0.0120	0.0123	0.0213	3,065	0.0121	0.0168	0.0047	21.6
18	90006		18	3048	3006	2	0.0118	0.0118	0.0124	0.0124	3.027	0.0118	0.0124	0.0006	2.8
18 DUP	•		-	2974	2925	7	0.0121	0.0121	0.0129	0.0129	2.950	0.0121	0.0129	0.0008	3.8
45	_		2	3003	3018	2	0.0122	0.0122	0.0147	0.0147	3.011	0.0122	0.0147	0.0025	11.9
			77	3079	3069	23	0.0124	0.0124	0.0152	0.0152	3.074	0.0124	0.0152	0.0028	13.0
2			2	2000	- A	6	1210.0	1210.0	0.0150	0.0150	255.7	1210.0	0.020	0.0029	14.0
P Grader	2000		35	3069	3015	88	0.0155	0.0133	0.0132	0.0132	3.042	0.0133	0.0132	0000	2 V
≤;	_		-!	2002	2542	5;	0.0120	0.0121	0.0121	1210.0	28.2	1210.0	1210.0	0.0000	70.
5.	\$50000 \$20000	7 7	ů,	2020	2000	809	0.017	0.0118	20.00	0.0118	3.059	71.00	8.0.0		C.0.
5			ع ر	2002	2000	5	20.00				7.050	2000	2000		
2 2			ŠK	3070	3054	80	25.0	0.0122	25.0	250	200.8	25	25.0		
35	-		12	3051	3036	90	0 0130	0.0130	0.0141	0110	7	0.140	0.0130		
38 DUP	900039	186	12	2991	3018	69	0.0121	0.0121	0.0121	0.0120	3.005	0.0121	0.0121	0000	
F BLANK	90006		26			69	0.0122	0.0122	0.0122	0.0122	3.000	0.0122	0.0122	0.000	TON V
EXHAUST											0	0.000	0.000	0.0000	40
RECIRC											0	0.000	0.0000	0.000	no semple

D E INITIALS: BN & LJL Q A INITIALS: LJL	6 9 8 8 9 9 9 8 4 4 4 4	Field Blank < NDL	INLET GRID B	104 >	- 10F - 38 	55 A 101	•	EXHAUST DUCT: < MOL
0 Q	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	4 2.8	8 4.6	12 8.5 7.0	12.1	16 8.5	_	
ESTS T 8485	EXHAUST GRID	3 1.9	7 4.2	11 10.3	11.2	15 8.0 6.9	11.9	GRID MOL: 0.1 mg/SAMPLE
TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485	ЕХНА	2 < MOL	9 0.9	10 5.2	22 4.8	3,5 3,6	18 2.8 3.8	UNITS: mg/H3
		4-	S MOL	6.0.	21 2.3	13 .	17 21.6	
TEST: PARTICULATE #4 DATE: 06-24-92 AM METHOD: NIOSH 500	GRID CHART - PARTICULATE	Painter Over 14.0 Painter Under < MDL	INLET GRID A	⊒ ¥ *	2A 0.5	g A		PAINT TYPE: BLUE WATERBASE

TEST: DATE: METHOD:	PARTICULATE 06-29-92 PM NIOSH 500	AF €		TRAVIS AFB PAINT BOOTI ACUREX PRO	AFB BOOTH TESTS PROJECT 8485	22	PAINT: OBJECT:	LT GREEN PRIMER QEC PANELS	PR IMER S		0 E 19	INITIALS: INITIALS:	88 & LJL LJL		
GRID LOC		ACUREX SAMPLE # FILTER # PUMP	** <u>Q</u>	PRE-CAL (ml/min)	POST-CAL (ml/min)	RUN TIME (min)	PRE #1 (9)	PRE #2 (g)	POST #1 (9)	POST #2 (g)	AVG FLOW (L/MIN)	PRE AVG POST AVG	POST AVG (g)	PART UT (g)	PARTICULATE (mg/M3)
	900151	80	55	3010	3033	88	0.0122	0.0122	0.0123	0.0123	3.022	0.0122	0.0123	0.0001	0.5
21	900152	5	25		3033	88	0.0126		0.0127	0.0126	3.017	0.0127	0.0127	0.0000	
<b>57 ·</b>	\$21004	145	7,		***	3	0.0130	0.0129	0.0129	0.0129	5.009	0.0130	0.0129	0.0000	교 ()
\$ 1	\$0012¢	411	Q:		3	8	0.0117	0.017	0.011/	0.011/	3	7110.0	7,110.0	0.000	- - -
<b>^</b>	551004	212	A .		5085	85	0.0131	0.0132	0.0151	0.0151	5.073	0.0151	0.0131	0.000	
		6	3		2002	8	0.0128	0.0128	0.0127	0.0127	200.0	0.0128	0.0127	0.000	101
and o		92	2 :		3003	8	0.0129	510.0	0.0128	0.0129	3.019	0.0129	5.0.0	0,000	) * *
	500158	9	21		2040	8	0.0135	0.0132	0.0133	0.0133	5.021	0.0152	0.0135	0.0001	C.5
10	900159	011	25		3006	8	0.0136	0.0135	0.0136	0.0135	3.021	0.0136	0.0135	0.000	<u> </u>
0	900160	120	33		3069	8	0.0122	0.0123	0.0123	0.0123	3.055	0.0123	0.0123	0.0000	JOH V
0	900161	8	32		3069	8	0.0123	0.0124	0.0124	0.0124	3.065	0.0123	0.0124	0.0001	0.5
=	900162	23	3		3051	8	0.0135	0.0135	0.0136	0.0136	3.026	0.0135	0.0136	0.0001	0.5
12	900163	182	25		3021	8	0.0127	0.0127	0.0127	0.0127	3.027	0.0127	0.0127	0.0000	
21	900164	119	89		3103	19	0.0125	0.0125	0.0125	0.0125	3.069	0.0125	0.0125	0.000	
22			2		3015	8	0.0130	0.0130	0.0131	0.0131	3.008	0.0130	0.0131	0.0001	0.5
53	900166		₹) i		2985	89	0.0119		0.0122	0.0122	2.994	0.0119	0.0122	0.0003	5.5
24	900167		*		2968	8	0.0117	0.0117	0.0118	0.0118	2.987	0.0117	0.0118	0.0001	
13	900168		200		3048	8	0.0134		0.0135	0.0134	3.029	0.0134	0.0134	0.000	⊒, •
41	900169		02		3033	3	0.0128		0.0129	0.0130	3.057	0.0128	0.0150	0.0002	0.
5	2004		5		3048	3	0.0150		0.0133	0.0155	3.058	0.0150	0.0133	0.0003	4.
16	900171		53		3033	8	0.0120	0.0120	0.0121	0.0121	3.042	0.0120	0.0121	0.0001	0°.5
17	900172		20		3033	19	0.0120	0.0121	0.0122	0.0122	3.042	0.0121	0.0122	10000	S. 0
10 t	900173		2		3045	8	0.0155	0.0155	0.0134	0.0155	3,045	0.0155	0.0134	L0000	v.,
61	900174	211	0,0		3082	8:	0.0151	0.0151	0.0134	0.0155	5.061	0.0151	0.0155	0.0002	0.0
			_;		3021	8	0.0128	0.0153	0.0150	0.0130	5.035	0.075	0.0150	0.0001	
20 02	900176		2;		5015	6	0.0155	0.0152	0.0132	0.0155	5.015	0.0155	0.0155	0.0000	ر آھ
			5		2962	10	0.0125	0.0124	0.0126	0.0127	3.003	0.0123	0.0120	0.000	
P under			52		3027	8	0.0152	0.0151	0.0152	0.0151	3.039	0.0132	0.0151	0.000	2
<b>~</b>			28		3012	19	0.0127	0.0127	0.0127	0.0126	3.026	0.0127	0.0127	0.000	- FE
24			43		3054	29	0.0120	0.0120	0.0119	0.0119	3.007	0.0120	0.0119	0.000	10± ×
34			2		3119	29	0.0127	0.0127	0.0126	0.0125	3.090	0.0127	0.0126	0.000	10H >
8			7		3012	28	0.0124	0.0124	0.0124	0.0124	5.996	0.0124	0.0124	0.000	*
18 DUP			4	2975	2884	19	0.0139	0.0138	0.0138	0.0138	2.930	0.0138	0.0138	0.000	<u>1</u> 0.
28			-	2882	3033	3	0.0125	0.0125	0.0125	0.0125	3.012	0.0125	0.0125	0.000	, FDL
38	900150		-	2960	2887	8	0.0130	0.0130	0.0130	0.0130	2.924	0.0130	0.0130	0.000	
F BLANK			M			88	0.0119	0.0120	0.0120	0.0119	3.000	0.0119	0.0120		0.5
<b>EXHAUST</b>											0000	0.0000	0.0000		no semple
RECIRC		•									000.0	0.000	0.000	0.000	no sample

INLET GRID B Field Blank 0.5 EXHAUST DUCT: no sample RECIRC DUCT: no sample 28 < PDL D E INITIALS: BN & LJL Q A INITIALS: LJL 38 • 10 8 < MDL 12 < MDL 0.5 0.5 JOH Y PAINTER MOL: 0.1 mg/SAMPLE GRID MOL: 0.1 mg/SAMPLE 20 2 24 1.0 0.5 1.5 1.4 0.5 **₩** > **EXHAUST GRID** 19 \$ N Ξ TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485 OSHA TWA: 77 Mg/H3 0.5 0.5 0.5 1.0 UNITS: mg/M3 5 5 5 5 5 6 V MOI 13 22 0 7 0.5 0.5 13 < MOL **₩** > V HDL JOH V 11 21 PAINT TYPE: LT GREEN PRIMER OBJECT: QEC PANELS GRID CHART - PARTICULATE TEST: PARTICULATE #5 DATE: 06-29-92 PM METHOD: NIOSH 500 Painter Over 0.5 INLET GRID A Painter Under < MOL 24 • HDL ¥ • 10: 74 \* PDL

•	DATE:		SINGLE PASS PARTICULATE 07-01-92 AM2 NICEL SON	LATE #1		BOOTH TESTS	S	PAINT: OBJECT:	PRIMER RAMP &	& GRAY TOPCOAT QEC PANELS	DAT.	DE	INITIALS: INITIALS:	BN & LJL		
4.5         3009         3013         6.0113         0.0133         0.0133         0.0133         0.0103         0.0132         0.0103         0.0104         0.0132         0.0103         0.0104         0.0132         0.0103         0.0104         0.0132         0.0103         0.0104         0.0132         0.0103         0.0104         0.0132         0.0103	GRID LOC	ACUREX SAMPLE #	FILTER # P		PRE-CAL (ml/min)	POST-CAL (ml/min)	RUN TIME	(RAW DAT PRE #1 (g)	A, BALANCE PRE #2 (9)			AVG FLOW	PRE AVG (9)	POST AVG		PARTICULATE (mg/M3)
900115         4,1         500         5003         6,2         0,012         0,013         0,013         0,013         0,013         0,013         0,013         0,013         0,000         4 months           900187         4,4         53         2597         2991         200         6,0116         0,0116         0,0116         0,0116         0,0116         0,0117         2,997         0,0117         0,0117         2,997         0,0117         0,0117         2,997         0,0117         0,0118         0,0118         0,0117         2,997         0,0117         0,0117         2,997         0,0117         0,0117         2,997         0,0117         0,0117         2,997         0,0117         0,0117         2,997         0,0117         0,0117         2,997         0,011		900185	t t t	3						0.0133	0.0133	3.021	0.0133	0.0133	0.0000	
WOOTS 1         44         58         299, 299, 298, 2013         COURT COURT         COURT C		900186		- 1				_		0.0128	0.0128	3.021	0.0128	0.0128	0.0000	
900185         74         53         2994         303         62         0.0116         0.0117         0.0117         0.0117         0.0117         0.0117         0.0117         0.0117         0.0117         0.0117         0.0118         0.0117         0.0118	~	900187		~				_		0.0132	0.0133	2.963	0.0132	0.0132	0.0000	
900188 175 59 3000 2994 0 62 0.0127 0.0127 2.997 0.0127 2.997 0.0128 0.0107 0.0101 0.5900 0 62 0.0128 0.0127 0.0127 0.0127 0.0127 0.0128 0.0101 0.5900 0 62 0.0123 0.0123 0.0127 0.0122 0.0101 0.5900 0 10 0.0129 0.0129 0.0127 0.0128 0.0127 0.0128 0.0101 0.0132 0.0132 0.		900214		<b>.</b>				_		0.0116	0.0116	3.012	0.0116	0.0116	0.000	X.
900199 155 59 500 5994 62 0.0127 0.0127 0.0127 2.993 0.0127 0.0127 0.0128 0.0129 0.012		900188		•				_		0.0127	0.0127	5.986	0.0126	0.0127	0.0001	0.5
900199 19 53 3009 2857 62 0.0123 0.0124 0.0125 1.0124 0.0125 0.0112 0.0112 0.0112 0.0112 0.0103 0.0019 0.0103 114 24 3025 3005 62 0.0131 0.0121 0.0122 0.011		900189		Ki				_		0.0128	0.0127	2.997	0.0127	0.0128	0.0001	0.5
900192 147 24 800		900190		i Per						0.0124	0.0124	2 983	0.0123	0.0124	0.0001	0.5
11		900101								0.0122	0.0122	000	0 0121	0 0122	0.001	
900193         117         24         306         56         0.0121         0.0123         0.0124         0.0123         0.0124         0.0123         0.0124         0.0123         0.0124         0.0123         <		000100		, =						0.0112	0.0132	A 015	1410	0.01	900	
900194 136 19 2991 2977 62 0.0123 0.0128 0.0128 2.984 0.0121 0.0107 0.0003 2.75 0.0003 0.0003 1.4 0.0003 1.4 130 19 2991 2977 62 0.0117 0.0123 0.0123 2.976 0.0123 0.0107 0.0103 1.0 10103 0.0003 1.4 13 13 13 13 13 13 13 13 13 13 13 13 13		000103		70						7010	0.0126	250.1	1210	0.0124	000	
900213 187 35 2000 3015 62 0.0172 0.0123 0.0123 0.0172 0.0173 0.0000 3.5.2 900174 187 35 2004 3015 62 0.0172 0.0123 0.0123 0.0172 0.0173 0.0100 9.0173 0.0100 9.0173 0.017		000195		4 =						00.00	90.00	2000	7250	0.00 0.00 0.00 0.00	000	
900199         17         5         3049         30		200194		- •						20.00	20000	200	1	20.00	7000	
900195 187 5 2904 2083 2015 0.0152 0.0153 5.0175 0.0152 0.0152 0.0152 1.15 0.0195 1.0000 1.15 0.0195 1.15 0.0195 1				- ;						5710.0	0.0163	2.0.5	710.0	0.0163	0000	3.0
900196 177 2 3027 3018 6.5 0.0157 0.0153 0.0157 3.015 0.0157 0.0157 1.0177 0.0103 1.6 0.0199 1.7 2 502 2 5027 3018 6.5 0.0157 0.0153 0.0159 2.025 0.0153 0.0153 0.0153 0.0159 0.0159 1.6 0.0159	훒			'n						0.0123	0.0123	2.976	0.0123	0.0123	0.000	Ž.
900197 127 7 2 2994 3030 62 0.0133 0.0135 0.0135 2.012 0.0133 0.0135 0.01095 1.6 900197 127 900197 127 7 2 2995 3030 62 0.0133 0.0135 0.0135 2.995 0.0135 0.01095 1.6 900199 104 54 2983 2.995 6.0127 0.0135 0.0135 2.995 0.0127 0.0135 0		-		- •						0.0130	0.0129	3.023	0.0127	0.0129	0.0002	-
900198 143 7 2965 2971 62 0.0133 0.0140 0.0139 2.996 0.0133 0.0199 144 9 900198 143 7 2965 2977 2946 0.0135		-		4						0.0136	0.0135	3.012	0.0133	0.0136	0.0003	9.0
900202 152 31 2977 2940 63 0.0127 0.0137 0.0135 0.0135 2.959 0.0127 0.0130 0.0003 1.6 900201 164 54 2983 2995 62 0.0136 0.0135 0.0135 2.995 0.0135 0.				-						0.0140	0.0139	2.968	0.0133	0.0139	0.0000	N. 3
900200 104 54 2983 2985 62 0.0136 0.0135 2.984 0.0135 0.0035 0.0009 4.9 900200 105 30 30 30 2996 62 0.0136 0.0135 2.997 0.0138 0.0135 0.0004 2.2 900201 103 30 3000 2994 62 0.0136 0.0135 2.997 0.0138 0.0132 0.0004 2.2 900202 107 20 2980 2974 62 0.0136 0.0134 2.0113 2.097 0.0135 0.0105 0.0104 2.2 900203 107 29 3006 3012 62 0.0136 0.0134 3.019 0.0135 0.0105 0.0104 9.8 900204 130 4.7 3000 2988 62 0.0137 0.0135 2.994 0.0137 0.0134 1.0 900205 174 15 2968 2903 63 0.0135 0.0135 0.0135 2.994 0.0137 0.0103 1.6 900206 174 15 2968 2903 63 0.0135 0.0135 0.0135 0.0135 0.0135 0.0101 1.1.7 900207 74 15 2968 2903 63 0.0135 0.0135 0.0135 0.0135 0.0135 0.0135 1.6 900208 174 15 2968 2903 63 0.0135 0	Ž			1						0.0130	0.0129	2.959	0.0127	0.0130	0.0003	9.0
900200 1699 50 3033 2898 62 0.0131 0.0134 0.0132 3.016 0.0131 0.0134 0.0003 1.0 900201 103 200 2994 62 0.0136 0.0132 0.0132 2.977 0.0133 0.0103 0.0004 2.2 900202 107 200 2990 2974 62 0.0135 0.0132 0.0132 2.977 0.0135 0.0103 0.0015 6.2 900204 103 204 55 3006 2998 62 0.0125 0.0134 0.0134 3.090 0.0150 0.0140 0.0014 7.5 900204 120 47 3000 2998 62 0.0121 0.0134 0.0134 3.090 0.0120 0.0114 7.5 900205 142 34 3009 2908 62 0.0131 0.0134 0.0134 3.090 0.0120 0.0103 1.6 900206 174 15 2898 62 0.0131 0.0135 0.0135 0.0135 0.0131 0.0132 1.02 900208 78 10 3015 3110 63 0.0137 0.0137 0.0137 0.0137 0.0137 1.02 900208 78 10 3015 3110 63 0.0137 0.0137 0.0137 0.0137 0.0137 0.0012 1.02 900108 162 299 2993 2995 62 0.0137 0.0137 0.0137 0.0137 0.0137 0.0107 0.0107 0.0020 1.02 900177 196 39 2893 2892 62 0.0137 0.0137 0.0137 0.0137 0.0137 0.0107 0.0107 0.0020 0.0000	2	900199		iñ i						0.0135	0.0135	2.984	0.0126	0.0135	0.000	<b>3</b>
900202 103 2000 2594 62 0.0158 0.0153 2.997 0.0152 0.0014	2	900200	_	ñ						0.0134	0.0133	3.016	0.0131	0.01%	0.0003	9.0
900203 107 20 2980 2974 62 0.0135 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0153 0.0015 9.5 900203 99 5 13 300 2997 62 0.0125 0.0140 0.0140 2.0175 0.0140 0.0140 0.0154 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0015 0.0140 0.0134 0.0015 0.0140 0.0134 0.0015 0.0140 0.0134 0.0015 0.0140 0.0134 0.0015 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0014 0.0144 0.0144 0.0144 0.0144 0.0014		900201		ñ						0.0132	0.0132	2.997	0.0128	0.0132	0.0004	2.2
95         13         3030         2991         61         0.0125         0.0140         3.011         0.0125         0.0140         3.011         0.0126         0.0134         0.0121         0.0121         0.0124         0.0127         0.0137         0.0127         0.0127         0.0127         0.0127         0.0127         0.0127         0.0127         0.0127         0.0127         0.0127         0.0127         0.0127         0.0127         0.0127         0		900202		N						0.0153	0.0153	2.977	0.0135	0.0153	0.0018	0.0
900204 130 47 3000 2988 62 0.0123 0.0154 0.0154 0.0124 0.0134 0.0134 0.0134 1.6 90021 1.6 900204 130 47 3000 2988 62 0.0124 0.0155 0.0155 0.0152 0.0152 0.0152 0.0154 1.6 900205 1142 34 3009 62 0.0135 0.0155 0.0155 0.0152 0.0153 0.0152 0.0152 0.0154 1.6 900206 174 15 2968 2983 63 0.0156 0.0156 0.0157 0.		900203		-						0.0140	0.0140	3.011	0.0125	0.0140	0.0015	N 1
900204 130 47 3000 2988 62 0.0133 0.0152 0.0154 2.994 0.0151 0.0154 0.0155 0.0157 0.0157 0.0157 0.0157 0.0157 0.0157 0.0157 0.0157 0.0157 0.0157 0.0157 0.0157 0.0157 0.0155 0.01				in :						0.0134	0.0134	3.009	0.0120	0.0134	0.0014	ç.
900205 142 34 3009 500 0.0153 0.0155 0.0155 5.007 0.0153 1.0152 0.0155 1.0152 1.0152 0.0155 1.0152 0.0000 0		900204		41						0.0125	0.0124	25.7	1210.0	42.0.0	0.0003	0.0
900207 174 15 2965 2983 65 0.01120 0.0137 0.		20202		4						0.0155	20.00	2000	0.0155	20.00	A100-0	2.0
900207 76 10 3000 3046 02 0.0117 0.0115 0.0137 0.0117 0.0117 0.01137 0.0020 0.0000 0.0		900500		-						0.0148	0.0149	2.970	07.0.0	0.0143	0.0020	7
900208 78 10 3015 3110 65 0.0127 0.0137 0.0137 5.065 0.0127 0.0138 0.0000 <		900207		-						0.0137	0.0137	3.027	20.0	0.0137	0700.0	
900184 106 49 2983 2925 62 0.0124 0.0125 0.0124 0.0125 0.0125 0.0125 0.0125 0.0125 0.0125 0.0125 0.0125 0.0125 0.0125 0.0125 0.0127 0.0127 0.0127 0.0127 0.0127 0.0127 0.0127 0.0127 0.0127 0.0127 0.0127 0.0127 0.0127 0.0127 0.0127 0.0127 0.0127 0.0127 0.0128 0.0000 0.0				-						0.0137	0.0137	3.063	0.0127	0.0157	0.00.0	
900183 182 52 3036 3012 62 0.0127 0.0127 0.0127 0.0127 0.0127 0.0127 0.0127 0.0127 0.0127 0.0127 0.0127 0.0127 0.0127 0.0127 0.0129 0.0000 < MOL 900177 196 39 2994 61 0.0129 0.0129 0.0129 0.0129 0.0129 0.0000 < MOL 900178 72 1 2968 2934 62 0.0125 0.0126 0.0126 0.0126 0.0126 0.0129 0.0129 0.0000 < MOL 900179 72 1 2968 2934 62 0.0125 0.0120 0.0120 0.0120 0.0120 0.0120 0.0120 0.0000 < MOL 900189 111 6 3018 3009 62 0.0134 0.0133 0.012 0.0134 0.0133 0.0000 < MOL 900181 147 16 2977 3000 62 0.0134 0.0132 0.0123 0.0000 0 0.0000 0	w		•	4						0.0123	0.0123	5.954	0.0125	0.0123	0000	
900177 196 39 2985 2994 61 0.0129 0.0130 0.0129 2.990 0.0129 0.0129 0.0129 0.0100 < MDL 900177 196 39 2985 3042 61 0.0125 0.0124 0.0124 3.014 0.0124 0.0124 0.0124 0.0124 0.0124 0.0124 0.0124 0.0124 0.0124 0.0124 0.0124 0.0124 0.0124 0.0124 0.0133 0.0000 < MDL 900179 72 1 2968 2934 62 0.0130 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0134 0.0133 0.0000 < MDL 900181 147 16 2977 3000 62 0.0124 0.0134 0.0124 0.0124 0.0124 0.0123 0.0000 < MDL 900182 158 32 2994 2977 61 0.0122 0.0122 0.0122 0.0121 2.986 0.0122 0.0121 0.0000 0.0000 no sample	under			'n						0.0127	0.0127	3.024	0.0127	0.0127	0.000	
900178 161 36 2985 3042 61 0.0125 0.0124 0.0124 3.014 0.0124 0.0124 0.0124 0.0127 0.0000 < MOL 900179 72 1 2968 2934 62 0.0120 0.0120 0.0120 2.0120 2.0120 0.0000 c MOL 900182 158 32 2994 2977 61 0.0122 0.0122 0.0122 0.0121 0.0000 0.0		900177		m						0.0130	0.0129	2.99	0.0129	0.0129	0000	
900179 72 1 2968 2934 62 0.0120 0.0120 0.0120 0.0120 0.0120 0.0120 0.0120 0.0120 0.0120 0.0120 0.0000 < MDL 900180 111 6 3018 3009 62 0.0134 0.0134 0.0134 0.0133 3.014 0.0134 0.0134 0.0133 0.0000 < MDL 900181 147 16 2977 3000 62 0.0124 0.0124 0.0124 0.0123 2.989 0.0124 0.0133 0.0000 < MDL 900182 158 32 2994 2977 61 0.0122 0.0122 0.0121 0.0000 0.0000 0.0000 0.0000 0.0000 no semple		900178		M						0,0124	0.0124	3.014	0.0124	0.0124	0.000	_
900160 111 6 3018 3009 62 0.0134 0.0133 0.0134 0.0133 3.014 0.0134 0.0133 0.0000 < MDL 900160 111 6 2977 3000 62 0.0124 0.0124 0.0123 2.986 0.0124 0.0123 0.0000 < MDL 900162 158 32 2994 2977 61 0.0122 0.0122 0.0121 0.00000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.		900179								0.0120	0.0120	2.951	0.0120	0.0120	0.000	- E
900181 147 16 2977 3000 62 0.0124 0.0124 0.0123 2.989 0.0124 0.0123 0.0000 < MDL 900182 158 32 2994 2977 61 0.0122 0.0122 0.0121 2.986 0.0122 0.0121 0.0000 < MDL 900182 158 32 2994 2977 61 0.0122 0.0122 0.0121 2.986 0.0120 0.0000 0.0000 0.0000 c.mpl		900180		_						0.0134	0.0133	3.014	0.0134	0.0133	0.0000	<u>.</u>
900182 158 32 2994 2977 61 0.0122 0.0122 0.0121 2.986 0.0122 0.0121 0.0000 < MDL 0.000 0.0000		900181		<u>~</u>				ö		0.0124	0.0123	5.989	0.0124	0.0123	0,000	, <u>1</u> 0,
0.000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000				m				o'		0.0122	0.0121	2.986	0.0122	0.0121		•
0.0000 0.0000 0.0000 no sample	<b>BLANK?</b>											0.000	0.000	0000		Ome s
	EXMAUST											0.000	0.000	0000		die

TRAVIS AFB
PAINT BOOTH TESTS
ACUREX PROJECT 8485

D E INITIALS: BN & LJL Q A INITIALS: LJL

TE #1		1 < MOL
TEST: SINGLE PASS PARTICULATE #1 DATE: 07-01-92 AM2 METHOD: NIOSH 500	GRID CHART - PARTICULATE	Painter Over < MOL Painter Under < MOL

3 < MOL 4 MOL 7 0.5 8 0.5 11 3.2 1.1 4 MOL 23 4.9 24 1.6 15 8.2 1.6 16 1.6 19 10.7 20 5.2	0 0 0 0 0 0 0
4 MDL 4 MDL 4 MDL 3 4.9 5 8.2 7.5 10.7	
^ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	
<sup>™</sup> ,	
	1
< #DL 0.5 0.5 3.3 1.6 4.8 11.7	
2	
< PDL   1.6   1.6   1.6   7   10.2   7   10.2   10.	
- s 2 2 5 7:	1

PAINTER MOL: 0.1 mg/SAMPLE

RECIRC DUCT: no sample

TEST:		S.P. PARTICULATE #2		TRAVIS AFB	NFB		PAINT:	GRAY TOPCOAT	CAT TABLE		DE	INITIALS:	171 % RS		
METHOD:				ACUREX	CUREX PROJECT 8485	:82		Y Y	S & IABLE		ς .		1		
GRID LOC	ACUREX	# FILTER #	PUMP *	PRE-CAL (ml/min)	POST-CAL (ml/min)	RUN TIME (min)	PRE #1	PRE #2 (9)	POST #1 (9)	POST #2 (9)	AVG FLOW	PRE AVG POST AVG	POST AVG	PART WT (g)	PARTICULA (mg/H3)
1	1 900209	249	55	3012	1	19	0.0119	:	0.0120	0.0120	2.993	0.0120	0.0120	0.000	JOH V
	2 900215	216	15	2983		8	0.0128	0.0128	0.0127	0.0127	3.008	0.0128	0.0127	0.000	
2 DUP	_		2	3060		8	0.0119		0.0119	0.0119	3.076	0.0119	0.0119	0.000	OH V
	Ī	255	50	3003		89	0.0121		0.0124	0.0124	3.002	0.0122	0.0124	0.0002	1.0
	4 900218		8	2994		89	0.0121	0.0122	0.0125	0.0124	3,033	0.0121	0.0125	0.0004	1.9
	5 900219		=	3033		89	0.0127		0.0131	0.0131	3.081	0.0129	0.0131	0.0002	1.0
•	6 900220		-	3036		8	0.0124		0.0125	0.0125	3.007	0.0124	0.0125	0.0001	0.5
	7 900221		43	2980		88	0,0129		0.0131	0.0131	2.983	0.0129	0.0131	0.0002	1.0
	8 900228		28	2968		8	0.0120		0.0122	0.0122	2.958	0.0120	0.0122	0.0002	1.0
	9 900223		53	3030		89	0.0134		0.0137	0.0137	3.039	0.0134	0.0137	0.0003	1.5
F	0 900224		2	3060		83	0.0129		0.0137	0.0136	3.068	0.0129	0.0137	0.0008	ю. М
-	1 900225		&	2004		8	0.0133	0.0134	0.0144	0.0144	2.945	0.0134	0.0144	0.0010	5.0
-	2 900226		2	2994		88	0.0132		0.0138	0.0139	2.964	0.0132	0.0138	0.0006	3.0
12 PUP			S	2008		8	0.0121		0.0128	0.0128	3.013	0.0122	0.0128	9000.0	5.9
21	_		33	2983		19	0.0125	0.0129	0.0132	0.0131	5.989	0.0127	0.0131	0.0004	2.0
	_		7	2971		8	0.0122		0.0131	0.0131	2.968	0.0121	0.0131	0.0010	0.
22 PUP			5	3018		69	0.0117		0.0124	0.0125	3.011	0.0117	0.0124	0.0007	Y.
X;			<b>*</b>	3000		8	0.0119	0.0119	0.0133	0.0132	% 7	0.0119	0.0133	0.0014	0
77			24	3030		3	0.0132		0.0139	0.0139	3.026	0.0152	0.0139	2000.0	4.
-	5 900255		3,	3		8	0.0151		20.00	0.0135	200	0.0151	20.0	0.0003	Ç.,
~ •	4 Y00234	522	0 5	2000	3018	8 4	0.0124		0.0150	20.0	5.014		277	250	
7,			ž	2085		8 %	0.0127	0.0126	1750	2710	2 072	200	7710	2000	
14 25			3.2	202		38	0.0123		0.0131	0.0131	2,00	0.0124	0.0131	0.0007	M
	Ť		12	3015		19	0.0129		0.0138	0.0137	2.995	0.0128	0.0137	0.0009	4.5
	8 900239	542	2	3000		19	0.0123	0.0124	0.0140	0.0139	3.027	0.0123	0.0140	0.0017	8.4
<u></u>	9 900240		45	3033		3	0.0120		0.0135	0.0134	3.030	0.0120	0.0135	0.0015	7.3
N	0 900241		8	3042		8	0.0127		0.0136	0.0136	3.042	0.0128	0.0136	0.0008	0°
P over	•		25	3012		8	0.0131	0.0133	0.0153	0.0154	3.029	0.0132	0.0153	0.0021	10.2
P under			64	2974		19	0.0123		0.0129	0.0129	2.977	0.0123	0.0129	0.000	3.0
<del>-</del>			3	2941		67	0.0113	0.0115	0.0115	0.0114	2.929	0.0114	0.0114	0000	<u>ē</u>
~	2A 900244		35	2977		29	0.0126		0.0126	0.0125	2.945	0.0126	0.0125	0.000	<u>.</u>
M)			2	2977		29	0.0128		0.0127	0.0127	2.968	0.0128	0.0127	0.000	- -
	B 90024		2	1662		8	0.0123		0.0124	0.0123	5.012	0.0124	0.0125	0000	
Ni	B 900247		2:	3048		8	0.0119	0.0118	0.0118	7110.0	986	9110.0	0.013		2 i
			2	3006		8	0.0117		7110.0	0.01	200	7110.0	7.LL.0		
F BLANK?	- 1														
PFILEC	= -										800	888	0000	0000	eldmos on

MLET CRID Field Blank EXHAUST DUCT:no sample RECIRC DUCT:no sample D E INITIALS: BN & LJL Q A INITIALS: LJL 유 · 2 2 2 3 10E > 3.9 1.0 3.0 1.9 3.4 GRID MOL: 0.1 mg/SAMPLE PAINTER HOL: 0.1 mg/SAMPLE 42 9 ನ 2 5.0 7.9 7.3 6.9 1.0 1.0 EXHAUST GRID \$ \$ = ສ TRAVIS AFB
PAINT BOOTH TESTS
ACUREX PROJECT 8485 OSHA TWA: 77 mg/MS 0.5 3.8 . w. o 6.3 8.4 UNITS: Mg/HS <u>ğ</u>ğ **e** \* 2 22 2.0 1.5 1.0 1.5 10H > 4 5 21 CBJECT: BOX, PIPES & TABLE PAINT TYPE: GRAY TOPCOAT TEST: S.P. PARTICULATE #2 DATE: 07-01-92 PM METHOD: NIOSN 500 GRID CHART - PARTICULATE . . . . . . . . . . . . . . . Painter Over 10.2 Painter Under 3.0 . . . . . . . . . . . . . . . INLET GRID A 24 MDL 10. % th MPL

TEST: DATE: METHOD:	METALS #1 06-22-92 PM NIOSH 7300	#1 2 PM 300		TRAVIS PAINT B	TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485	35	PAINT: OBJECT:	LT GREEN PRIMER COMFORT PALLET	PRIMER ALLET		D E	INITIALS: INITIALS:	רזו		
GRID LOC	ACUREX	BASE # SAMPLE #	# PUMP #	PRE-CAL (ml/min)	POST-CAL (ml/min)	RUN TIME (min)	(ng)	ZINC (gu)	STRONT IUM (ug)	CHROMIUM AVG FLOW (ug) (L/MIN)	AVG FLOW (L/MIN)	LEAD (ug/M3)	21NC (ug/H3)	STRONTIUM (ug/H3)	CHROMIUM (ug/M3)
	Į,		7	t t t	5 3039	> 27	0.075	0.80	0.80	0.57	3.042	iQ# Y	5.6	5.6	7.0
7	<b>—</b>		M.	50		> 97	0.075	1.06	1.72	1.22	2.990	· MDL	7.7	12.5	8.9
ν,	•					> 25	0.075	1.46	7.47	4.52	3.039	10E	10.2	52.3	31.6
<b>\$</b> 11	<i>u</i> c	0 EX921070	3 F			> 07	20.0	24.0	15.88	50.0	2.987			9.41	-65
<b>n «</b>	4 6	26 EX921072	J &-		5 2151	V 97	20.0	5.5	75.37	0C*  77 k	7.77	) ()	1 c	2.71	7°50 7°50
^	,		- 14*			7 97	, c	122	3.4	90	8.0		0	117.0	200
- 60	-	EX921	,			7 97	0.07	09 0	26.92	14.68	2.078			181	107.2
0	. 2	21 EX921075				> 1.4	0.075	1.06	5.78	3.54	2.984	- V	7.6	41.2	25.2
10					(7)	> 25	0.075	0.48	24.34	14.37	3.024	JOH >	3.4	171.3	101.1
Ξ	2	25 EX921077		14 298		> 25	0.075	0.86	31.50	18.80	2.946	<b>10H</b> >	6.2	227.5	135.8
-			•	3066		> 25	0.07	0.50	< 0.30 ×	0.30	3.048	로 당 マ	3.5	를 (	ਹੂ ਵ •
15 UC		10 EX921091	7		3000	¥ 04 7	0.070	50.0	27.27	33.82	5.003		4 0	20 m	2.447
22	• -					× 14		\$ K	26.12	15.81	3.008	<u> </u>	0 10	7.78	11.8
12	. ~	_	- 147			> 97	0.075	0.62	59.14	36.16	3.021	101	4.5	425.6	260.2
54	-	11 EX921090	rv.	24 306	3158		0.24	3.08	72.09	42.58	3.112	1.6	21.1	492.9	291.1
£.			PT)				0.14	2.25	12.58	7.44	3.065	1.0	16.0	89.2	52.8
1 1 1	<b>V</b>	4 EX921080	7			× × × × × × × × × × × × × × × × × × ×	0.0 C K	0.00	40.12 44 55	24.22	2.703	Ž \$	٠.٠ د.٧	282.1	1/0.5
15 DUP		17 EX921092				7	0.075	0.41	30.64	18.41	3.029		5.0	219.9	132.2
						> 97	0.075	77.0	70.80	42.48	3.006	JOH V	3.2	512.0	307.2
17	~					> 94	0.073	0.56	3.52	3.36	3.035	₩ •	0.4	25.2	24.1
<b>∞</b> (		3 EX921084				4	0.075	0.51	16.68	10.23	3.026	ر اور ا	9.	117.3	6.5
2.5					1027	9 4	4 5	15.0	44.20	84 07	301.5	). 	90	1026.1	780.0
9		4 FX921127				,	0.075	6	51.22	30.21	2.080		4.4	382.0	225
						455 4	0.075	0.46	6.78	4.26	2.981	101	3.4	50.5	31.8
14	_	_	N			> 97	0.075	0.42	< 0.30	1.18	3.017	Y FOL	3.0	V ₩DF	8.5
<b>X</b> i	m)				3009	> 57	0.075	0.62	< 0.30 ×	0.30	3.006	JOE V	9.4	JOH V	JOH V
¥S.			~ (				0.075	84.0	× 0.30 ×	0.30	3.003	<u>.</u>	0.1	ا ا	10H V
9 00		S EXYZION	4-			V 94	250	0.40	0.30	1 84	1 180		6.7	<u> </u>	12C
3.5	4							77	0.55	2	000		, C	)   	2
P over *	212	2 EX921279				38 4	0.075	0.58	60.14	35.28	3.006	V MOL	5.1	526.5	308.9
							0.075	0.58	14.52	8.60	2.973	< 100 ×	5.1	128.5	
BLANK											000.0	no semplem	no sample	no sampleno	o semple
LOCATION		ACETONE	MITRIC	FILTER	IMPINGER	CCU FT)	(GO)	Cug)	(Ug)	(ug) (M3)	(M3)	(ug/NG)	Z1MC (ug/M3)	(ug/M3) (ug/M3)	CHROMIUM (Ug/M3)
EXHAUST		EX921376 EX921380	EX921377 EX921381	20	8 EX921379 4 EX921395	38.80 48.98	2.5	32.05 133	15.85 15.4	25.4	1.098	^ MDL 1.8	%.5 %.0	14.4	23.1 63.1
				EXHAUS	T ACETONE	EX921376 <	2.5	1.85	7.3	4.50	1.098	<u> </u>	1.7	9.9	4.1
						EX921378 <	2.5	4 1.25	0.85	1.70	1.098		) FOI V	0.8	2.5

TEST: METALS #1 DATE: 06-22-92 PM METHOD: NIOSH 7300	TRAVIS AF PAINT BOO ACUREX PR	S AFB BOOTH TESTS X PROJECT 8485	PAINT: OBJECT:	PAINT: LT GREEN PRIMER OBJECT: COMFORT PALLET	RIMER		D E IN	D E INITIALS: LJL Q A INITIALS:	רו		
ACUREX BASE PUMP # (ml/min) (ml/min) (min)	PRE-CAL (ml/min)	POST-CAL RUN TIME (ml/min)	(ng)	21NC (ug)	NC STRONTIUM CHROMIUM AVG FLOW LEAD A9) (ug) (LU) (L/MIN) (ug/M3)	CHROMIUM (Ug)	AVG FLOW (L/MIN)	LEAD (ug/M3)	ZINC (ug/H3)	ZINC STRONTIUM CHROHIUM	CHROMIUM (ug/M3)
2	: : : : : :	IMPINGER EX921379 < 0.5	< 0.5	52	c 0.2	12.00	1.098	<b>₩</b> >	22.8	√ MDL	10.9
	RECIRC	ACETONE EX921380 MITDIC EX921381	2.5		15 5.3	5.40	1.386	로 로 * *	10.8	8.8 6.4	3.9 18.8
		FILTER EX921394 2.5	2.5		1.6		1.386	- <u>ē</u>	13.0	1.2 * FDL	31.7

D E INITIALS: LJL Q A INITIALS: 0	1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	10H > 10H >	S NOL	12	\$ 24 1.6 28 < PDL	4 MOL: 4 MOL 4 MOL 518	1,0 20 0.7
TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485	EXHAUST GRID	2 < MDL 3	6 + MDL	10 11 ×	22 23 C3 C3 <	51 51 > HOL 51	18 < #DL
TEST: METALS #1 DATE: 06-22-92 PM THOD: NIOSH 7300 D CHART 1 - LEAD	\$ C C C C C C C C C C C C C C C C C C C	Painter Over 1	INLET GRID A 5 < MOL	) + HDL	21 + MDL	0.1	17 × mol.

INLET GRID B 8.0 3.2 29.5 3.5 4.5 ä 8 88 EXHAUST DUCT: RECIRC DUCT: 0 D E INITIALS: LJL Q A INITIALS: 5.9 5.0 21.1 3.5 3.1 PAINTER MOL: 0.3 UB/SAMPLE GRID MOL: 0.3 UG/SAMPLE 8 12 2 54 8 3.6 4.1 10.2 9.4 6.2 4.5 **EXHAUST GRID** 4 ສ 5 Ξ PAINT BOOTH TESTS ACUREX PROJECT 8485 3.6 5.0 3.4 5.3 3.5 7.7 **\$** OSHA TWA: 1000 Ug/H3 9 14 22 UNITS: Ug/H3 16.0 4.0 7.6 8.8 5.6 3.3 17 7 21 PAINT TYPE: LT GREEN PRIMER OBJECT: COMFORT PALLET Painter Over 5.16 5.1 2nd Painter Under 5.1 2nd TEST: METALS #1 DATE: 06-22-92 PM METHOD: NIOSH 7300 INLET GRID A GRID CHART 2 - ZINC 3.0 9.4 3.6 న Ş **≤** 

FRHAUST GRID  1 5.6 2 12.5 3 52.3 4 115.6  For a control of the co	THOD: NIOSH 7300  CHART 3 - STRONTIUM		ACUREX PROJECT 8485	CT 8485		
For the first state of the first		; ; ; ; ; ; ; ;	EXH	AUST GRID	10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
21 55.2 6 42.3 7 117.0 8 181.9 9 41.2 10 171.3 11 227.5 416.8 21 55.2 22 184.8 23 425.6 492.9 15 69.2 14 282.1 15 242.6 15 512.0	Painter Over 382.0 526.5 2nd Painter Under 50.5 128.5 2nd	5.6				
21 55.2 22 4.25.6 492.9  13 69.2 14 82.1 15 22.6 492.9  17 25.2 184.8 282.1 15 242.6 512.0  31 277.7 20 20 24.1	INLET GRID A					INLET GRID B
55.2 22 46.6 245.6 24 492.9 28  55.2 184.8 245.6 492.9 28  14 282.1 15 242.6 512.0 38  25.2 18 17.3 19 577.7 20 1024.1	104 >		10 171.3	11 227.5	12 < MDL 416.8	<b>Q</b>
15 69.2 14 15 242.6 16 512.0 219.9 17.3 117.3 117.3 1024.1	7		184.8	23 425.6	492.9	- S8 - MOL
25.2 18 17.3 577.7	۲		14 282.1	15 242.6 219.9	16 512.0	e M
			18 117.3	19 577.7	20 1024.1	· · · · · · · · · · · · · · · · · · ·

INLET GRID B 13.0 2.8 23.1 63.1 로 \* \* æ 8 EXHAUST DUCT: RECIRC DUCT: 0 D E INITIALS: LJL Q A INITIALS: 16 307.2 20 589.1 291.1 107.2 70.1 244.8 12 < MOL PAINTER MOL: 0.3 UB/SAMPLE GRID MOL: 0.3 Ug/SAMPLE **©** 142.9 345.8 31.6 69.0 135.8 260.2 EXHAUST GRID 6 = 2 3 TRAVIS AFB
PAINT BOOTH TESTS
ACUREX PROJECT 8485 14 170.3 101.1 111.8 71.9 8.9 25.4 18 22 OSHA TUA: 50 UG/H3 UNITS: Ug/M3 52.8 24.1 10.9 25.2 34.4 4.0 17 2 21 PAINT TYPE: LT GREEN PRIMER OBJECT: COMFORT PALLET GRID CHART 4 - CHROMIUM Painter Over 225.3 308.9 2nd Painter Under 31.8 76.1 2nd INLET GRID A TEST: METALS #1 DATE: 06-22-92 PM METHOD: NIOSH 7300 8.5 24 \* HDL 34 A HOL \$

						,									
٥	ACUREX SAMPLE	BASE # SAMPLE	* PUMP *	PRE-CAL (ml/min)	POST-CAL RUN TIME (ml/min) (min)	RUN TIME (min)	LEAD (ug)	ZINC (ng)	STRONTIUM (ug)	CHROMIUM (ug)	AVG FLOW (L/MIN)	LEAD (ug/M3)	ZINC (ug/M3)	STRONTIUM (ug/M3)	CHROM1UM (ug/M3)
	-		t5 64	3006		83	0.075	0.34	0.72	0.57	3.030	<u>2</u>	1.7	3.6	2.9
Z DUP		79 EX921099		3066	3129	3.3	0.075	0.45	1.58	1.05	3.098	1 <u>2</u>	2.3	.0	5.1
M.				3018		99	0.075	0.48	10.23	77.9	3.050	JOH Y	2.4	50.8	32.0
<b>4</b> 0		EX921		3003		8:	0.07	0.88	27.44	17.02	2.992	- F	2.5	139.0	86.2
^ <		EX921		2036		V 69	C 0.0	90.0	20.0	7.10	3.014	<u> </u>	ν, ς 20 π	4.0	0.0
~		50 EX921104		3036	3015	8 %	0.077	2,20	38.86	23.37	3.0.5	70	10.6	104.6	117.0
· 80		EX9211		3045		8	0.077	0.98	21.02	12.75	3.067	7.0	4	103.9	63.0
0	_	EX9211		3042		8:	0.075	0.63	44.90	25.78	3.021	JOH >	2.5	225.2	129.3
2:		34 EX921107	200	3006		84	0.0 0.0 0.0	0.71	87.57	51.41	2.88	₹ •	9.4	442.9	260.0
12	•			3063		8 %	0.07	9.0	82.74	48.74	3.053	<u> </u>	) +	4.10.7	241.0
21		EX921		3030		8	0.075	0.81	30.76	17.88	3.061	Ğ.	4.0	152.3	88.5
25		EX9211		3039		29	0.07	0.7	8.6	59.48	m .	7.0	χ.,	482.3	289.8
3 2 2		5 FX921113		2000		8		**	158.90	27.701	3.038		0 O	2 <del>2</del> 2	4.77
•		EX9211		3069		38	0.075	0.51	91.50	55.22	3.056	101	2.5	453.7	273.8
13				3072		<b>%</b> :	0.075	99.0	33.16	19.91	3.054	10H >	M.	2.5	8.8
14 Pulo		1 EX921116 0 Ex021117		3035		83	٠. د د	0.68 4.68	80.82 91.82	5.5 5.5 8.6 8.6	3.018	<u> </u>	4.5	7.504	25/1./ 25/8 /R
5		EX9211		3072		, 38	200	0.74	111.80	88	3, 101	0.4	, v	546.3	313.0
16				3063		8:	0.075	0.88	122.56	68.46	3.048	JOH V	4.4	609.2	340.3
- 4	Ī	4 EX921120		1202		83	0.0 درد	0.58	8.72	5.07	5.017	<u> </u>	4.5	45.8	5.55
2				3075		3 %	0.07	7.53	101.06	56.86	3.054		37.4	501.4	282.1
		EX921		3036		8	0.085	0.63	91.47	50.81	3.130	9.0	3.0	442.8	246.0
•		32 EX921124		3015		65	0.11	1.77	206.86	118.34	2.979	9.0	9.1	1068.5	611.3
i i	7	35 EX921125	2 6	2000	Ċ	0 4 0 4	5 c	0.00	8.10	4.0	2.039	ž §	0.5		*
24				3060		3.50	0.075	0.8	0.30 <	0.30	3.057	, <u>1</u>			9
				3000		<b>65</b> <	0.075	0.42	0.30 <	0.30	2.993	JOH Y	2.2	V ₩DF	<u>1</u> 04 ×
SA DUP		49 EX921096		2985		) L	0.0 K	92	0.30 <	0.30	2.977	ਰ ਵ • •	120.9		ğ ;
28			28	3024	2962	3.50	0.07	0.41	0.36	0.32	2.93	1 d	2.1	1.9	1.6
88		3 EX921130		3036		\$ 50	0.075	0.32	0.33 7	0.28	3.010	달 *	9.	7.1	<u> </u>
LLD BLANK						8	0.00	0000	0000	0.30	3.5	•	0	2	?
LOCATION		SAMPLES	MITRIC	FILTER	IMPINGER	SAMPLE (CU FT)	LEAD (ug)	ZINC (ug)	STRONTIUM (ug)	CHROMIUM (ug)	SAMPLE (H3)	LEAD (ug/H3)	ZINC (ug/M3)	STRONT IUM (ug/M3)	CHROMIUM (ug/M3)
EXMAUST RECIRC		EX921382 EX921386	EX921383 EX921387	EX921384 EX921416	EX921385 EX921417	39.20 40.84	00	85.6 53.9	13.13 10.75	30.08	1.109	* * *	77.2	11.8 9.3	27.1
				EXHAUST	LLI.	EX921382 < EX921383 <	2.5	5.6	%. %. %.	5.4	1.109	<u> </u>	5.0	7.6	4.70
					FILTER	EX921384 < EX921385 <	2.5 0.5 5	7.7 2.8	0.93 < 0.2	1.28	 81:-	로 로 로 로	10H > 59.5	<b>0</b> 0	15.3

(ug) (ug) (L/MIN) (ug/M3) (ug/	TEST: METALS #2 DATE: 06-24-92 PM METHOD: NIOSH 7300 ACUREX BASE	TRAVIS A PAINT BO ACUREX P	S AFB BOOTH TESTS X PROJECT 8485 AL POST-CAL RU	N TIME	PAINT: OBJECT: LEAD	PAINT: LT GREEN PRIMER OBJECT: SPLITTERS LEAD ZINC STRON!	PRIMER	CHROMIUM	D E IN Q A IN AVG FLOW	D E INITIALS: Q A INITIALS: S FLOW LEAD	ZINC		DITIO
CC ACETONE EX921386 < 2.5 10.9 4.2 4.9 1.156 < MOL NITRIC EX921387 < 0.5 20 5.7 18.00 1.156 < MOL FILTER EX921416 < 2.5 < 1.25 0.85 1.7 1.156 < MOL	GRID LOC SAMPLE # SAMPLE # PUMP #	(ml/min)	(ml/min)	(min)	(£a)	(Bn)	(bn)	(fn)	(L/MIN)	(ug/M3)	M/Bn)	a i	() (ug/M3) (ug/M3)
NITRIC EX921387 < 0.5 20 5.7 18.00 1.156 < MOL FILTER EX921416 < 2.5 < 1.25 0.85 1.7 1.156 < MOL		RECIRC	ACETONE E	×921386 ×	2.5			6.4	1.156	) MOL >	7.6		3.6
3X921416 < 2.5 < 1.25 0.85 1.7 1.156 < HOL			MITRIC E	K921387 <	0.5			18.00	1,156	, <u>10</u>	17.3		o. •
			FILTER	x921416 <	2.5			1.7	1.156	\d¥ ×	<b>₩</b>		0.7

00		FIELD BLANK  < 0.4	INLET GRID	18 A FOL	28 < MOL	38 490.		EXHAUST DUCT: < NOL
D E INITIALS: Q A INITIALS:	1	10H > 7	8.0	12 < HDL	24 < MOL	16	20 0.4	
ESTS T 8485		3 < MOL	7 0.4	# * *	33 < #DL < #DL	15 0.4	19 ×	GRID MOL: 0.075 Ug/SAMPLE
PAINT BOOTH TESTS ACUREX PROJECT 8485	EXHAUST GRID	2 < MOL < MOL < MOL	704 >	10 < FDL	22 0.4	24 108 >	18 < MOL	Ug/H3
	0 0 0 0 0 0 0 0	1 < MDL	5 < MDL	9 < MDL	21 < MOL	13 < MOL	17 < MDL	R UNITS: Ug/H3
DATE: 06-24-92 PM THOD: NIOSH 7300 D CHART 1 - LEAD		inter Over 0.6 inter Unde < MDL	INLET GRID A	1A < MOL	2A < MDL	<u>ទី</u> គ `	** < MOL 1MIN	PAINT TYPE: LT GREEN PRIMER

00		FIELD BLANK 1.8	INLET GRID B	1.7	28 2.1	M 1.6		EXHAUST DUCT: 77.2 RECIRC DUCT: 46.6
D E INITIALS: Q A INITIALS:		4 4.5	80 80°	12 3.1	24 2.5	16 4.4	20 3.0	!
TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485	EXHAUST GRID	3 2.4	7 10.6	11 . 5.3	£2. 3.9	15 3.6	19 37.4	GRID MOL: 0.3 UG/SAMPLE PAINTER MOL: 0.3 UG/SAMPLE
TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 848		2 2.5 2.3	6 2.5	10 3.6	22 3.5	14 3.4 15.6	18 7.2	UNITS: UB/M3 OSHA TWA: 1000 Ug/M3
	-	1 1.7	5 2.8	9 3.2	21 4.0	13 3.3	17 2.9	
TEST: METALS #2 DATE: 06-24-92 PM METHOD: NIOSH 7300	GRID CHART 2 - ZINC	Painter Over 9.1 Painter Under 2.0	INLET GRID A	1A 1.9	24 4.1	¥.	** 120.9 1MIN	PAINT TYPE: LT GREEN F OBJECT: SPLITTERS

D E INITIALS: 0 O A INITIALS: 0		4 139.0 FIELD BLANK	B 103.9	18 < MOL 12 410.7	24 453.7 28 1.9	16 609.2 38 1.7	20 442.8	ug/SAMPLE EXHAUST DUCT: 11.8
TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485	EXHAUST GRID	3 50.8 8.0	.6 7 194.6	.9.727	23 846.0 795.1	15 546.3 .5	19 501.4	GRID MOL: 0.3 ug/SAMPLE
TRAVIS AFB PAINT BOOT ACUREX PRO		3.6	9.67 6 49.6	10 442.9	152.3 22 482.3	14 405.7 453.5 453.5	18 43.8 374.0	UNITS: Ug/H3
TEST: METALS #2 DATE: 06-24-92 PM METHOD: NIOSH 7300 GRID CHART 3 - STRONTIUM		Painter Over 1 1068.5 Painter Under 41.3	ET GRID A 5	1A < HDL 9 225	2A 152 152	13 164.5 3A + HDL + HDL	11	PAINT TYPE: LT GREEN PRIMER UNITS:

ALS: 0	FIELD BLANK	INLET GRID B	ige •	28	38 A MOL		EXHAUST DUCT: 27.1 RECIRC DUCT: 35.1
D E INITIALS: Q A INITIALS:	4 86.2	8 63.0	12 241.9	24 273.8	16 340.3	20 246.0	ug/SAMPLE ug/SAMPLE
8485	3 32.0	7 117.0	11 431.3	23 501.4 473.2	313.0	19 282.1	GRID MDL: 0.3 UG/SAMPLE PAINTER MDL: 0.3 UG/SAMPLE
TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485	2 4.2 5.3	6 30.3	10 260.0	22 289.8	14 227.7 258.8	18 210.1	ug/H3 50 ua/H3
	2.9	5.6	9 129.3	21 88.5	13 98.8	17 25.5	UNITS:
TEST: METALS #2 DATE: 06-24-92 PM METHOD: NIOSH 7300 GRID CHART 4 - CHROMIUM	Painter Over 611.3 Painter Under 24.4	GRID A	10e *	2x < FDL	Ş X	MINI JOHN **	PAINT TYPE: LT GREEN PRIMER CALECT: SPITTERS

Color   Colo	TEST: MI DATE: ON METHODE N	METALS #3 06-25-92 AM1 NIOSH 7300	3 AM1 30		TRAVIS AF PAINT BOO ACUREX PR	FB OTH TESTS ROJECT 8485	×	PAINT: OBJECT:	LT GREEN PRIMER BRAKE PARTS, HU	LT GREEN PRIMER BRAKE PARTS, HUBS, RAMP	AMP	0 E A IX	INITIALS: INITIALS:	ភ		
12   12   12   13   13   13   13   13	AN GRID LOC S	CUREX	BASE SAMPLE		PRE-CAL (ml/min)		RUN TIME (min)	LEAD (ug)	ZINC (ug)	STRONTIUM (ug)	CHROMIUM (Ug)	AVG FLOW (L/MIN)	LEAD (ug/M3)	ZINC (Ug/M3)	STRONT IUM (ug/M3)	
Figure   F		5		25			85	1 610	8	1 63	4.70	2 0.75	¥ 0	27.1	0	7.7
Fig. 8602121   23   2997   3010   55   2700   2578   2.56   1.04   5022   124   1524	. ~	3 2		) =			200	0,50	25.5			2 000	, r		7.7	3
112   ENCRITICA   22   2977   3100   51   3.770   4.13   2.46   2.46   2.74   2.97   1000   400   401   40	l Mi	8		1			35	2,100	75. 78	2.15	1.8	3.022	12.4	152.4	2.0	100
116   FORTZIZI   22   2599   3020   51   61   62   62   63   64   64   64   64   64   64   64	4	15					200	1 200	CE 7	2 46	7	2002	21.4	26.0	16.2	5.2
The Properties   The Transformeries   The Properties   The Properties   The Properties   The Properties   The Properties   The Properties   The Properties   The Properties   The Properties   The Properties   The Properties   The Properties   The Properties   The Properties	· ru	105	EX921212				20	0.077	3.87	2.54	1.77	3.014	5.0	25.7	16.9	11.7
17   17   17   17   17   17   17   17	•	7						0.075	1.65	3.57	5.6	3.008		9.5	20.5	32.3
The Properties   Color   Col		8						0.075	1.92	5.73	5.01	3.032		10.9		28.5
7.6 EK921216 16 2991 2994 58 0.130 5.40 4.38 2.77, 2.942 0.0 534,5 66.2 7.6 EK921217 6 14 2977 2004 58 0.130 5.40 11.0 7.35 2.942 0.0 5 34,5 66.2 7.6 EK921218 24 3018 3015 304 0.003 30.00 12.35 3.005 1.0 17.1 15.7 10.0 7.6 EK92121 7 2004 2051 3048 9.0 0.07 1.30 1.30 1.25 1.0 1.0 1.0 1.2 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0		117					58	0.091	1.65	4.89	3.00	3.029	0.5	4.6		17.1
74 ER921231	€	92					58	0.130	7.06	4.38	2.74	2.993	7.0	23.4		15.8
156 ENOZIZISE 14 30018 3015 58 0.003 30.00 2.78 26.64 15.50 3.005 1.1 15.7 149.0 100 ENOZIZISE 14 3002 3046 3057 58 0.005 1.189 65.71 2.75 3.005 1.0 10.0 ENOZIZISE 14 3002 3057 305 58 0.005 1.48 65.71 27.36 3.007 0.4 77 69.4 100 ENOZIZISE 14 3002 3057 3054 58 0.007 1.44 65.71 27.36 3.007 0.4 77 69.4 10.0 ENOZIZISE 14 3005 3057 305 58 0.007 1.44 65.71 27.36 3.007 0.4 77 69.4 10.0 ENOZIZISE 14 3005 3059 59 0.007 1.44 65.71 27.36 3.007 0.4 77 69.4 10.0 ENOZIZISE 14 3005 3059 59 0.007 1.46 65.71 27.3 3.005 0.00 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.	٥,	2					28	0.110	5.88	11.30	7.32	2.942	9.0	34.5		42.9
95 ENYOZIZO 22 3 3088 364 0.000 1.38 12.56 15.90 5.065 1.1 15.7 140.9 14	9	130					58	0.083	30.80	30.98	23.51	3.017	0.5	176.0	177.1	134.4
10   12   13   14   15   15   15   15   15   15   15	- (	25					28	0.200	2.7	26.64	15.90	3.065		15.7	149.9	89.4
150   150	12	8					58	0.076	1.38	12.36	8.25	3.073	4.0	7.7	7.69	46.3
19   19   19   19   19   19   19   19	56	8					82	0.082	2.95	16.97	13.20	2.973	0.5	 	4.86	76.6
FRANCISCA   1.5   2004   2004   2007   2.44   2.01   10.47   2.003   4.60   10.67   2.003   4.60   10.67   2.003   4.60   10.67   2.003   4.60   10.67   2.003   4.60   10.67   2.003   4.60   10.67   2.003   4.60   10.67   2.003   4.60   10.67   2.003   4.60   10.67   2.003   4.60   10.67   2.003   4.60   10.67   2.003   4.60   10.67   2.003   4.60   10.67   2.003   4.60   10.67   2.003   4.60   10.67   2.003   4.60   10.67   2.003   4.60   10.67	75	25					280	0.00	1.87	45.0	27.30	20.0		70.7	7.867	24.8
15   15   15   15   15   15   15   15	32	41					200	0.070	**	2.00	15.27	5.035		2,0	1.01	900
\$2 EK921226         20         3036         3035         304         59          0.075         1.36         24.39         14.72         3.036         4.01         7.7         198.15           12 EK921227         3         3045         3045         59          0.075         2.02         24.39         14.72         3.056         4.01         7.7         198.15           14 EK921227         3         3042         59          0.075         3.02         26.12         3.05         4.01         17.4         149.2           15 EK921231         3         3024         3097         58          0.075         3.02         26.88         16.17         3.06         400.1         17.7         116.5         2.97         40.1         17.7         3.06         40.1         17.7         117.5         27.7         17.7 <td< td=""><td></td><td>36</td><td></td><td></td><td></td><td></td><td>× × × × ×</td><td></td><td>CY 53</td><td>18.01</td><td>10.40</td><td>7.930 7.054</td><td>2 5</td><td>200</td><td>101.0</td><td>4.64</td></td<>		36					× × × × ×		CY 53	18.01	10.40	7.930 7.054	2 5	200	101.0	4.64
12 E 1997   12.7   1		3.5					2 8	K	7.6	02.70	14.72	450.5	\ \ \ \ \ \	7.7	148.5	3.5
Characteristic   Char		124					265	0.075	2.82	24.50	14.62	3.059	101	15.6	135.8	81.0
75 E8921223 31 3018 28991 58 < 0.075 5.30 26.88 16.17 3.005 < MOL 17.4 140.9  76 E8921231 11 2980 2977 59 < 0.075 5.60 19.68 16.17 3.005 < MOL 17.4 140.9  77 E8921231 11 2980 2977 59 < 0.075 5.60 19.68 16.17 3.016 < MOL 11.5 1.9  78 E8921231 11 2980 2977 59 < 0.075 5.60 19.68 11.54 2.979 < MOL 11.9 112.0  78 E8921234 29 2988 2928 58 < 0.075 5.71 19.77 11.96 2.995		3					65	0.210	7.80	48.99	29.34	2.997	1.2	27.1	277.1	165.9
97 EV22133	15	K					58 <	0.075	3.03	26.12	15.93	3.005	ğ ¥	17.4	149.9	7.16
17   17   17   17   17   17   17   17	9:	76.					588	0.07	7.32	26.88	16.17	3.016	<u>Q</u>	6.1.5	153.7	92.5
100 EX921233   15 2997   2988   2928   58 0.0075   3.77   119.77   119.65   2.997   0.15   32.3   402.45   5989   2928   2928   58 0.0075   3.77   119.77   119.65   2.998   0.15   21.6   115.2   112.7   119.77   119.65   2.998   0.16   112.7   112.7   112.7   119.65   2.998   0.16   112.7	~ <u>«</u>	57	EX921231				× × ×	2000	00.7	60.VI	26.54	4.0.x	100	27.Y	211.0	120.1
SOURCE   S	2	. 2	FX021233				2 45	0.03	5	60.09	89	8	5.0	2.5	7.07	2.072
59 EY021269 30 3030 2940 57 0.100 3.32 19.18 11.56 2.985 0.6 19.5 112.7    112.7   1	20	8	EX921234				58 <	0.075	3.71	19.77	1.0	2.958	_	21.6	115.2	69.7
Color	8	29					57	0.100	3.32	19.18	11.56	2.985	9.0	19.5	112.7	67.9
66 EK921201 33 3082 3021 57 20.460 6.18 < 0.75 4.35 3.052 117.6 35.5 < HDL 156 EK921201 33 3082 3021 57 20.460 6.18 < 0.75 < 0.75 3.020 11.5 6 35.5 < HDL 156 EK921202 6 306 3033 57 0.250 0.88 < 0.75 < 0.75 3.020 1.5 5.1 < HDL 156 EK921205 19 3012 2977 57 0.250 0.88 < 0.75 < 0.75 3.020 1.5 5.1 < HDL 156 EK921205 19 3012 2977 57 0.250 0.88 < 0.75 < 0.75 2.995 4.5 16.9 < HDL 166 EK921207 4 3012 2974 55 2.600 4.71 < 0.75 2.995 17.3 2.995 10.0	5	3					> 95	0.075	5.44	< 0.30	1.14	2.994	년 *	14.6	¥DL	6.8
SAMPLES	<b>∀</b> ;	29					57	20.460	6.18	۷.0°	4.35	3.052	117.6	35.5	<u>.</u>	25.0
SAMPLES  SAMPLES  SAMPLES  SAMPLES  EXCETONE NITRIC FILTER IMPINGER (CU FT) (Lag) (L		۶					75	20.0	3.5	۸ ، د د د	C.K	3.050	 	5.5		<u> </u>
CONTRICT   CONTRICT	2						7		200	CK SC	C K	2000			į ;	
106 EX921206   12 3012   2974   55 2.600   4.71   0.75   0.75   2.993   15.8   28.6   HDL     116 EX921207   4 3015   2940   56 2.880   4.98   0.75   0.75   2.978   17.3   29.9   HDL     12	¥ = =	38					25	1.880	5.93		. c	3.042	10.8	3.5		
116 EX921207	28	50					55	2.600	4.71	< 0.75 <	6.7	2.993	15.8	28.6	V PDL	)OH >
72 EX92127B	38	116					26	2.880	86.4	× 0.75 ×	0.7	2.978	17.3	6.62	< MOL	로 •
SAMPLES SAMPLE LEAD ZINC STRONTIUM CHROMIUM SAMPLE LEAD ZINC STRONTIUM CHROMIUM SAMPLE LEAD ZINC STRONTIUM CHROMIUM SAMPLE LEAD ZINC STRONTIUM CHROMIUM SAMPLE LEAD ZINC STRONTIUM CHROMIUM SAMPLE LEAD ZINC STRONTIUM CHROMIUM SAMPLE LEAD ZINC STRONTIUM CHROMIUM SAMPLE LEAD ZINC STRONTIUM CHROMIUM SAMPLE LEAD ZINC STRONTIUM CHROMIUM SAMPLE LEAD ZINC STRONTIUM SAMPLE STRONTIUM SAMPLE STRONTIUM SAMPLE STRONTIUM SAMPLE LEAD ZINC STRONTIUM SAMPLE STRONTIUM SAMPLE LEAD ZINC STRONTIUM SAMPLE STRONTIUM S	BLANK	2					28	0.330	1.98	0.32 <	0.73	3.000	1.9	71.4		< 4.5
ACETONE MITRIC FILTER IMPINGER (CU FT) (Lighton Court			e A MOI E C				1	45	1	CTDONTILE	- Cubona		242	2	erbour 11 m	
T EK921388 EK921389 EK921389 EK921391 38.00 0 12.3 5.9 8.55 1.075 < MOL 11.4 5.5 EK921382 EK921389 EK921349 37.31 14.5 120.5 5.7 88.7 1.056 13.7 114.1 5.4 EK921392 EK921392 EK921393 EK921399 EK921398 < 2.5 5.1 3.8 1.075 < MOL 5.1 4.7 EK921392 EK921388 < 2.5 < 1.25 < 0.5 0.5 1.075 < MOL C	LOCATION		ACETONE	MITRIC	FILTER	IMPINGER	(CU FT)	60	(gu)	(Bn)	(ng)	(M3)	(ug/H3)	(ug/H3)	(ug/K3)	
ACETONE EX921388 < 2.5 5.5 5.1 3.8 1.075 < MOL 5.1 4.7 MITRIC EX921389 < 0.5 4.1 0.8 2.4 1.075 < MOL 3.8 0.7 FILTER EX921390 < 2.5 < 1.25 < 0.5 0.5 1.075 < MOL < MOL < MOL MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MOL < MO	EXHAUST RECIRC			EX921389 EX921393	EX921390 EX921348		38.00	14.5	12.3 120.5	5.9	8.55 88.7	1.075	< PDL 13.7	11.4	5.5	8.0 8.0
MIRIC EX21389 < 0.5					EVMANCE		FY021388 <	2.5	10°	5 1	K.	1 07	3		7.7	K.
EXYZ1391 < 0.5 < 1.45 < 0.5 < 1.4 1.075 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 < 101 <							EX921389 <			8	2.4	1.07	ē		0.7	2.2
							EX921390 <	, C		0.0 0.0	ξ.	5 C		E		- C

TEST: METALS #3 DATE: 06-25-92 AN1 METHOD: NIOSH 7300	TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485	PAINT: OBJECT:	LT GREEN PRIMER BRAKE PARTS, HUBS, RAMP	IIMER 5, HUBS, R	AMP.	D E IN	D E INITIALS: LJL Q A INITIALS:	5		
ACUREX BASE PUNP # (ml/min) (ml/min) (min)	PRE-CAL POST-CAL RUN TIME (ml/min) (ml/min)	LEAD (ug)	ZINC S (ng)	STRONTIUM (	CHROMIUM AVG FLOW LEAD (Ug/M3)	IVG FLOW	LEAD (ug/H3)	ZINC (ug/H3)	STRONTIUM CHROMIUM (ug/M3) (ug/M3)	CHROMIUM (ug/M3)
	RECIRC ACETONE EX921392 < 25 NITRIC EX921393 12 FILTER EX921348 < 2.5 IMPINGER EX921349 < 0.5	25 12 2.5	3,34 3,54 58 <	25 2.4 34 3.3 3.5 < 0.5 58 < 0.2 <	3 72 13.7 0.2	1.056 1.056 1.056	11.4 11.4 10.5 10.5 10.5 10.5 10.5 10.5 10.5 10.5	23.7 32.2 54.9	2.3 3.1 < MDL < MDL	2.8 68.2 13.0 * MDL

TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485  EXHAUST GRID  1 9.3 2 3.7 3 12.4  5 0.5 6 MOL  21 0.5 6 MOL  21 0.5 10 0.5 11 1.1  21 0.5 7 MOL  21 0.5 6 MOL  31 1.1  21 0.5 7 MOL  4 MOL  4 MOL  4 MOL  4 MOL  4 MOL  4 MOL  5 MOL  6 MOL  6 MOL  7 MOL  9 0.5 MOL  17 MOL  18 0.5 MOL  17 MOL  18 0.5 MOL  17 MOL  18 0.5 MOL  17 MOL  18 0.5 MOL  18 0.5 MOL  17 MOL  18 0.5 MOL  18 0.5 MOL  18 0.5 MOL  18 0.5 MOL  17 MOL  18 0.5 MOL  18 0.5 MOL  17 MOL  18 0.5 MOL	D E INITIALS: LJL Q A INITIALS: 0	-	4 21.4 Field Blank	8 0.7 TB 10.8	12 0.4	24 < MOL 28 < MOL 15.8	16 < MDL 38 17.3	20 × MDL	SAMPLE EXHAUST DUCT: < MOL
1 9.3 1 9.3 5 0.5 5 0.5 1 4 60L 4 60L			12.4	7 < NDL 0.5		· 23	15 < MOL	5.0	GRID MOL: 0.075 UG/SAMPLE
1 9.3 21 0.5 4 50 4 50 4 50 4 50 4 50 4 50 4 50 4 5	RAVIS AFB AINT BOOTH TESTS CUREX PROJECT 8485	EXHAUST GRI				22 < PDL			
	<b>⊢</b> ∆ <b>∢</b>		1				<del></del>	17 A FOL	

INLET GRID B . . . . . . . . . . . . . . . . Field Blank 11.4 28.6 ٥. % 11.4 114.1 34.1 0 D E INITIALS: LJL Q A INITIALS: 8 8 粤 EXHAUST DUCT: RECIRC DUCT: 21.6 54.9 14.0 88.2 41.9 23.4 7.7 GRID MOL: 0.3 UG/SAMPLE PAINTER MDL: 0.3 Ug/SAMPLE 19 20 2 54 8 32.3 152.4 10.9 15.7 8.2 17.4 EXHAUST GRID 5 4 Ξ 23 TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485 10 176.0 OSHA TWA: 1000 ug/ 27.8 9.5 10.7 27.1 14.5 UNITS: UB/H3 13 7 22 9 2 11.3 7.7 15.6 31.9 34.5 25.7 23.1 OBJECT: BRAKE PARTS, HUBS, RAMP 11 21 13 PAINT TYPE: LT GREEN PRIMER TEST: METALS #3
DATE: 06-25-92 AM1
METHOD: NIOSH 7300
GRID CHART 2 ~ ZINC Painter Under 14.6 Painter Over 19.5 INLET GRID A 16.9 35.5 5.1 5.1 ¥ **≤** న

TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 6485  EKHAUST G  1 9.3 2 5.6  16.9 6 20.5  16.9 66.2 177.1  21 98.4 2 258.7  13 138.5 14 277.1  17 112.0 18 231.6	D E INITIALS: LJL Q A INITIALS:		4 14.2 Field Blank 1.8	8 25.2 18 18 18	12 69.4	24, 72.0 28 101.8 < HDL	16 153.7 38 MDL	115.2	COID MILE O 3 INVESTMENT NET- 5 5
1 9.3 5 16.9 66.2 21 98.4 135.8 135.8	IS AFB T BOOTH TESTS EX PROJECT 8485	1	5.6	7 20.5	11.21	258.7	15 17.77	231.6	8 6 8 8 6 8 6 8 6 8 6 8 6 8 6 8 6 8 6 8
METALS #3 06-25-92 AM1 NIOSH 7300 RT 3 - STRONTI 112.7 Painter Over 112.7 Painter Under C MDL C	TEST: METALS #3  DATE: 06-25-92 AM1  METHOD: NIOSH 7300  ACURE GRID CHART 3 - STRONTIUM		-					17 112.0	LATTS:

Q A INITIALS: 0		Field Blank < 4.3	INLET GRID B	<b>1 2</b> •	28 < MOL	38		EXHAUST DUCT: 8.0
14	6 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	4 15.2	8 15.8	12 46.3	24 42.9 60.2	16 92.5	20 69.7	
	EXHAUST GRID	3 10.9	7 28.5 17.1	11 89.4	23 86.8	15 91.4	19 240.3	GRID MOL: 0.3 ug/SAMPLE
ACUREX PROJECT 8485	ЕХНАИ	2 < MOL	6 32.3	10	22 154.8	14 165.9	18 139.1	ug/K3
PAINT	\$ B B B B B B B B B B B B B B B B B B B	7.7	5 11.7	9 42.9	21 76.6	13 83.6 81.0	17 65.7	UNITS:
JEST: METALS #3 DATE: 06-25-92 AM1 METHOD: NIOSH 7300 GRID CHART 4 - CHROMIUM	£	Painter Over 67.9 Painter Under 6.8	INLET GRID A	25.0	10H > Y2	ş *		PAINT TYPE: LT GREEN PRIMER

The color of the	Colored Mark   Alexa   Colored Mark   Mark   Colored Mark   Colo	TEST: DATE: METHOD:	METALS #4 06-26-92 A NIOSH 7300		TRAVIS A PAINT BO ACUREX P		₹.	PAINT: OBJECT:	LT GREEN PRIMER THRUST REVERSER	PRIMER Verser		D E IN	:: ::	80	BK & LJL	ב רזו
144 E9921242	144 E9921242   13 2971   2903   77 < 0.075   0.48   1.11   0.71   2.937   2.937   2.945   2.047   2.	₽ :	ACUREX SAMPLE #	# PUMP	PRE-C (ml/m	POST-CAL (ml/min)	RUN TIME (min)	(cog)	ZINC (ng)	STRONTIUM (ug)	<u>₹</u>	AVG FLOW (L/MIN)	ے ح	EAD Jg/M3)	.EAD ZINC Jg/M3) (Jg/M3)	
2 125 EV92124.2 28 3023 3072 80 6 0.075 1.04 4.71 2.90 3.021 4 205 EV92124.2 29 3053 3077 81 6 0.075 1.04 4.71 2.90 3.021 4 205 EV92124.2 29 3053 3077 81 6 0.075 1.04 4.71 2.90 5.05 1.05 1.05 1.05 1.05 1.05 1.05 1.0	2 122 EN921243 28 3029 3012 80 < 0.075 1.04 4.71 2.90 3.021 4.02		144		2		> 11	0.075	0.48	1.11	0.71	2.937	٧	Ē	MDL 2.1	2.1
Color   Colo	\$ 102 ENOTITION \$ 105. 10.05	21	125		I PH		80	0.075	1.04	4.71	2.90	3.021	V	10	10L 4.3	K.41
\$ 98 ENGY21245 15 2083 3077 71 117 7.33 4.46 2.000 2.000 4.000 4.000 110 ENGY21245 15 2083 3077 71 117 7.33 4.46 2.000 4.000 4.000 110 ENGY21245 15 2083 3077 71 11 71 7.33 4.46 2.000 4.000 110 ENGY21245 15 2083 3073 70 4.000 7.000 110 110 110 ENGY21249 15 3020 3053 81 4.000 7.000 4.000 110 110 110 ENGY2125 46 3013 3063 81 4.000 7.000 4.000 110 110 ENGY2125 41 3039 3063 81 4.000 7.000 4.000 110 110 ENGY2125 41 3039 3063 81 4.000 7.000 4.000 114 1.000 114 ENGY2125 41 3039 3063 81 4.000 110 110 110 ENGY2125 41 3049 3003 81 4.000 110 110 110 ENGY2125 41 3049 3003 81 4.000 110 110 110 110 ENGY2125 41 3049 3003 81 4.000 110 110 110 110 ENGY2125 41 3049 3003 81 4.000 110 110 110 110 ENGY2125 41 3049 3003 81 4.000 110 110 110 110 110 110 110 110 110	6 by Exposized 15 2988 3007 70 0.075 1.10 11.2 7.38 4.46 2.996 4.10 Exposized 15 2988 3007 70 0.075 1.10 31.25 21.71 3.020 4.10 10 Exposized 15 2988 3007 70 0.075 1.10 31.25 21.71 3.020 4.10 10 Exposized 15 3028 3007 70 0.075 1.00 17.43 10.42 3.003 4.10 10.42 3.003 10.4	<b>~</b>	122		M 10		× 080	0.07	9.0°	28.48	16.83	3.060	v '	ے و	DL 3.4	3.4
6 DUP 51 ENGY1247 19 3045 2994 79 0.077 1.10 31.25 27.71 31.020 4    7 14 ENGY1247 19 3045 2994 79 0.077 1.10 31.25 27.71 31.020 4    8 ENGY1249 6 3030 3053 81 0.075 0.68 71.88 45.59 1.04    9 139 ENGY1249 6 3030 3053 81 0.075 0.68 71.88 45.59 3.047 4    10 84 ENGY1250 6 3030 3053 81 0.075 0.68 71.88 45.59 3.047 4    11 10 ENGY1245 12 3033 3054 81 0.075 0.68 71.88 45.59 3.047 4    12 84 ENGY1251 12 3039 3012 80 0.100 2.08 71.87 78 22.78 3.047 4    13 8 ENGY1254 12 2994 3013 80 0.100 2.05 144.55 77.82 3.052    14 14 ENGY1255 13 3039 3012 80 0.095 0.50 144.55 77.82 3.052    15 8 ENGY1255 13 3039 3017 80 0.095 0.50 144.55 77.82 3.052    15 8 ENGY1255 13 3039 3017 80 0.016 0.52 167.79 86.88 3.052    15 8 ENGY1255 31 3045 2997 3107 80 0.017 0.55 144.55 77.82 3.052    15 8 ENGY1255 31 3039 3017 80 0.017 0.57 144.55 77.82 3.052    16 8 ENGY1255 31 3015 3057 3066 80 0.017 0.57 144.55 77.82 3.052    16 8 ENGY1255 31 3015 3024 3077 80 0.017 0.57 144.55 12.97    16 8 ENGY1255 31 3015 3024 3017 80 0.017 0.057 0.66 45.44 26.90 3.001    16 8 ENGY1255 31 3024 3018 3025 0.038 145.74 26.90 3.001    16 8 ENGY1255 32 3024 3023 3018 302 0.007 0.017 0.007 0.04 14.55 12.907    10 200 ENGY1265 45 3009 3018 307 0.007 0.06 45.44 26.90 3.001    10 200 ENGY1265 45 3009 3018 307 0.007 0.05 0.06 45.44 26.90 3.001    10 200 ENGY1265 45 3009 3018 307 0.007 0.	6 DUP 51 EXPOSIZATO 19 3043 2994 79 0 0.075 1.10 31.25 21.77 3.020 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	t u	CO S		30		2 8	20.0	1.02	45.36	\$0.07	5.056 2.056	¥ 3	<del>ا</del> ح	7.0	- ° 4
6 DUP 51 EXCRETES 1 24 2043 5074 81 < 0.007 1.00 17.2 51.0 51.0 51.0 51.0 51.0 51.0 51.0 51.0	6 DUP 51 ENSTITAS 24 2988 5074 81 < 0.075 1.08 71.43 10.42 3.003 <	1	100		4 1		2 8			2000	24.40	7 030	2 5	٠.	, , , , , , , , , , , , , , , , , , ,	4.4
Fig. 1972   Fig.	1		2.5		30		× × ×	20.0	0.0	57.15	10.71	3.020	2 5		0 · ·	9 4
15   15   15   15   15   15   15   15	B   B   EN921249		171		<b>4</b> W		0 6			75 28	74.07	2.003	2 9		\$ C	* *
139 E8921256	13   15   15   15   15   15   15   15	- 00	8		א ר		2 6	200	20.0	25.52	05.17	770°E				
10 84 EY921251 42 3033 3024 80 0.100 2.08 99.64 54.88 3.026 11 0.1 62 EX921252 21 3039 3012 80 0.110 0.52 167.79 96.84 3.026 12 12 1402 EX921252 21 3039 3012 80 0.110 0.52 167.79 96.84 3.026 12 12 1402 EX921255 48 2997 3107 80 0.010 0.52 167.79 96.84 3.026 12 12 1402 EX921265 48 2997 3107 80 0.010 0.52 167.79 96.84 3.026 12 12 1402 EX921265 31 2988 2997 3107 78 < 0.075 0.54 12.61 71.22 2.977 78 < 0.075 0.54 12.61 71.22 2.977 78 < 0.075 0.54 12.61 71.22 2.977 78 < 0.075 0.54 12.61 71.22 2.977 78 < 0.075 0.54 12.61 71.22 2.977 78 < 0.075 0.54 12.61 71.22 2.977 78 < 0.075 0.54 12.61 71.22 2.977 78 < 0.075 0.54 12.61 71.22 2.977 78 < 0.075 0.54 12.61 71.22 2.977 78 14.7 80.00 0.11 < 0.30 119.78 69.06 3.002 14.7 80.00 14.	10 86 EX921251 42 3033 3024 80 0.100 2.08 93.66 54.88 3.029 11 102 EX921252 21 3039 3012 80 0.110 0.52 167.79 96.26 3.029 11 104 63 EX921255 48 2897 3107 80 0.011 0.62 167.79 96.26 3.052 21 142 EX921266 31 2888 2895 0.09 0.51 122.61 77.82 3.052 22 142 EX921266 31 2888 2895 80 0.012 0.51 122.61 77.22 2.977 23 151 EX921267 35 3057 3066 80 0.012 0.57 104.75 77.82 3.052 24 153 EX921267 31 3024 3027 778 0.013 122.61 77.22 2.977 25 151 EX921267 31 3024 3027 778 0.014 3.32 19.18 11.56 3.062 26 15 EX921267 31 3027 3066 80 0.017 0.57 10.67 114.36 3.062 27 15 EX921267 31 3024 3027 778 0.017 0.57 20.46 114.36 3.002 28 EX921269 55 2978 3015 778 0.077 0.68 45.44 26.90 3.021 29 Over 11 EX921267 49 3048 3072 80 0.099 1.10 107.84 62.74 3.002 20 14 EX921267 45 3003 3003 811 0.17 1.22 114.36 62.71 3.003 21 14 EX921267 45 3009 3018 81 0.17 1.22 114.36 62.71 3.003 24 EX92127 40 2048 3003 77 0.075 0.78 0.38 0.46 6.74 3.002 25 14 EX92127 40 2048 3003 77 0.075 0.78 0.38 0.46 5.44 26.90 3.001 27 0.097 0.075 0.77 0.66 45.44 26.90 3.001 28 EX92127 40 2048 3003 77 0.075 0.78 0.38 0.46 5.44 26.90 3.001 28 EX92127 40 2048 3003 77 0.075 0.78 0.38 0.40 0.54 3.002 29 10 EX92127 40 2048 3003 77 0.075 0.78 0.38 0.40 0.54 3.002 20 14 EX92127 40 2048 3003 77 0.075 0.78 0.38 0.40 0.54 3.002 20 14 EX92127 40 3048 3003 77 0.075 0.78 0.38 0.40 0.54 3.002 21 EXPRESSIVE 45 3009 77 0.075 0.78 0.38 0.40 0.54 3.002 22 14 EXPRESSIVE 45 3009 77 0.075 0.78 0.38 0.38 0.42 3.003 24 15 EX92127 40 3048 3003 77 0.075 0.78 0.38 0.38 0.42 3.003 25 15 EXPRESSIVE 47 3015 3000 77 0.075 0.78 0.51 0.51 2.903 26 16 EXPRESSIVE 47 0.075 0.78 0.38 0.30 0.50 0.50 0.50 0.50 0.50 0.50 0.50	•	139		יא ו		78	0.075	0.42	39.45	22.78	3.041				1.8 166.3
102 E921552   21 3039 3012   80 0.110 0.52 167.79 96.84 3.026   104	102 EV921252	2	8		189		08	0.100	2.08	3.5	54.88	3.029	0	4	8.6	4 8.6 386.5
1 DUP	DUP   658 EV921254   12 28994   3003   61   0.11   0.62   175.76   106.70   2.8999     2		102		m		80	0.110	0.52	167.79	26.84	3.026	0	'n	5 2.1	5 2.1 693.2
12 145 EX921255 48 2897 3107 80 0.095 0.50 144.55 77.82 3.052 1.052 142 EX921265 48 2895 2965 80 0.095 0.51 122.61 71.22 2.977 22 142 EX921265 31 2988 2965 80 0.012 0.57 201.46 114.36 3.062 2.977 24 153 EX921266 11 3024 3057 79 0.11 < 0.13 12.61 71.22 2.977 79 0.11 < 0.13 12.61 71.25 2.977 79 0.11 < 0.13 12.61 71.25 2.975 1.05 1.05 1.05 1.05 1.05 1.05 1.05 1.0	12   145 EK921255		63		~		8	0.11	0.62	175.76	106.70	2.999	0	'n.	2.6	5 2.6 723.7
1,0   EXY21265   1,1   2043   2945   2947   1,0   0.017   0.511   12.01   2.774   2.011   2.015   2.011   2.015   2.	Columbia C	12	145	255	(N)		88	8	0.50	134.55	77.82	3.052	ò	•	2.0	0.0 0.0
15   EX921267   35   3057   3066   80   0.11   0.30   190.76   114.36   3.052   3.05	24 151 EV271267 35 3057 3066 80 0.11 c 0.57 12.64 114.35 3.055 3.0	25	101		36		0 0		0.40	122 41	74 22	5.01	20		200	2 4 54.0
24         153 EX921268         53         3015         3091         80         0.11         0.30         180.76         104.70         3.053           13         159 EX921266         11         3024         3027         79         0.11         3.32         19.18         11.56         3.026           14         147 EX921256         31         3024         3027         79         0.19         1.82         204.99         117.51         2.976           15         142 EX921256         32         2978         81         0.079         0.38         145.74         85.04         2.976           16         18 EX921260         1         3036         2951         79         0.077         0.69         6.69         4.06         2.994         4.06         2.994         2.994         4.06         2.994         2.994         4.06         2.994         4.06         2.994         4.06         2.994         4.06         2.994         4.06         2.994         4.06         2.994         4.06         2.994         4.06         2.994         4.06         2.994         4.06         2.994         4.06         2.994         4.06         2.994         4.06         2.994         4.06	24         153 EX921268         53         3015         3091         80         0.11         0.13         180.76         104.70         3.053           13         159 EX921266         53         3015         3091         70         0.11         3.32         19.18         11.56         3.026           14         147 EX921257         30         3033         2971         78         0.078         0.30         119.78         69.06         3.026           15         86 EX921259         35         2978         3012         80         0.079         0.30         119.78         69.06         3.026           16         86 EX921259         55         2978         3018         79         0.075         0.69         6.69         4.06         2.994         4.06         2.994         4.06         2.994         4.06         2.994         4.06         2.994         4.06         2.994         4.06         2.994         4.06         2.994         4.06         2.994         4.06         2.994         4.06         2.994         4.06         2.994         4.06         2.994         4.06         2.994         4.06         2.994         4.06         2.994         4.06         2.994	35	1.5		4 14		8 &	0.0	0.57	201.46	116.36	3.062				2.3 822.6
13   159 EX921256   11   3024   3027   79   0.1   3.32   19.18   11.56   3.026     14   147 EX921257   30   3033   2971   78   0.078   0.30   119.78   69.06   3.002     15   138 EX921256   35   2978   3015   80   0.095   0.38   145.74   85.04   2.996     16   86 EX921250   1   3036   2951   79   0.075   0.69   6.69   4.06   2.994     17   192 EX921260   1   3036   2951   79   0.077   0.66   45.44   25.09   3.021     18   149 EX921263   44   3003   3003   81   0.077   0.66   45.44   26.90   3.021     19   200 EX921264   45   3003   3018   81   0.077   0.64   45.47   27.72   3.005     10   200 EX921265   44   3003   3018   81   0.077   0.64   45.67   27.72   3.005     14   EX921264   45   3009   3018   81   0.077   0.22   114.36   66.21   3.014     14   200 EX921276   34   3048   3003   77   0.098   0.38   157.58   91.44   3.026     15   200 EX921277   40   2971   2245   77   0.098   0.38   157.58   91.44   3.026     15   200 EX921277   54   3021   3045   77   0.075   5.42   0.35   0.35   2.993     16   200 EX921238   51   2985   3000   77   0.075   1.23   0.38   0.42   3.035     18   148 EX921239   20   2965   2985   76   0.075   1.08   0.55   0.51   2.975     18   148 EX921240   17   3015   3005   76   0.075   1.08   0.55   0.51   2.975     15   200 EX921240   17   3015   3005   1.08   0.55   0.51   2.975     15   200 EX921240   17   3015   3005   3.08   0.55   0.51   3.012     15   200 EX921240   17   3015   3005   30	13   159 EX921256   11   3024   3027   79   0.1   3.32   19.18   11.56   3.026   11.51   13.024   30.33   2971   78   0.078   0.30   119.78   69.06   3.002   13.002   13.002   13.002   13.002   13.002   14.5	25	153		) IN		8	0	c 0.30	180.76	18.20	3.053	0		) <del>1</del> 0+ v	
14         147 EX921257         30         3033         2971         78         0.078         0.30         119.76         69.06         3.002           15         133 EX921256         32         3024         2928         81         0.19         1.82         204.99         117.51         2.976           16         18 EX921256         1         3036         2951         79         0.075         0.69         6.69         4.06         2.997           18         149 EX921261         18         3024         3018         78         0.077         0.66         45.44         26.90         3.021           18         149 EX921261         18         3024         3018         81         0.077         0.66         45.44         26.90         3.021           19         200 FX         3033         3018         81         0.077         0.66         45.44         26.90         3.021           20         14 EX921262         14         3003         3018         81         0.077         0.66         45.44         26.90         3.021           20         14 EX921262         14         3003         3018         0.077         0.66         45.44         26	14         147 EX921257         30         3033         2971         78         0.078         0.30         119.78         69.06         3.002           15         133 EX921256         32         2024         2928         81         0.19         1.82         204.99         117.51         2.976           16         86 EX921256         1         3036         2951         79         0.075         0.69         6.69         4.06         2.997           17         192 EX921261         18         3024         3018         81         0.077         0.66         45.44         26.90         3.021           18         149 EX921262         14         3003         3018         81         0.077         0.66         45.44         26.90         3.021           19         143 EX921262         14         3003         3018         81         0.077         0.66         45.44         26.90         3.021           20         114 EX921262         14         3003         3072         80         0.078         1.16.36         45.44         3.06         3.014           20         114 EX921264         45         3048         3003         77         0.098         <	13	159	256	M		2	0.1	3.32	19.18	11.56	3.026	4.0		13.9	
15 135 EV921256 32 3024 2928 81 0.19 1.82 204.99 117.51 2.976 16 86 EV921256 1 3036 2951 79 0.095 0.58 145.74 65.04 2.997 17 192 EV921261 18 3024 3018 77 0.077 0.66 45.44 26.90 3.021 18 149 EV921261 18 3024 3018 81 0.077 0.66 45.44 26.90 3.021 19 200 EV921262 14 3003 3018 81 0.077 0.42 47.67 27.72 3.003 20 14 EV921263 45 3009 3018 81 0.17 1.22 14.36 65.21 3.046 20 14 EV921276 34 3048 3003 77 0.098 0.38 157.58 91.44 3.026 21 11 EV921277 40 2971 2945 77 < 0.075 0.39 15.87 9.50 2.958 21 12 EV921238 51 2985 3000 77 < 0.075 5.42 0.38 0.42 3.03	15 135 EX921256 32 3024 2228 81 0.19 1.82 204.99 117.51 2.976 16 8 EX921256 1 3036 2251 79 0.00 0.095 0.38 145.74 85.04 2.997 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	14	147	257	MI		2	0.078	< 0.30	119.78	90.69	3.002	N.0		10E V	< PDL 511.5
17   192 EXYZ1253   3.35   2575   79   0.075   0.55   14.574   25.974   4.06   2.994   4.06   4.06   2.994   4.06   4.06   2.994   4.06   4.06   4.06   2.994   4.06   4.06   4.06   2.994   4.06   4.06   4.06   4.06   2.994   4.06   4.06   4.06   4.06   2.994   4.06   4.06   4.06   4.06   4.06   2.994   4.06   4.06   4.06   4.06   4.06   2.994   4.06   4.0	17   192 EN221264   13   13   13   13   14   15   15   15   15   15   15   15	5.5	133	258	ru ć		5	0.19	1.82	205.8	17.51	2.976	B .		9.7	7.6 850.4
18   149 EV221261   18   3024   3018   78   0.077   0.66   45.44   26.90   3.021     19   143 EV221262   14   3003   3003   81 < 0.075   0.42   47.67   27.72   3.003     19   200 EV221263   49   3048   3072   80   0.098   1.10   107.84   62.74   3.060     20   114 EV221264   45   3009   3018   81   0.17   1.22   114.36   66.21   3.014     20   114 EV221276   34   3048   3003   77   0.098   0.38   15.758   91.44   3.005     30   123 EV221277   54   3021   3046   77 < 0.075   5.42   0.64   0.54   3.042     31   148 EV221238   51   2985   3000   77 < 0.075   0.77   0.37   0.38   0.42   3.03     32   148 EV221240   17   3015   3009   76   0.075   1.23   0.51   2.975     31   148 EV221240   17   3015   3009   76   0.017   0.51   0.51   0.51     32   148 EV221240   17   3015   3009   76   0.017   1.05   0.51   0.51   2.975     33   148 EV221245   17   3015   3009   76   0.017   1.05   0.51   0.51   0.51     34   148 EV221240   17   3015   3009   76   0.017   1.05   0.51   0.51   0.51     35   148 EV221240   17   3015   1.08   0.52   0.51   2.975     36   148 EV221255   14	18 149 EV221261 18 3024 3018 78 0.077 0.66 45.44 26.90 3.021 19 143 EV221262 14 3003 3003 81 < 0.077 0.66 45.44 26.90 3.021 19 143 EV221262 49 3048 3072 80 0.098 1.10 107.84 62.74 3.060 20 114 EV221264 49 3048 3018 81 0.17 1.22 114.36 66.21 3.014 10 10 EV221264 40 2971 2945 77 < 0.098 1.38 157.58 91.44 3.056 11	10	85	600	4		38	250	909	*/°C*	5 4 5 4	700,7			- 0	200000
18 Dup         143 EX921262         14         3003         3003         81 < 0.075         0.42         47.67         27.72         3.003            19	B DUP	60	149	261	M		22	0.077	8	45.44	26.90	3.021	0.3		2.8	2.8 192.8
19 200 EY921263 49 3048 3072 80 0.098 1.10 107.84 62.74 3.060 20 114 EY921264 45 3009 3018 81 0.17 1.22 114.36 66.21 3.014  P over 111 EY921276 45 3009 3018 81 0.17 1.22 114.36 66.21 3.014  Under 82 EY921277 40 3971 2945 77 < 0.075 0.39 15.87 9.50 2.958 < 2.4 123 EX921237 54 3021 3045 77 < 0.075 5.42 0.64 0.54 3.042 < 3.4 123 EX921238 51 2985 3000 77 < 0.075 1.23 0.38 0.42 3.03 2.993 < 1.4 EX921239 51 2985 3000 77 < 0.075 0.78 0.52 0.30 2.993 < 3.4 148 EX921240 17 3015 3009 76 0.077 0.78 0.52 0.51 2.975 < 3.8 166 EY92144 43 3012 76 < 0.075 1.08 0.52 0.51 2.975 < 3.012 4.14 1.15 0.51 0.44 3.012 < 3.012 4.14 1.15 0.51 0.51 0.44 3.012 < 3.012 4.14 1.15 0.51 0.51 0.51 0.51 0.51 0.51 0.51	19 200 EX921263 49 3048 3072 80 0.098 1.10 107.84 62.74 3.060 20 114 EX921264 45 3009 3018 81 0.17 1.22 114.36 66.21 3.014 P over 114 EX921264 45 3009 3018 81 0.17 1.22 114.36 66.21 3.014 IN TO EX921276 34 3048 77 < 0.075 0.39 15.87 9.50 2.958 <		143	262	in)		> 18	0.075	0.42	17.67	27.72	3.003			1.7	1.7 196.0
20 114 EX221264 45 3409 3418 81 0.17 1.22 114.36 66.21 5.014  P over 111 EX221276 45 3403 77 0.098 0.38 157.58 91.44 5.026  Under 82 22277 40 2971 2945 77 0.075 0.39 15.87 9.50 2.958 4 1 2 2 3 1 1 3 1 1 2 3 1 1 3 1 1 3 1 1 3 1 1 3 1 1 3 1 1 3 1 1 3 1 1 3 1 1 3 1 3 1 1 3 1 1 3 1	20 114 EXC21264 45 3009 3018 81 0.17 1.22 114.56 66.21 5.014  P over 111 EXV21276 34 3048 3003 77 0.098 0.38 157.58 91.44 5.026  Under 122 EXV21277 52 3018 3066 77 0.075 5.42 0.39 15.87 9.50 2.958  ZA 123 EXV21237 54 3021 3045 77 0.075 5.42 0.64 0.54 3.042  SA 124 EXV21238 51 2985 3000 77 0.075 0.78 0.52 0.54 3.033  ZB 127 EXV21240 17 3015 3009 76 0.075 0.78 0.52 0.51 2.975  SB 166 EXV21241 43 3012 3012 76 0.075 1.08 0.52 0.42 3.012  BLANK 158 EXV21235 7 0.000 7	5	200	263	MI		8	0.098	1.10	107.84	62.74	3.060	4.0		7.5	4.5 440.5
Under 82 EXC21270 34 3045 3003 77 0.075 0.38 15.75 91.44 5.020 1.075 0.293 1.075 0.275 1.23 0.293 1.075 0.275 1.23 0.250 0.293 1.075 0.275 1.075 0.275 0.293 1.075 0.275 0.293 1.075 0.275 0.293 1.075 0.275 0.293 1.075 0.275 0.293 1.075 0.275 0.293 1.075 0.275 0.293 1.075 0.275	Under 82 EXC1277 40 2971 2945 77 < 0.075 0.39 157.28 91.54 5.022 1.004 1.005 1	-	4LL	*	A) 1		51	0.17	7.22	114.36	2.83	5.014			0.0	5.0 468.5
14 70 EX221236 52 3018 3066 77 < 0.075 5.42 0.64 0.54 3.042 1.04	TA 70 EXP21236 52 3018 3066 77 < 0.075 5.42 0.64 0.54 3.042 ZA 123 EXP21236 52 3018 3066 77 < 0.075 1.23 0.38 0.42 3.033 3A 54 EXP21238 51 2985 3000 77 < 0.075 2.74 0.32 0.30 2.993 18 148 EXP21239 20 2965 2985 76 < 0.075 0.77 0.78 0.52 0.51 2.975 28 127 EXP21240 17 3015 3009 76 0.075 0.78 0.52 0.51 2.975 38 166 EXP21241 43 3012 3012 76 < 0.075 1.08 0.52 0.42 3.012 BLANK 158 EXP21235 7 7 9 < 0.075 3.58 < 0.30 < 0.30 3.000 0.000 0.000	<b>-</b>	- C8	27.0	20		12	200	0.08	15,38	44.0	2.020 0.020 0.058	2		0,1	7.070 0.1
2A 123 EX921237 54 3021 3045 77 < 0.075 1.23 0.38 0.42 3.033 3A 54 EX921238 51 2985 3000 77 < 0.075 2.74 0.32 0.30 2.993 18 146 EX921240 17 3015 3009 76 0.015 0.78 0.52 0.51 2.975 2B 162 EX921240 17 3015 3009 76 0.01 4.12 0.51 0.44 3.012 3B 164 EX921245 7 7	2A 123 EX921237 54 3021 3045 77 < 0.075 1.23 0.38 0.42 3.033	3	32	236	1 347		12	0.075	5.42	79	0.54	3.042			2	_
3A 54 EX921238 51 2985 3000 77 < 0.075 2.74 0.32 0.30 2.993 18 148 EX921239 20 2965 2985 76 < 0.075 0.78 0.52 0.51 2.975 28 1427 EX921240 17 3015 3009 76 0.1 4.12 0.51 0.44 3.012 38 166 EX92135 7 70 0.075 1.08 0.52 0.42 3.012 8LANK 158 EX921235 7 79 < 0.075 3.58 < 0.30 < 0.30 3.000 <	3A 54 EX921238 51 2985 3000 77 < 0.075 2.74 0.32 0.30 2.993 18 148 EX921239 20 2965 2985 76 < 0.075 0.78 0.52 0.51 2.975 2.975 2.77 0.52 0.51 2.975 28 127 EX921240 17 3015 3009 76 0.075 0.1 4.12 0.51 2.975 3.012 38 166 EX921241 43 3012 3012 76 < 0.075 1.08 0.52 0.42 3.012 8LANK 158 EX921235 7 7 79 < 0.075 3.58 < 0.30 < 0.30 3.000 0.00	2A	123	237	(M)		71.	0.075	1.23	0.38	0.42	3.033	<b>10</b>		5,3	5.3
18 148 EX921239 20 2965 2985 76 < 0.075 0.78 0.52 0.51 2.975 < 28 157 EX921240 17 3015 3009 76 0.1 4.12 0.51 0.44 3.012 38 164 EX921241 43 3012 3012 76 0.075 1.08 0.52 0.42 3.012 8LANK 158 EX921235 7 7 79 < 0.075 3.58 < 0.30 < 0.30 < 0.30 3.000 <	18 148 EX921239 20 2965 2985 76 < 0.075 0.78 0.52 0.51 2.975 28 127 EX921240 17 3015 3009 76 0.017 4.12 0.51 0.44 3.012 38 166 EX921241 43 3012 3012 76 < 0.075 1.08 0.52 0.42 3.012 BLANK 158 EX921235 7 7 < 0.075 3.58 < 0.30 < 0.30 3.000 0.000 p.	34	24	238	~		× 11	0.075	2.7%	0.32	0.30	2.993	Y HOL		11.9	11.9
28 127 EXYZ1240 17 3012 3012 76 0.075 1:08 0.52 0.42 3.012 4 8.012 4 15 12 4 15 12 4 15 12 4 15 12 4 15 12 4 15 12 4 15 12 4 15 12 4 15 12 4 15 12 4 15 12 4 15 12 4 15 12 4 15 12 4 15 12 4 12 4	28 127 EXYZ1240 17 3013 3012 76 0.11 4.12 0.51 0.44 3.012 38 166 EX921241 43 3012 3012 76 < 0.075 1.08 0.52 0.42 3.012 BLANK 158 EX921235 7 7 0.007 3.58 < 0.30 < 0.30 0.000	<b>#</b> (	148	239	<b>(</b> 1)		× %	0.075	0.78	0.52	0.51	2.975	년 *		4.6	3.4
BLANK 158 EX921235 7 JULY 79 < 0.075 3.58 < 0.30 < 0.30 3.000 <	BLANK 158 EX921235 7 301 77 < 0.075 3.58 < 0.30 < 0.300 0.000 p	9 2	774	240	<b>1</b> M		2,42	, c	7	0.5	44.0	3.012			7.0	2.2 2.7
		BLA	82	235	,		22	0.075	3.58	< 0.30 ×	0.30	3.000	< 0.3		15.1	15.1 < 1.3
FIGURES MILLEROLLS STATE STATES		LOCATION				IMPINGER	(CU FT.)	(Bn)	(Bn)	(Bn)		(#3)	(ug/K3)		(ng/kg)	(ug/H3) (ug/H3)
SAMPLES SAMPLES SAMPLE LEAD ZINC STRONTIUM CHRONIUM SAMPLE OCATION ACETOME NITRIC FILTER IMPINGER (CU FT) (ug) (ug) (ug) (ug)	OCATION ACETOME NITRIC FILTER IMPINGER (CU FT) (Ug) (Ug) (Ug) (N3)	EXHAUST RECIRC		1447 EX9214	EX921	EX921450	48.30	00	25.5	14.08	21.58	1.367	¥ ¥ ¥		18.7	18.7 12.3 42.9 10.8
OCATION ACETONE NITRIC FILTER IMPINGER (CU FT) (Ug) (Ug) (Ug) (Ng) (Ng)  EXHAUST EX921447 EX921448 EX921450 EX921450 48.30 0 25.5 16.8 21.58 1.367  RECIRC EX921455 EX921457 EX921457 EX921458 46.09 0 56 14.08 43 1.304	OCATION ACETONE NITRIC FILTER IMPINGER (CU FT) (ug) (ug) (ug) (wg) (M3)  EXMANST EX921447 EX921449 EX921450 48.30 0 25.5 16.8 21.58 1.367  RECIRC EX921455 EX921456 EX921457 EX921458 46.09 0 56 14.08 43 1.304				EXHAUST	ACETONE	EX921447 <	2.5	5.2	10.6	8.9	1.367	JOH >		3.8	
OCATION         SAMPLE         LEAD         ZINC         STRONTIUM CHRONIUM SAMPLE           OCATION         ACETONE         NITRIC         FILTER IMPINGER         (CU FT)         (Ug)         (Ug)         (Ug)         (NG) <t< td=""><td>OCATION ACETOME NITRIC FILTER IMPINGER (CU FT) (ug) (ug) (ug) (N3)  EXHAUST EX921447 EX921448 EX921449 EX921450 48.30 0 25.5 16.8 21.58 1.367  RECIRC EX921455 EX921456 EX921457 EX921447 &lt; 2.5 5.2 10.6 6.8 1.367</td><td></td><td></td><td></td><td></td><td></td><td>EX921448 &lt;</td><td>0.5</td><td>2.3</td><td>9.4</td><td>3.50</td><td>1.367</td><td><u> </u></td><td></td><td>1.7 M</td><td>-</td></t<>	OCATION ACETOME NITRIC FILTER IMPINGER (CU FT) (ug) (ug) (ug) (N3)  EXHAUST EX921447 EX921448 EX921449 EX921450 48.30 0 25.5 16.8 21.58 1.367  RECIRC EX921455 EX921456 EX921457 EX921447 < 2.5 5.2 10.6 6.8 1.367						EX921448 <	0.5	2.3	9.4	3.50	1.367	<u> </u>		1.7 M	-
COATION         SAMPLES         SAMPLE         LEAD         ZINC         STRONTIUM         CHROHIUM SAMPLE           EXMAUST         EXP21447         EXP21446         EXP21446         EXP21445         EXP21446         EXP2144	OCATION ACETONE NITRIC FILTER IMPINGER (CU FT) (ug) (ug) (ug) (H3)  EXHAUST EX921447 EX921448 EX921449 EX921450 48.30 0 25.5 16.8 21.58 1.367  RECIRC EX921455 EX921456 EX921457 EX921457 < 2.5 14.08 4.3 1.367  EXHAUST ACETONE EX921447 < 2.5 5.2 10.6 6.8 1.367  FILTED EX921448 0.5 5.3 4.6 3.50 1.367					œ	EX921450 <	0.5	200	< 0.2	07.6	1.367	₩ ₩			13.2 < ND
COLATION         SAMPLE SAMPLE         LEAD         ZINC         STRONTIUM         CMGD/LE           EXHAUST         EXP21447 EX921448 EX921450         48.30         0         25.5         16.8         21.58         1.367           RECIRC         EX921455 EX921457 EX921458         46.09         0         25.5         16.8         21.58         1.367           RECIRC         EX921455 EX921457 EX921458         46.09         0         56         14.08         43         1.364           RECIRC         EX921457 EX921458 EX921468         0.5         5.2         10.6         6.8         1.367           RITRIC         EX921469 < 2.5	OCATION         ACETONE         NITRIC         FILTER         IMPINGER         (CU FT)         (Ug)         (Ug)         (Ug)         (Ug)         (W3)           EXMAUST         EX921447 EX921449 EX921456         EX921456 EX921456 EX921457 EX921458         46.09         0         25.5         16.08         21.58         1.304           RECIRC         EX921455 EX921457 EX921458         EX921447 EX921447         2.5         5.2         10.6         6.8         1.367           NITRIC         EX921449 EX921449         2.5         4.125         1.6         1.86         1.367           IMPINGER         EX921450 EX921450         0.5         1.8         0.2         9.40         1.367															

	UM CHRONIUM ) (ug/M3)	8 2.8 4 19.9 6 1.1
	STRONTIUM C (ug/M3) (	2.8 7.4 0.6 * MDL
INITIALS: BN & LJL INITIALS:	ZINC (ug/M3)	8.4 19.2 4 PDL 15.3
NITIALS: NITIALS:	LEAD (ug/M3)	2222 * * * *
0 F 11	CHROMIUM AVG FLOW LEAD (Ug) (L/MIN) (Ug/M3)	306,1
	CHROMIUM (ug)	3.6 26.00 1.4 12.00
R IMER Erser	STRONTIUM (ug)	3.7 9.6 0.78 : 0.2
LT GREEN PRIMER THRUST REVERSER	(Bn)	11 25 1.25 20 <
PAINT: OBJECT:	(ng)	0 2 5 5 5 5 5 5
ς.	RUN TIME (min)	EX921455 < EX921456 < EX921457 < EX921457 <
TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485	POST-CAL RUN TIME (ml/min)	ACETONE NITRIC FILTER INPINGER
TRAVIS AF PAINT BOO ACUREX PR	PRE-CAL (ml/min)	RECIRC
S #4 -92 AM1 7300	ACUREX BASE PUMP # (ml/min)	
TEST: METALS #4 DATE: 06-26-92 AM1 METHOD: NIOSH 7300	ACURE) GRID LOC SAMPLI	

Painter Over 1		ACUREX PROJECT 8485			
	0 0 0 0 0 0 0 0 0 0 0	EXHAUST GRID	9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	9	
nder	< HOL 2	- HOL	3 × MDL	10H >	Field Blank < 0.3
INLET GRID A	9 10H >	104 >	7 < HDL	8 - MDL - MDL	INLET GRID B
•	10 + HDL	<b>7.</b> 0	11 0.5 0.5	12 0.4	,
21 × HDL	1 22 <	7.0	23 0.5	24 0.5	28 0.4
3A 4 MDL	14 17	£:0	15 0.8	16 0.4	100 > 9E
71	7	3 0.3 < HOL	19 0.4	20 0.7	
PAINT TYPE: LT GREEN PRIMER U	UNITS: Ug/H3	9 8 8 8 9 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	GRID MDL: 0.075 ug/SAMPLE	.g/SAMPLE	EXHAUST DUCT: < MOL

INLET GRID B Field Blank 15.1 45.9 18.7 3.4 18.0 4.7 D E INITIALS: BN & LJL Q A INITIALS: 0 38 # 8 **EXHAUST DUCT:** RECIRC DUCT: 5.0 1.6 2.0 24 NDL 4.1 3.2 GRID MOL: 0.3 UG/SAMPLE PAINTER MOL: 0.3 UB/SAMPLE 2 2 12 80 7.6 2.4 2.3 4.5 3.4 2.1 EXHAUST GRID 2 2 = 2 TRAVIS AFB
PAINT BOOTH TESTS
ACUREX PROJECT 8485 2.8 4.4 8.6 2.1 14 < MOL 18 OBJECT: THRUST REVERSER OSHA TWA: 1000 ug/M3 2 22 Ug/N3 UNITS: 2.9 2.0 13.9 4.9 1.8 2.1 5 17 21 0 PAINT TYPE: LT GREEN PRIMER Painter Over TEST: METALS #4
DATE: 06-26-92 AM1
METHOD: NIOSH 7300 Painter Under 1.7 INLET GRID A GRID CHART 2 - ZINC 5.3 11.9 23.1 ¥ న ٤

INLET GRID B Field Blank < 1.3 2.3 10.8 D E INITIALS: BN & LJL Q A INITIALS: 0 2.2 2.3 12.3 9 82 8 **EXHAUST DUCT:** RECIRC DUCT: EXHAUST GRID 12 551.1 24 740.1 16 608.0 183.2 291.3 468.5 GRID MDL: 0.3 Ug/SAMPLE PAINTER MOL: 0.3 UB/SAMPLE 20 40 15 850.4 116.3 339,4 693.2 723.7 822.6 440.5 4 = ຄ TRAVIS AFB
PAINT BOOTH TESTS
ACUREX PROJECT 8485 10 386.5 514.9 14 511.5 18 192.8 196.0 19.5 131.0 ~ 9 OSHA TWA: 7? UG/H3 ug/H3 6.4 31.2 166.3 22.1 80.2 28.3 UNITS: 17 2 2 OBJECT: THRUST REVERSER PAINT TYPE: LT GREEN PRIMER GRID CHART 3 - STRONTIUM Painter Over 676.4 TEST: METALS #4 DATE: 06-26-92 AM1 METHOD: NIOSH 7300 Painter Under 69.7 INLET GRID A 1.6 1.4 2.7 ¥ ≤ న

INLET GRID B Field Blank < 1.3 33.0 **1**.8 15.8 2.3 4.9 D E INITIALS: BN & LJL Q A INITIALS: 0 F 恕 8 EXHAUST DUCT: RECIRC DUCT: 20 271.2 16 354.7 318.7 24 428.7 176.6 107.6 PAINTER MOL: 0.3 Ug/SAMPLE GRID MOL: 0.3 Ug/SAMPLE 15 487.5 19 256.3 6.995 68.7 202.1 439.3 **EXHAUST GRID** 23 = 18 114.2 114.0 TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485 14 294.9 10 226.5 22 299.1 91.0 42.8 12.0 OSHA TWA: 50 ug/M3 Ug/IG UNITS: 17.2 127.5 48.4 18.8 8.1 3.1 4 5 7 PAINT TYPE: LT GREEN PRIMER OBJECT: THRUST REVERSER GRID CHART 4 - CHROMIUM Painter Over 392.5 TEST: METALS #4 DATE: 06-26-92 AM1 METHOD: NIOSH 7300 Painter Under 41.7 INLET GRID A 1.8 1.3 2.3 ă ≤ ð

TEST: ME DATE: 06 METHOD: NJ	METALS #5 06-26-92 AM2 NIOSH 7300 Non paint time deducted	2 ime dedu	cted	TRAVIS AF PAINT BOO ACUREX PR	TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485	<u>~</u>		PAINT: OBJECT:	GUNSHIP GRAY POLY THRUST REVERSER	AY POLY Erser			0 P I	INITIALS: INITIALS:	i
10 LOC	UREX MPLE #	*	PUMP #	υĘ	POST-CAL (ml/min)	RUN TIME (min)	LEAD (ug)	ZINC (ug)	STRONT IUM (ug)	CHROMIUM (ug)	AVG FLOW	LEAD (ug/M3)	ZINC (ug/M3)	STRONTIUM (ug/M3)	CHROMIUM (ug/M3)
8 8 8		5 1 5 1													
- (	189 EX	EX921157	25	5003		8	0.0	26.0	> 0.30 >	0.30	5.032		4.0		1 2 3
~ 1	157 EX	251128	Ç!		•	8	0.07	70.0	0.30 ×	0.30	2.030		1.1		
٠,	188 EX	EX921139	_ `		3000	28	0.00	0.50	0.30 <	0.30	3.008		U. T	<u> </u>	- N
<b>.</b>	198 EX	721140	ع ه			> /0	C K	0.0	0.00	0.50	3.020				
^	211 EX	141176	8,0			83		9.0	0.30 ×	0.50	5.0.4 4.0.4		C. 7		
		EXY21142	¥ .			83	0.00		0.30	0.00	2.032		-	<b>2 3</b>	
0 000		EX921143	Ç,	2010		83	20.0	2 20 7	20.50	200	000	2 S	22.7		
~ α			2 4		2001	83		72.0	0.30	0.00	2 984		1.7		
00		EX021146	7.			3 %		75.0	> 05.00	0.30	3.017		2.7	100	101
.0	136 EX	EX921147	9			8	0.075	0.62	< 0.30 <	0.30	3.065	JOH V	3.1	V MDL	· MDL
=		EX921148	25			<b>%</b> :	0.075	7.05	< 0.30 <	0.30	3.057		6. K	<u>2</u>	JOE V
12		EX921149	ನ	2985		8:	0.07	8.42	0.30	0.21	2.988	₹ •	42.7	2 2 3	- 3
7.5		EX921150	\$ \$			83	0,0	87.0	0.50	0.50	200	2 <u>2</u>	٠. ٢. د		<u> </u>
23		EX921152	55	3015	3008	3 %	000	0.76	× 0.30 ×	0.30	3.012	. v	m m	101	- F
54		EX921153	=			* 89	0.075	0.34	< 0.30 <	0.30	3.035	JOH Y	1.6	JOH >	JOH >
13		EX921154	35			<b>9</b>	0.075	0.30	< 0.30 <	0.30	3.036		+ .	10E	10±
<b>1</b> 5		EX921155				8:	0.07	0.57	× 0.30 ×	0.30	2.983	를 를 * '	5.5	로 5 • ·	ار د د
5 7		EX921156	2 5			84	200	20.00	0.50	0 ° °	200		- v		- ^
o <u>t</u>		EX921137	<u> </u>			* ×		09	0.30	55.0	3.056	2 E	. w		- 60
8			53	3036		88	0.075	0.57	< 0.30 <	0.30	3.047	e v	2.8	10H V	TON >
4		EX921160	25			<b>9</b>	0.075	2.18	< 0.30	0.34	20.0	) *	10.7	₽ •	1.7
-			₽:			> 29	0.07	9.0	× 0°.30 ×	0.30	3.015	<b>Q</b>	5.5	<b>E</b> 9	₹.
		EX921162	7,4	3003		V /9	0.0 C K	86.0	0.30	0.50	× ×		3 %	, 1	- k
P over		EX921103	£ 5			* *		3,45	0.30	200	2.063		200		
		921131	5			× 29	50.0	0.41	< 0.30 <	0.30	3.014	10£ >	2.0	104 >	· MOL
<b>72</b>		EX921132	-			> 19	0.075	5.78	< 0.30 <	0.30	2.979	Y NOT	0° &	· MDL	V MOL
34		EX921133	2	3018		8:	0.088	3.68	< 0.30 <	0.30	3.033	7.0	4.0	<b>1</b>	<u> </u>
9 2		EX921134	₹ 5			83	50°C	0,78	20.30	35	7.002		, 0		
97		021136	2 5			8 8	200	27.0	0.30 ×	0.30	2.977				
8		200	3			3						no sampleno			
BLANK											0.000	no sampleno no sampleno	no sampleno no sampleno	no sampleno no sampleno	o sample o sample
														***************************************	7000000
LOCATION		SAMPLES	MITRIC	FILTER	IMP INGER	SAMPLE (CU FT)	(rg)	ZINC (ng)	STROWT IUM (ug)	(ug) (M3)	SAMPLE (M3)	LEAD (ug/H3)	21KC (Vg/K3)	(ug/N3) (ug/N3)	(ug/N3)
EXHAUST RECIRC	۵۵	EX921451   EX921459	EX921452 EX921460	EX921453 EX921461	EX921454 EX921462	49.30	010	51.4	0.93	16.73	1.395	4.0 4.0	39.6	0.5	12.0
				EXHAUST			2.5	24.0	0.93	1.08	1.395	101 >	17.2	0.7	0.8
							2.5	1.3	^ ^ 0.2 0.5 0.5	0.65		<u> </u>	9.0.5	<u> </u>	4.00
					IMPINGER	EX921454 <	6.5	77	× 0.2	13.00	C	V MOL	0.0		 

TEST: METALS #5 DATE: 06-26-92 AM2 METHOD: NIOSH 7300 Non paint time deducted	TRAVIS PAINT ACUREX	AFB BOOTH TESTS ( PROJECT 8485	PA	PAINT: G	GUNSHIP GRAY POLY THRUST REVERSER	NY POLY ERSER			0 0 E	D E INITIALS: Q A INITIALS:	ž
ACUREX BASE GRID LOC SAMPLE # SAMPLE # PUMP # (ml/min)	PRE-CAL (ml/min)	POST-CAL RUN TIME (ml/min) (min)	LEAD ZI (ug) (t	ZINC S (ug)	(Ug)	CHROMIUM (ug)	CHROMIUM AVG FLOW (Ug) (L/MIN)	LEAD (ug/M3)	ZINC (ug/M3)	STRONT IUM (ug/M3)	CHROMIUM (ug/M3)
	RECIRC	ACETONE EX921459 < NITRIC EX921460 < FILTER EX921461 <	2.5 0.5 2.5 <	13 7.6 4 1.25 4 29 4	0.58 0.2 0.5 0.2	3.2 7.60 1.03 19.00	1.253	<u> </u>	10.4 6.1 4.80 23.2	0.5 * #0! * #0! * #0!	2.6 6.1 15.2

0			INLET GRID	1 <b>6</b> 1	28 • PDL	£,		EXHAUST DUCT: < NOL
D A INITIALS:	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	10M > 7	80 V	12 • FDL	24 < MOL	16	20 <b>* MOL</b> <b>* MOL</b>	
8485	6 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	3 < MOL	7 < 150	11 A MOL	23 < 401.	15	19 ^ MDL	GRID MOL: 0.075 ug/SAMPLE
ACUREX PROJECT 8485	EXHAUST GRID	104 > 2	10H > 9	10 < MDL	22 < MOL	14 < MDL	18 < MDL	ug/N3
72		10£ >	10	TOM >	21 < PDL	13	17 < MOL	CMITS:
METHOD: NIOSH 7300 Non paint time deducted GRID CHART 1 - LEAD	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	Painter Over < NDL Painter Under < NDL	INLET GRID A	10 <b>.</b> >	70e ×	XA A		PAINT TYPE: GUNSHIP GRAY POLY

S: LJL 0			INLET GRID		28 3.9	34 2.1	·	EXHAUST DUCT: 36.8 RECIRC DUCT: 39.6
D E INITIALS: LJL Q A INITIALS:	8	4 1.7	82	12 42.7	24 1.6	16 2.8	20 3.3 3.4	3 ug/SAMPLE 3 ug/SAMPLE
TESTS CT 8485	EXHAUST GRID	æ ئ.	7 22.7	11 34.9	3.8	15 1.6	19 10.7	GRID MOL: 0.3 ug/SAMPLE PAINTER MOL: 0.3 ug/SAMPLE
TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485	EXH	2 1.7	6 MOL 2.4	10 3.1	22 2.4	14 2.9	18 2.8	ug/H3 1000 ug/H3
ted.		4.6	ر د نع	9 2.7	21 1.9	1.5	17 3.4	UNITS: OSHA TWA:
TEST: METALS #5 DATE: 06-26-92 AM2 METHOD: NIOSH 7300 Non paint time deducted	פאות כאשאו כי בואר	Painter Over 3.2 Painter Under 2.9	INLET GRID A	5.0	28.0 29.0	34 18.4		PAINT TYPE: GLMSHIP GRAY POLY  OBJECT: THRUST REVERSER

B TH TESTS OJECT 8485	3 < HDL	10H > 10H > .	11 12 12 + MDL < MDL	23 24 NDL < NDL	15 16 16 × 101 × 101	19 ° 801 ° 8
TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8485	2 < MDL	10# > 10# >	10 • #DL	22 • NDL	14 A MOL	18 ^ <b>9</b> 0L
TEST: METALS #5 DATE: 06-26-92 AM2 METHOD: NIOSH 7300 Non paint time deducted GRID CHART 3 - STRONTIUM	1 < 100.	\$ * MOL	, * **********************************	74 • <b>3</b> 0	13 < PDL	17 < 10L

INLET GRID B 12.0 24.6 28 **, H**DL æ , 1€ 38 • 101 **EXHAUST DUCT:** RECIRC DUCT: 0 D E INITIALS: LJL Q A INITIALS: 20 < MOL 1.5 24 < HOL 1:1 2.1 ) 10# v A MOL GRID MOL: 0.3 UG/SAMPLE PAINTER MDL: 0.3 Ug/SAMPLE 42 9 60 £. 1.7 ±2, 10€ 10€ 7 < MOL 11 4 MDL A MOL **EXHAUST GRID** 2 6 TRAVIS AFB
PAINT BOOTH TESTS
ACUREX PROJECT 8485 22 < MDL 10 • 101 18 • 101 를 를 당 수 14 < PDL of v OBJECT: THRUST REVERSER OSHA TWA: 50 UG/M3 PAINT TYPE: GUNSHIP GRAY POLY UNITS: UG/M3 2.8 13 < HDL 21 < HOL 10H > · MOL **₩** > 4 TEST: METALS #5
DATE: 06-26-92 AM2
METHOD: NIOSH 7300
Non paint time deducted
GRID CHART 4 - CHROMIUM Painter Over Painter Under < MDL INLET GRID A \*\* . #0L אסו א ₽ \*

TEST: DATE:	ISOCYANATES 06-23-92 AM		TRAVIS AFB PAINT BOOTH	AFB DOTH TESTS	PAINT: S OBJECT:	WHITE TOPCOAT	COAT	D E by: Q A by:	N.
TE I HOU:	USHA 42/NIUSH	ISCC NSOIN			Printed:	das-57			
GRID LOC	ACUREX FILTER #	BASE SAMPLE #	PUMP #	PRE-CAL (ml/min)	POST-CAL (ml/min)	RUN TIME (min)	(gg)	AVG FLOW (L/MIN)	HD1 (ug/M3)
-	19	EX920714	41	726	920	09	2	0.924	OH >
2	21	_	13	626	1058	58	2	1.019	V MOL
M	٥	EX920716	4	1009	1000	09	Q	1,005	V MOI
4	4	EX920717	35	716	086	09	Q	0.982	ON V
5	14	_	33	8	1018	9	2	1.009	TOM >
9	2	EX920719	12	945	776	09	QN	0.961	V MOI
7	9		20	975	981	9	2	0.978	TOH >
80	13	EX920721	2	992	975	9	2	786.0	V MOI
0	12	_	15	993	1019	09	2	1.006	YOH >
5	S	_	18	696	786	9	Q	0.978	Y HOL
=	80	EX920724	10	786	1056	61	2	1.022	< MOL
	17	_	14	945	945	8	2	0.945	YOH >
12 DUP	23	_	43	88	970	9	Q	0.983	Y HOL
21	33		<b>*</b>	1001	1036	09	Q	1.019	Y HOI
22	16	EX920727	57	020	1015	9	Q	0.997	JOH Y
23	₽	EX920728	٥	863	1045	9	2	1.019	TOH Y
54	_	EX920729	×	866	985	3	9	0.989	- HOI
13	30	_	07	8	1011	8	Q	1.003	JOH >
7	23	_	2	566	1040	97	Q	1.017	YOH >
	31	_	22	935	971	8	S	0.953	YOH >
15 000	35	_	42	1003	1008	8	2	1.006	Y MOL
16	56	_	sn.	8	1004	61	£	266.0	<b>MOL</b> >
17	27	_	_	8	1005	3	Q	0.998	JOH >
8	K	_		8	966	8	9	0.993	10# ×
6	54	_	7	952	1160	8	£	1.056	10H >
		_	23	1034	1056	8	2	1.045	< +DL
P over	0051 imp	_	19	786	963	29	16	726.0	278.6
P under	0050 imp	_	30	962	1024	20	0.2	0.993	3.4
¥	8	_	M	066	786	26	£	0.989	10H >
2	&	_	28	970	981	29	2	0.976	Y MOL
AA.	28	_	27	965	963	29	2	796.0	< HDL
9	=	EX920711	32	876	929	29	9	0.939	JOH >
28	32	EX920712	31	937	932	29	£	0.935	Y HOL
880	\$	EX920713	22	942	8	25	£	696.0	· HOL
F BLAKK	10,000	0,0000			0			-	no sample
DECTED #		EX920049	25	C 40	4054	25	9 0	1.927	10.0
200		EAVEOUND	,		100			200-	

O A INITIALS: BM		INLET GRID	104 × 100 ×		·	EXHAUST DUCT: 16.9 RECIRC DUCT: 17.3
	, < HDL	8 < MOL	12 < MDL < MDL 24 < MDL 24	16	20 <b>POL</b>	ug/SAMPLE 15 ug/SAMPLE
S1S	A MOL	7 < 401	11	15 < MOL < MOL	19 < 1101.	GRID MOL: 0.5 ug/SAMPLE PAINTER MOL: 0.05 ug/SAMPLE
TRAVIS AFB PAINT BOOTH TESTS	Z < MDL	104 >	10 < HDL 22 < HOL	14 N NDL	18 • HDL	UNITS: UG/M3 OSHA TWA: 40 UG/M3
	1 <del>-</del> 5 <u>-</u> 5 <u>-</u>	5 - FDL	9 < 1901 21 < 1901 4 1901	104 ×	17 < HDL	
TEST: ISOCYANATES #1 DATE: 06-23-92 AM METHOD: 0SHA 42/NIOSH 5521 GRID CHART 4 - HDI	Painter Over 278.6 Painter Under 3.4	INCET GRID A	** *** *******************************	년 * 동		PAINT TYPE: WHITE TOPCOAT OBJECT: COMFORT PALLET

LET TOO					SULVE LANGE			- 12	
	_	OSHA 42/NIOSH 5521	TRAVI	TRAVIS AFB PAINT BOOTH TESTS	T BOOTH 1	ESTS		Printed:	24-Sep
GRID LOC	ACUREX FILTER #	BASE SAMPLE #	PUMP #	PRE-CAL (ml/min)	POST-CAL (ml/min)	RUN TIME (min)	(g)	AVG FLOW (L/MIR)	HDI (Ug/H3)
•	65	EX920683	41	876	796	99	£	0.956	OH V
N	09	EX920684	15	866	1005	29	9	000	G.
PP.)	54	EX920685	23		1048	38	9	1.044	GW V
4	36	EX920686	28	,	1006	55	9	0 0085	i GN V
. ru	2	_	12		070	3	9	0 07	
· <b>v</b> C	29		, P.	-	1000	3 %	9	1 001	No.
1	69	_	14		1000	3 %	2 9	0805	
7 DUP	23	_	4	1004	1003	3 3	2 5	1 0045	
	515	_	-	1000	180	3 \$	2 9	0005	
0		FX920692	12	071	077	3 %	2 9	0.057	
10	28.		12	1021	1078	3 \$	2 9	1 0505	
-	3	_	17	800	1005	3 3	2 9	1 0015	101
12	38	_	07		8	3.5	9	0.0025	
2	58	_	23		1019	38	9	1.007	G. V
22	36	_	43		993	8	2	-	NO.
23	42	EX920698	\$2	•	1020	65	2	1.0165	₩ •
5	88	_	10		973	8	2	0.9805	10£ ×
24 PCP	m	EX920700	18	1017	1026	8	ş	1.0215	
		_	-	982	1008	19	2	0.995	<b>10H &gt;</b>
13 000	67	_	22	971	1036	22	ş	1.0035	Y HOL
14	57	EX920703	13	796	1014	3	0.8		12.6
5	20	EX920704	21	1000	1003	9	£	1.0015	V MOL
92	48	EX920705	54	970	1017	8	ş	0.9935	YOH Y
17	44	EX920706	_	988	1014	8	皇	1.001	JOH Y
<b>9</b> 2	55	EX920707	42	1019	1016	65	웊	1.0175	< MOL
5	_	EX920740	SO.		1010	8	윺	1.0085	S V
2	7,4	EX920673	×		1052	9	2	1.05	10H >
P over	. 0060imp	_	33	1045	1060 0301	9	<b></b>	_	43.9
P under	. 00621mp	EX920062	35		1016	65	0.2	_	3.0
¥	8	_	100	883	975	8	윺	0	ig v
ঠ	97	_	•	1000	1008	%	2	1.00%	V NOT
34	•	-	27	_	1071	8	물	1.064	<b>₩</b> ×
#	2	EX920680	30		8	65	£	0.9	Y MOL
28	•	EX920681	19	•	1015	39	웊	1.0115	A MOL
38	4	_	•	980	959	8	윺	0.9695	JOH Y
F BLANK	. 45	EX920676	26	호	1012.114	65.48571	0.5	1.006157	7.6
<b>EXHAUST</b>	C 67	EX920671	2		1039	. 58	윺	1.023	<b>10</b> 4 ×
RECIRC C		EX920672	32	_	966	29	웊	1.0045	₽ •
<b>EXHAUST</b>	1 0063 imp		38		1038	58	2	1.048	32.9

Q A INITIALS: Q A INITIALS: printed: 24-Sep		Field Blank 7.6 Nominal value	INLET GRID B		284 ADL	38 88		EXHAUST DUCT: < WOL CASSET 32.9 IMPING PROPERTY ( MAIL CASSET)
	8 8 8 9 9 9 9 9	10st > 7	85 JGE A	12 < HDL	24 < MDL < MDL	16 • FDL	20 < HDL	og/SAMPLE
ESTS	EXHAUST GRID	3 < MOL	70H >	11 < FDL	23 • PDL	15 • MDL	. 19 × × × × × × × × × × × × × × × × × ×	GRID MOL: 0.5 ug/SAMPLE
PAINT BOOTH TESTS	EXHA	2 < FDL.	10e > 9	10 < MDL	22 < MOL	14 12.6	18 < MDL	UNITS: US/N3
		1 < #DL	10e > 5c	9 < MOL	21 • HDL	13	17 < MOL	TOPCOAT
DATE: 06-25-92 AMZ DATE: 06-25-92 AMZ METHOD: 05HA 42 & NIOSH 5521	ART 3 -	Painter Over 43.9 Painter Under 3.0	INLET GRID A		2A < MOL	3A _ HOL		PAINT TYPE: WHITE TOPCOAT

Color   Colo	TEST: 1 DATE: 0 METHOD: 0	150CTANALES 06-25-92 PM 0SHA 42 & N	R NIOSH 5521		PAINT BOOT ACUREX PRO	TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8463	, ra	PAINT: OBJECT:	CAMEL GRAY AIR SPLITTERS	ERS		D E	INITIALS: INITIALS:	1
73         EVR20537         113         1014         1018         56         ND         ND         1016         ND         1016         ND         1016         ND         1016         ND         1016         ND         ND         ND         ND         1016         ND	GRID LOC F	CUREX	<b>*</b> ±		PRE-CAL (ml/min)	POST-CAL (ml/min)	RUN TIME (min)	101 (9a)	(6n)	HD 1	AVG FLOW		MD1 (ug/M3)	HD1 (ug/M3)
94. KEN200338         12. 973 973 973 978         18. ND         ND         0.9755 8401         8 ND         ND         0.9755 8401         8 ND         ND         ND         ND         ND         10.0035 8401         8 ND         <	-	27	EX920537	13	1014	1018	56	Ş	Ş	æ	1.016	\ MDL	JOH >	JOH >
77         REVOCASION         2.8         100.6         1011         57         ND         ND         10.0085         < MD         < MD           6.4         REVOCASION         2.4         1017         1000         1001         57         ND         ND         ND         10.0035         < MD	~	76	EX920538	12	973	978	58	QN	QN	ð	0.9755	A MOL	A MOL	<b>₩</b> •
RE REPORTINGAL         24         1017         1029         558         ND         ND         10.023         < ND            RE REPORTINGAL         31         1001         1003         597         58         ND         ND         1000         < ND	M	11	EX920539	28	1006	1011	57	QN	Q	2	1.0085	Y MOL	→ MOL	V MDL
R. EV92054.1         3.1         1000         1001         57         ND         ND         ND         1000         6 MD         6 MD         ND         1000         6 MD         6 MD         ND         1000         6 MD	4	78	EX920540	54	1017	1029	58	QN	9	2	1.023	JOH >	< MOL	Y MDF
BB EN920542         11         1003         997         58         ND	S	ž	EX920541	31	1000	1001	57	QH.	2	2	1,0005	TOH >	TOM >	OH V
BS EX2056,7         11         1008         1008         SB         ND         ND         ND         10.08         CMD         ND <td>9</td> <td>88</td> <td>EX920542</td> <td>21</td> <td>1003</td> <td>200</td> <td>58</td> <td>Q</td> <td>9</td> <td>2</td> <td>-</td> <td>IOH &gt;</td> <td>OH V</td> <td>IQH V</td>	9	88	EX920542	21	1003	200	58	Q	9	2	-	IOH >	OH V	IQH V
REVENDESALATION         1         981         980         58         ND         ND         0.9805         < MOIL         CMD	ے	89	EX920567	=	1008	1008	58	2	2	2	1.008	- FOL	Q V	- FE
79         ENZOSCÁL         20         972         966         56         ND         ND         ND         10.05         < MD         MD         ND	~	82	EX920543	-	981	980	58	2	2	2	0.9805	YOL >	JOE V	JOE V
92 EV220545 14 1078 1076 58 ND ND ND 1.075 < MD < MD 1	0	2	EX920544	20	972	896	58	9	9	2	0.97	JOH V	JOH >	- HOL
85 EX920546         29 1020         1016         58 ND         ND         1,018         < MOL            86 EX920546         24 1034         1034         1104         58 ND         ND         ND         1,0915         < MOL	0	92	EX920545	14	1078	1074	58	9	9	2	1.076	JQ£ >	JOH >	- FDI
91 EX920547 4 1093 1104 558 ND ND ND 1.0985 < MOL < MOL < MOL 92 EX920546 5.2 1036 1036 1046 58 ND ND ND 1.0915 < MOL 93 EX920546 6.1 1036 1002 58 ND ND ND 1.0077 < MOL 94 EX920557 104 104 104 104 58 ND ND ND 1.0077 < MOL 95 EX920559 10 973 1046 1002 58 ND ND ND 1.0079 < MOL 96 EX920550 17 1005 1000 58 ND ND ND 1.0075 < MOL 96 EX920550 17 1005 1000 58 ND ND ND 1.0075 < MOL 97 EX920550 17 1005 1000 58 ND ND ND 1.0075 < MOL 98 EX920550 17 1005 1000 58 ND ND ND 1.0075 < MOL 99 EX920550 17 1005 1000 58 ND ND ND ND 1.0075 < MOL 90 EX920550 17 1005 1000 58 ND ND ND 1.0075 < MOL 90 EX920550 17 1005 1000 58 ND ND ND ND 1.0075 < MOL 90 EX920550 17 1005 1000 58 ND ND ND ND 1.0075 < MOL 90 EX920550 17 1005 1000 58 ND ND ND ND 1.0075 < MOL 90 EX920550 17 1005 1000 58 ND ND ND ND 1.0075 < MOL 90 EX920550 17 1005 1003 57 ND ND ND 1.0075 < MOL 90 EX920550 17 1007 1003 57 ND ND ND 1.0075 < MOL 90 EX920550 17 1007 1003 57 ND ND ND 1.0075 < MOL 90 EX920550 17 1007 1003 57 ND ND ND 1.0075 < MOL 90 EX920550 17 1007 1003 57 ND ND ND 1.0075 < MOL 90 EX920550 17 1007 1003 57 ND ND ND 1.0075 < MOL 90 EX920550 17 1007 1003 57 ND ND ND ND 1.0075 < MOL 90 EX920550 17 1007 1007 58 ND ND ND ND 1.0075 < MOL 90 EX920550 17 1007 1007 58 ND ND ND ND 1.0075 < MOL 90 EX920550 17 1007 1007 58 ND ND ND ND 1.0075 < MOL 90 EX920550 17 1007 1007 58 ND ND ND ND 1.0075 < MOL 90 EX920550 17 1007 1007 58 ND ND ND ND 1.0075 < MOL 90 EX920550 17 1007 1007 58 ND ND ND ND 1.0075 < MOL 90 EX920550 17 1007 1007 58 ND ND ND ND 1.0075 < MOL 90 EX920550 17 1007 1007 58 ND ND ND 1.0075 < MOL 90 EX920550 17 1007 1007 58 ND ND ND ND 1.0075 < MOL 90 EX920550 17 1007 1007 58 ND ND ND 1.0075 < MOL 90 EX920550 17 1007 1007 58 ND ND ND 1.0075 < MOL 90 EX920550 17 1007 1007 58 ND ND ND 1.0075 < MOL 90 EX920550 17 1007 1007 1007 58 ND ND ND 1.0075 < MOL 90 EX920550 1	0	85	EX920546	52	1020	1016	58	9	9	2	1.018	V MOL	A FOL	V HDL
86         ENY205648         22         1034         1067         50         ND         ND         1,0515         < ND            76         ENY205648         41         964         951         59         ND         ND         1,0515         < ND	=	91	EX920547	4	1093	1104	58	Q	2	읖	1,0985	A MOL	JOH V	JOH >
95         R/9205546         41         964         951         59         NO         NO         0.0577         6 MO         6 MO           96         R/920554         104         1046         58         NO         NO         1.067         6 MO         6 MO           97         1046         1046         58         NO         NO         1.007         6 MO         6 MO           96         107         1046         58         NO         NO         1.007         6 MO         6 MO           96         107         1046         1046         58         NO         NO         1.0075         6 MO         6 MO           96         107         107         104	ē.	8	EX920568	22	1036	1067	50	QN.	Q	2	1.0515	YOH Y	TOM Y	Y HDL
76         EV920557         23         1046         1046         58         ND         ND         ND         1.047         < MD            77         EV920558         16         1000         1002         58         ND         ND         ND         1.001          MD            78         EV9205560         25         1019         1024         58         ND         ND         1.001          MD            96         EV9205560         17         1014         1017         58         ND         ND         ND         1.0055          MD            101         EV9205560         17         1014         1017         58         ND         ND         ND         1.0055          MD         ND         ND         1.0055          MD         ND	~	R	EX920548	41	38	951	59	Q	ş	2	0.9573	< MOL	JOH V	Y HOL
77 EAV20558         16         1000         1002         58         ND         ND         ND         1.001         < MOL            71 EAV20559         16         973         1045         58         ND         ND         1.0045         < MOL		92	EX920557	ສ	1048	1046	58	Q		S	1.047	Y HOL	YOH V	<b>₩</b>
71 EXP22055         10         973         1045         58         ND         ND         ND         1,009         < MOL            96 EXP2056         15         1019         1024         58         ND         ND         1,0045         < MOL	Ņ	26	EX920558	9	1000	1002	58	9	Q¥	ş	1.001	V HOL	V HOL	< FOL
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YEXPLOSES         34         1052         1050         208         ND         ND         1051         C MOL <td>Ω,</td> <td>8</td> <td>EX920551</td> <td>2</td> <td>1026</td> <td>1024</td> <td>800</td> <td>2</td> <td>2</td> <td>2</td> <td>1.025</td> <td>JOH V</td> <td></td> <td>2 2</td>	Ω,	8	EX920551	2	1026	1024	800	2	2	2	1.025	JOH V		2 2
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104 EX920535 2 1039 1061 51 ND ND 1.05 < MDL < MDL < MDL < ST MD ND ND 0.9925 < MDL < MDL < ST MD ND ND 0.9925 < MDL < MDL < ST MD ND ND 0.9925 < MDL < MDL < ST MD ND ND 0.5925 < MDL < MDL < ST MD ND 0.5 1.048 < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL < MDL	8			•0	959	978	58	Q.	오	Ş	0.9685	JOH >	JOH >	JOH V
104 EX920535 2 1039 1061 51 NO ND ND 1.05 < NDL < NDL < ST 52 996 989 52 ND ND ND 0.9925 < NDL < NDL < ST 53 ND ND ND 0.5925 < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL < NDL <	¥										0	no semple	no sample	o sample
81 EX920536 32 996 989 52 ND ND ND 0.9925 < MDL < MDL < 1 371mp EX920037 36 1038 1058 51 ND ND 0.5 1.048 < MDL < MDL < MDL 391mp EX920039 39 1069 1086 52 ND ND 0.2 1.0775 < MDL < MDL	S	2	EX9	2	1039	1061	51	£	2	Ş	1.05	<u>6</u>	· HDL	JOH >
1 37imp EX920037 36 1038 1058 51 ND ND 0.5 1.048 < MDL < 1 1 39imp EX920039 39 1069 1086 52 ND ND 0.2 1.0775 < MDL < 1	U	æ	EX6	32	8	686	52	Ş	2	윷	0.9925	10H >	<b>1</b> 0 ×	) V
EX920039 39 1069 1086 52 ND ND 0.2 1.0775 < MDL < 1	-	37imp	EX6	%	1038	1058	51	2	2	0.5	1.048	_ ₹ •	JOH V	7.6
	_	39 imp	EX63	36	1069	1086	25	2	£	0.2	1.0775	- <b>NO</b> -	10K *	3.6

INLET GRID B 00 28 < MDL 18 • FDL 38 • POL D E INITIALS: Q A INITIALS: 24 < MDL 12 < MDL 16 \* PDL 20 \* MDL JOH > JOH > 8 19 < PDL 7 < MDL = ` ` ` JOH > 23 • PDL **EXHAUST GRID** TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8463 10.4 14 • MOL • MOL • MOL JOH V \* \* \* 10 • #DL 22 < MOL 18 21 < MDL 13 < PDL 9 \* **10**L 17 \* FDL A MOL ◆ MDL TEST: ISOCYANATES #3
DATE: 06-25-92 PM
METHOD: OSHA 42 & NIOSH 5521 Painter Over 17.2 INLET GRID A Painter Under 3.3 GRID CHART 3 - HDI \* , \*PDL 3A \* MDL า<u>ด</u> ส

TEST: DATE: METHOD:	1SOCYANA 06-30-92 0SHA 42	TES #4 AM1 & NIOSH 5521		TRAVIS AFB PAINT BOOT ACUREX PRO	TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8463	ឆ	PAINT: 08JECT:	DARK GRAY TOPCOAT QEC PANELS (PLANE SIDING)	TOPCOAT (PLANE	SIDING)	D E	INITIALS: INITIALS:	וזו
GRID LOC	ACUREX SAMPLE #	BASE SAMPLE # PUMP	**	PRE-CAL (ml/min)	POST-CAL (ml/min)	RUN TIME	101 (gu)	<b>(</b> 6n)	101 (00)	AVG FLOW (L/MIN)	1D1 (ug/M3)	MD1 (ug/M3)	HD1 (ug/M3)
-	148	EX920578	71	970	950	61	2	Ş	Ş	0.96	JOH >	7 <b>0₩</b> >	- MDL →
~~	156	EX920579	45	_	1014	61	2	Q	ş	1.028	< MDL	¥OF ∨	V MDL
M	159	<b>EX92</b>	34	1010	766	61	Q	9	9	1.002	<b>₩</b>	<b>₹</b>	√ #DL
4	151	EX920581	31	_	1066	61	2	9	Q.	1.08	^ <b>₹</b>		) <b>F</b> D
ī	174	EX920582	-			62	9	2	9	196.0	YOK Y	JOH >	V MOL
•	152	EX920583	19	_		61	S	9	2	1.012	A MOL	JOH Y	JOH V
4 DOP	155	EX920584	51	_		61	OR.	ş	9	1.0125	<b>₹</b>	JQ¥ ∨	v ¥Di
	157	EX920585	17	1023		61	2	Q	2	1.143	<b>₩</b>	V ₩DF	<b>₩</b> 0
•	147	EX920586	67			61	2	9	ş	0.9865	· HOL	10E v	10 <u>H</u> >
٥	154	EX920587	11			62	2	æ	2	1.0245	v ¥0r	<b>#</b> 01	<b>₩</b>
10	173	EX920588	55	•		61	Ş	9	Q	1.0045	<b>* * D *</b>	TOH Y	10£ ×
Ξ	•	EX920589	43	_		61	9	2	ð	0.000	<b>₩</b> >	10E >	
12	_	EX920590	13			8	2	9	Q.	0.9945	10# >	101 V	2 •
2	_	EX920591	2	_		61	2	2	Ş	1.0395	10± ×	<b>Q</b> •	₽ •
22	_	EX920592	21	-		61	2	9	2	1.017	<b>10</b> 1	٦ ٧	2 V
23	•	EX920593	18			61	2	2	2	1.0035	2		2
54	_	EX920594	54	•		9	Ş	2	2	1.014	2	101	2
13	_		24	·		6	2	2	£	2003			
14	121	EX920596	45				2	2	v. 0	210.1			200
5;	_ `		7			5	2 9	2 9	9	1.032			
2	<b>,</b> 4	EX920598	-			5	2 5	2 5	2 5	1 0125			2
	141	EX920399	7 6	•		4.5	2 5	2	2	0.0085	TON V	loi v	OH V
20		FX92	100	1015	982	6.0	2	9	0.5	0.9985	JOH Y	JOH >	8.5
20	-	EX92	8			61	2	2	£	1.0215	JOH Y	V MOL	10E >
20 DUP	_	EX92	m			61	2	Q	£	1.035	<u>Q</u>	10± ×	9
P over		EX920058	48			61	2	2		0.991	<b>1</b> 9	<b>1</b>	16.5
P under	S9 imp		3	·	Ì	.63	2	2	2	0.9805			10.
¥	•	EX92	3	-		61	2	2	2	1.000			2
Z	-	EX92	-	•		19	2	2	2	C9C4.0			
34	200	EX92	'n			5	2	2	2	10.0			
	_	EX95	7	1028	1015	5	2	2	2	5120.1			
18 000		EX92	9			61	2	2	2	7.030			
28	_	EX95	32	_	1036	9	2	2	2	1.0345	10E >		
38		EX92	<u>ت</u>	955		5	£	2	2	0.948			) NO.
F BLANK	0040			LOU	values	3	2	2	2.0	- (			7.0
F BLANK		EX95	~	nominal	values	3	2	2	2		2		104
<b>EXHAUST</b> (	77F C		52	_	766	22	ş	물	£	0.998			)   
RECIRC C		EX95	<u>.</u>	866		25	₽	<b>2</b>	2	6,6,0			
EXHAUST	1 57 imp	EX92	×			22	2	웊		0.9365	2	2	2.5
RECIRC I		EX92	ň			25	윷	£	2.0	16%.0	<b>1</b> € ×	) HOL	0.0

D E INITIALS: LJL Q A INITIALS:		Field Blank 1MP 3.3 FILT < MOL nominal values	INLET GRID B	<b>1</b>	28 4 MDL	38		EXHAUST DUCT: < MOL CASSETTE 19.0 IMPINGER
		, + HOL	8 • • • • • • • • • • • • • • • • • • •	12 < FDL	24 < HDL	16 • PDL	ر ب	2 9 6
STS 8463	EXHAUST GRID	3 < 190 L	7 < 101	11 00 >	23 * 10L	15 12.7	19 8.2	GRID MOL: 0.5 ug/SAMPLE
PAINT BOOTH TESTS ACUREX PROJECT 8463	EXHAU	2 < MDL	9 > 10# >	10 < #DL	22 < 1101.	14. 8.1	18 A PDL	UNITS: ug/H3
	; 0 1 2 2 2 3 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 < HDL	5 < MDL	70H >	21 < HDL	13 > PDL	17 < 101	U COAT
IEST: ISCUTANATES #4 DATE: 06-30-92 AMI METHOD: 0SHA 42 & NIOSH 5521 GRID CHART 4 - HDI			INLET GRID A	4 • • • • • • • • • • • • • • • • • • •	2A < 10L	S A		PAINT TYPE: DARK GRAY TOPCOAT UNITS: Ug/H3

Note: The field (solution) blank for NIOSH 5521 (used on the painter and duct samples) contained 0.2 ug, or a nominal 3.3 ug/H3 for a 60 minute test at 1 liter/min. The sample levels here are calculated in terms of actual volume and time.

0.951	RUN TE
0.948	1013 56 ND 1010 56 ND 952 57 ND 1066 57 ND
MO 0.9855 MO 0.9875 MO 0.9873 MO 0.9873 MO 0.9875 MO 0.9	
MO 1.006	828.25
1.028	8.23
1.068   Mol.	25.55
1,0025	
1,0065	
ND	26.26
No. 1.0235   No. 1.0235   No. 1.0335   No. 1.0335   No. 1.0335   No. 1.0335   No. 1.0335   No. 1.0335   No. 1.0335   No. 1.0335   No. 1.0415   No.	
NO   1.0305   NO   NO   NO   NO   NO   NO   NO   N	55
No	57
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TRAVIS AFB PAINT BOOTH TESTS ACUREX PROJECT 8463	EXHYD	2 < MOL	10± >	10 < PDL	22 < FDL < FDL	75 • FDL	18 < MDL	UNITS: UG/N3 OSHA TUA: 40 UG/N3
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TEST: ISOCYANATES #5 DATE: 06-30-92 AM2 METHOD: 0SHA 42 & NIOSH 5521	GRID CHART S - HDI	Painter Over 3.6 Painter Under 3.6	INLET GRID A	10 2 *	2A < FDL	¥,		PAINT TYPE: PRIMER OBJECT: PLANE ENGINE

Note: Primer does not contain isocymnates, however, the field (solution) blank for NIOSH 5521 (used on the painter and duct samples) contained 0.2 ug, or a nominal 3.3 ug/N3 for a 60 minute test at 1 liter/min. The level seen on the painter and duct samples here is the same 0.2 ug/sample calcusted in terms of the volume sampled.

### APPENDIX H

# QUALITY ASSURANCE/QUALITY CONTROL EVALUATION

A number of quality assørance/quality control (QA/QC) procedures were followed to assess the quality of the reported data. The data quality objectives (DQOs) are listed in Table H-1. The DQOs, defined in terms of measurement accuracy, precision, and completeness, were originally outlined in the Quality Assurance Project Plan (Reference 1). In response to the EPA QA review (Reference 2), the DQOs were subsequently revised and submitted in the Acurex Environmental letter dated 6 May 1992 (Reference 3). The high variability of normal booth operations causes difficulty in establishing DQOs.

# A. ASSESSMENT OF OVERALL DATA QUALITY

The DQO results are presented in Table H-2. Nearly all DQOs were achieved. Some objectives, for the integrated sampling, were not met for side-by-side duplicate samples taken at specific sampling locations. The variability detected from side-by-side duplicate analyses was due to sample orientation. Great effort was expended to ensure that the duplicate VOC, particulate, isocyanates, and metals sample systems had identical orientations. However, some samplers shifted slightly during painting.

### 1. Precision

To ensure data precision, air flow rate anemometer measurements at the booth exhaust and intake faces were obtained following each test. Duplicate anemometer measurements were taken at one randomly selected grid site per test. Split-flow duct flow rate measurements were taken according to EPA Method 2 prior to each sampling event. A duplicate measurement was taken every 2 days. Due to cyclonic flow patterns in the recirculation duct, it was not possible to measure the flow rate of the recirculated airstream using EPA Method 2. Therefore, the precision is undefinable.

To assess the precision of CEM sampling, the periodic zero, span, and reference gas response results were compared.

To assess precision of the integrated pollutant concentration measurements in the booth, duplicate samples were collected during each sampling event. Because sample collection occurred under dynamic operating conditions, a side-by-side sampling strategy was adopted to generate the required duplicates. The side-by-side samples were located and oriented as close to identically as possible, but under normal booth operating conditions the sampling system often shifted during the test. For this reason, the RPD at specific sampling locations was observed to be as high as 100 percent. However, when averaged over all the duplicate samples, the precision RPD DQO was met for each pollutant category.

Side-by-side duplicate samples were also collected in the integrated duct organic and isocyanate sampling events. Precision for EPA Method 5 and the Draft Multiple Metals trains could not be assessed because setting up side-by-side duplicate sampling trains was not possible.

TABLE H-1. DATA QUALITY OBJECTIVES.

Measurement Parameter	Measurement Method	Precision (RPD)	Accuracy (% Recovery)	Completeness (%)
Volume Flow				
Exhaust and intake faces	ACGIH Anemometer	20	±40	90
Ventilation ducts	EPA Method 2	20	±10	90
Particulate				
Exhaust and intake faces and painter	NIOSH 500	35	NM <sup>a,b</sup>	90
Ventilation ducts	EPA Method 5	NMc	NM <sup>c</sup>	90
Metals				
Exhaust and intake faces and painter	NIOSH 7300	35	±30	90
Ventilation ducts	Draft EPA Multiple Metals	NM <sup>d</sup>	±30	90
Organics				
Integrated	NIOSH 1300	35	±30	90
Continuous	EPA Method 25A BAAQMD ST-7	20 20	±20 ±20	90 90
Isocyanates				
Exhaust and intake faces and painter	OSHA 42	35	±30	90
Ventilation ducts	NIOSH 5521	35	±30	90
Paints				
% Volatile	Grab sample, wt. loss on drying	20	±20	90
Usage rate	Observation, gravimetric analysis	NMe	NMe	90
Density	Grab sample, wt/vol analysis	20	±20	90

<sup>&</sup>lt;sup>a</sup>NM = Not measured; not measurable.

<sup>&</sup>lt;sup>b</sup>Method states that the bias is not significant.

<sup>&</sup>lt;sup>c</sup>The primary error source is non-isokineticity. The isokineticity objective is 90 to 110 percent.

<sup>&</sup>lt;sup>d</sup>Precision (as relative standard deviation) listed in the method ranges between 10 and 25 percent.

<sup>&</sup>lt;sup>e</sup>Not definable. Estimated at ±50 percent.

TABLE H-2 DATA QUALITY RESULTS.

Measurement Parameter	Measurement Method	Precision (RPD)	Accuracy (% Recovery)	Completeness (%)	
Volume Flow					
Exhaust and intake faces	ACGIH Anemometer	5	NM <sup>a,b</sup>	95	
Exhaust duct	EPA Method 2	5	±2	95	
Recirculation duct	EPA Method 2	NMb	NM <sub>p</sub>	NM <sup>b</sup>	
Particulate					
Exhaust and intake faces and painter	NIOSH 500	32	NMc	90	
Ventilation ducts	EPA Method 5	NM <sup>d</sup>	NM <sup>d</sup>	90	
Metals					
Exhaust and intake faces and painter	NIOSH 7300	23	±15	90	
Ventilation ducts	Draft EPA Multiple Metals	NMe	±20	90	
Organics					
Integrated	NIOSH 1300	24	±30	86	
Continuous	EPA Method 25A BAAQMD ST-7	10 10	± 10 ± 10	90 90	
Isocyanates					
Exhaust and intake faces and painter	OSHA 42	10	NM <sup>f</sup>	95	
Ventilation ducts	NIOSH 5521	10	±18	90	
Paints					
% Volatile	Grab sample, wt. loss on drying	5	±13	100	
Usage rate	Observation, gravimetric analysis	NWa	ИМа	90	
Density	Grab sample, wt/vol analysis	2	±9	100	

<sup>&</sup>lt;sup>a</sup>NM = Not measured; not measurable.

bFlow rate is not measurable due to cyclonic flow patterns in the duct.

CMethod states that the bias is not significant.

The primary error source is non-isokineticity. The isokineticity objective is 90 to 110 percent.

<sup>&</sup>lt;sup>e</sup>Precision (as relative standard deviation) listed in the method ranges between 10 and 25 percent.

<sup>&</sup>lt;sup>f</sup>Spike analysis not conducted.

<sup>&</sup>lt;sup>g</sup>Not definable. Estimated at ±50 percent.

To assess precision of the paint percent volatile and density measurements, duplicate samples were collected and analyzed. The paint usage rate was determined gravimetrically. There is no practical method for assessing the precision or accuracy of this measurement.

## 2. Accuracy

Due to cyclonic flow patterns in the recirculation duct, the relative accuracy of the air flow rate measurements in the booth was not quantifiable. The accuracy of the measurement of the split-flow duct flow rate according to EPA Method 2 was established using calibrated standard pitot tubes.

To measure accuracy of the continuous organic concentration measurement, a midrange standard reference gas that was not a zero or span gas was used. A solvent mass balance calculation provided an additional means of measuring accuracy, by comparing the quantity of solvent released into the booth to the quantity measured by the continuous monitors in the exhaust streams.

Accuracy of the metals sampling at the exhaust and intake faces was measured through the spike and recovery of filter samples according to NIOSH 7300. NIOSH 1300 sampling accuracy was measured through the spike and recovery analysis of unused sample tubes. The spike compounds and concentrations were selected based on the paint solvents measured in the charcoal tubes. Spike and recovery analyses of particulate samples were not possible. For the exhaust and intake faces and the painter, accuracy for particulate sampling was not measurable. For the ventilation ducts, particulate measurement was also not measurable because the primary error source is non-isokineticity. The isokineticity objective is 90 to 110 percent.

OSHA Method 42 was followed in the analysis of isocyanate compounds obtained at the exhaust face and in the vicinity of the painter. The method does not call for spike and recovery samples, and such were therefore not performed. Instead, isocyanates standards were tracked to watch for instrument drift, loss of column performance, and other errors. In addition, four standards for each analyte were run at both the beginning and end of each analytical run. For NIOSH 5521, the laboratory obtained percent recovery data by spiking samples with urea.

To assess the accuracy of the paint percent volatile and density measurements, published values from MSDSs for these parameters were obtained from manufacturers and compared to the analytical results. Usage rate accuracy was not measurable.

# 3. Completeness

The 90-percent completeness DQO was selected based on the successful completion of similar projects in the past involving paint spray booth emissions sampling and evaluation. A completeness level of 90 percent ensured that sufficient valid data of known quality were collected to evaluate project success. A completeness of 90 percent was achieved in all of the sampling events, with the exception of the integrated organic sampling, in which an 85-percent completeness was achieved, rather than the projected 90-percent, due to the malfunction of the pumps used in the NIOSH 1300 sampling procedures.

# B. QUALITATIVE DATA QUALITY OBJECTIVES

The painting operations in the booth were highly variable and non-repetitious. Therefore, a primary concern was that the samples collected be representative of typical operations. For this reason, sampling occurred over a 3-week period.

Careful scheduling with the paint spray booth operator was required for the successful completion of this project. Acurex Environmental coordinated with the Travis AFB personnel to ensure that there was a sufficiently large workpiece backlog for each test series. Acurex Environmental also endeavored to ensure that a representative sample of each typical workpiece was evaluated.

### C. REFERENCES

- 1. Hughes, S. E. and Ayer, J., <u>Category III Quality Assurance Project Plan (QAPP)</u>, Acurex Environmental Corporation, Mountain View, California, prepared for U.S. Environmental Protection Agency, EPA Contract No. 68-D1-0146, Work Assignment 0/004, AEERL, Research Triangle Park, NC, March 1992.
- 2. EPA Quality Assurance Review of the Category III QAPP, EPA Contract No. 68-D1-0146, Work Assignment 0/004, April 1992.
- 3. Hughes, S. E. and Wolbach, C. D., Response to EPA Quality Assurance Review, May 6, 1992.

# APPENDIX I ECONOMIC CALCULATIONS

# SUMMARY TABLE

Costs for Incineration Devices with 35% heat recovery (Thousands of dollars) Capital Cost Annual O&M Cost \$550 \$297 \$192 \$127 \$81 Catalytic Incineration \$368 \$471 \$270 \$232 \$147 \$383 \$91 Annual O&M Cost Flowrate Thermal Incineration \$392 \$387 \$333 \$275 Capital Cost 15000 7500 3000 30000 dscfm 50 75 90 Percent Recirc

# ASSUMPTIONS

Capital cost for recirc/split-flow modification: \$60,000 VOC concentration in the exhaust increases linearly as the % recirc increases Net heat of combustion of volatile compounds is approximately

Exhaust Stream Characteristics

3000 Btu/scf

content	(Btu/lb)	0.41	0.81	1.62	4.06	
heat content	(Btu/scf)	0.03	90.0	0.12	0.3	
[NOC]	(mdd)	10	20	40	100	
		% recirc	0	50	75	

Calcs. in the manual are based on April 1988 dollars. Convert to August 1992 \$ with the following CE Equipment Indices: All calculations based on "Control Technologies for Hazardous Air Pollutants", EPA/625/6-91/014, June 1991. 369.4 Apr. 1988 CE Equipment Index:

Aug. 1992 CE Equipment Index:

390.8

Assume 10 year equipment lifetime and 10% annual interest rate.

40 hrs/wk 50 wks/vr	\$3.30 per 1000 cf \$0.06 per kWh	15000 dscfm 0.81 Btu/lb 77 F
Operating hours	Methane fuel cost Electricity cost	Fxhaust Temp.

# SAMPLE THERMAL INCINERATION CALCULATION

t recovery]		\$146,414 8 in. H2O 44511 kWh/yr \$2,626 \$1,750 \$263 \$3,500
[the spreadsheet calcs are set for 0, 35, 50, OR 70% heat recovery]	scfm scfm scfm	ANNUAL OPERATING COSTS DIRECT Methane Fuel Cost Pressure Drop Electricity usage Electricity costs Oper. Labor Costs Supervisory costs Maintenance labor and mat'l costs
[the spreadsheet calc	369.7 15369.7	\$162,627 \$191,900 \$308,960 \$326,858 \$60,000 \$386,858
98 % 35 % 0.253 Btu/lb-F 610 F 1600 F	Supplemental fuel (methane) requirements Total flow	nerator capital cost (Apr. 1988 \$) quipr:APITAL COSTS I Incin. Capital Cost (Apr. 1988\$) ug. 1992 dollars: ost to modify duct TOTAL CAPITAL COST
Destruction Eff. Heat Recovery Air Heat Cap (Cp) Temp. into Incin Combust. temp	Supplemental fuel (rr	Thermal Incinerator capital cost (Apr. Purchased EquipmAPITAL COSTS Total Thermal Incin. Capital Cost (Apr. Convert to Aug. 1992 dollars: Include the cost to modify duct TOTAL CAPITAL COST

\$3,308 \$7,737 \$3,869 \$3,869 \$62,981

> Administrative Property taxes Insurance

INDIRECT Overhead \$232,447

Capital Recovery
TOTAL ANNUAL OPER. COSTS

# **Economic Evaluation**

# SAMPLE CATALYTIC INCINERATION CALCULATION

					\$87,863	10 in. H2O	55103 kWh/yr	\$3,251	\$39,469	\$1,750	\$263	\$3,500		\$3,308	\$9,428	\$4,714	\$4,714	\$34,118	\$192,377
	scfm	scfm	ANNUAL OPERATING COSTS	DIRECT	Methane Fuel Cost	Pressure Drop	Electricity usage	Electricity costs	Catalyst replacement cost	Oper. Labor Costs	Supervisory costs	Maintenance labor and mat'l costs	INDIRECT	Overhead	Administrative	Property taxes	Insurance	Capital Recovery	TOTAL ANNUAL OPER. COSTS
	221.9	15221.9		\$204,694	\$241,538	\$388,877	\$411,405	\$60,000	\$471,405			r)			per cu ft				
997 F 1000 400	nents	flow		. 1988 \$)								40,000 (1/hr)	22.83 cu ft		\$3,000 per				
Temp at catalyst inlet Temp at catalyst outlet Temp after heat recovery	Supplemental fuel (methane) requirements	Total flow		Catalytic Incinerator capital cost (Apr.	Purchased Equipm APITAL COSTS	Total Incin. Capital Cost (Apr. 1988\$)	Convert to Aug. 1992 dollars:	Include the cost to modify duct	TOTAL CAPITAL COST			Space Velocity	Catalyst Bed Size	Assume a 2-vear catalyst life	Precious metal cost			3	

# **APPENDIX J**

# EXAMPLE CALCULATION WORKSHEET FOR PERCENT RECIRCULATION VERSUS PERCENT PARTICULATE REMOVAL EFFICIENCY

## PROJECTED POLLUTANT LEVELS WITH RECIRCULATION

This calculation assumes no split-flow.

% REMOVAL OF STRONTIUM CHROMATE 8 5

% REMOVAL OF ISOCYANATES: 85

RECIRCULATION RATE = 87.4%

This worksheet compares results to the TWA Em, not to the STEL

COMPOUNDS			-	
	DETECTED LEVEL W/O RECIRC. mg/m3	Current 8-hour TWA PEL or TLV mg/m3	PROJECTED LEVEL mg/m3	Booth Em Calculation (dimensionless)
ORGANICS VS. Em		-		
VOC1:	•			
MEK	5.80	590	•46	0.08
VOC2:				
MIBK	4.20	205	33	0.16
VOC3:				
TOLUENE	0.64	188	5	0.03
VOC4:				
N-BUTYL ACETATE	1.10	710	9	0.01
VOC5:	0.11	404	4	0.00
XYLENES VOC6:	0.11	434	1	0.00
ETHYL ACETATE	0.26	1400	2	0.00
VOC7:	0.26	1400	2	0.00
2-BUTANOL	0.28	305	2	0.01
2 50 1711 02	0.20	000	ORGANIC Em	0.29
METAL Em CALCULATIONS				Metal Em
STRONT CHROMATE as Cr	0.0063	0.05	0.050	1
ISOCYANATE Em CALCULA	TIONS			HDI Em
HDI	0.000570	0.034	0.005	0.13